

NOVA SCOTIA CEMERIMENT OF EUVIRONMENT LEBRARY

---PROVINCE OF NOVA SCOTIA DEPARTMENT OF THE ENVIRONMENT WATER PLANNING AND MANAGEMENT DIVISION PRELIMINARY REPORT

GROUNDWATER SURVEY OF THE PLYMOUTH AREA PICTOU COUNTY NOVA SCOTIA

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TABLE OF CONTENTS

ACKNOWLEDGEMENTS		
INTRODUCTION		
FIELD WORK		
LOCATION AND PHYSIOGRAPHY		
CLIMATE	2	
GEOLOGY Bedrock Surficial Glacial Histo	2 4 5	
GROUNDWATER FLOW		
GROUNDWATER QUALIT Salt Fluoride Origin Health In Economic	Y 7 pplications 12 Implications 12	
TESTHOLE RESULTS Surficial Bedrock	13 14	
CONCLUSIONS	15	
RECOMMENDATIONS		
BIBLIOGRAPHY		

FIGURES

APPENDICES

LIST OF FIGURES

1. Topographic location map, 1:50,000

2. Sample locations, Park area

3. Sample locations, general area

4. Bedrock geology

5. Bedrock surface elevations

6. Surficial geology

7. Depth to bedrock

8. Water table elevation, Park area

9. Piezometric levels, general area

10. Chloride as related to well depth

11. Na/CI ratio as related to Na/Ca ratio

12. Chloride values, Park area

13. Chloride values, general area

14. Fluoride as related to well depth

15. Fluoride as related to chloride

16. Fluoride as related to alkalinity

17. Fluoride as related to calcium

18. Trilinear plot of groundwater chemical composition

19. Cross section

20. Water level fluctuations in testholes, January to July 1976

LIST OF APPENDICES

- 1. Summary table of well data
- 2. Groundwater chemical analyses
- 3. Summary logs of wells drilled on the Stellarton Inverval, N.S.D.O.E. and N.S.D.M.
- 4. Summary logs of backhoe testpits, N.S.D.O.E.
- 5. Summary of N.S.Dept. of Highways Borehole Records
- 6. Summary of N.S.Dept. of Mines Borehole records
- 7. Letter from Dr. R.M. Brown
- 8. Letter from Mr.C.E.Tupper

We would like to express thanks to the many homeowners in the area for their interest and co-operation in the sampling program. Without their assistance this study would not have been possible.

We would also like to thank Mr.E.D.Stewart of E.D.Stewart Well Drilling and Mr. Wayne Chisolm of G.W.Reid Well Drilling for their interest and assistance in locating some of the well log information.

We also appreciate the time and effort of Mr. D. Hirtle of the N.S. Department of the Environment for the draughting of the figures.

INTRODUCTION

Due to the number of complaints of poor water quality in the Plymouth Park area, a survey was carried out in June and July 1975 to determine the extent and cause of the problem, and possible solutions to the problem. Specifically, the complaints were of salt, iron, manganese and hydrogen sulfide. 1.

FIELD WORK

In June 1975, well logs were located, and preliminary samples analyzed in the field for alkalinity, hardness and chloride. In July 1975, 38 samples were collected for complete chemical analysis. Surficial mapping was carried out, using exposures in road cuts, ditches, and stream banks.

Due to high fluoride and chloride values in some of the first 38 samples, the following work was carried out in September 1975: 1) 29 wells were resampled for fluoride, 2) 18 additional samples were taken for complete chemical analysis, and 3) 14 samples were taken for isotope analyses. The latter analyses, for tritium and deuterium, were run by Dr.R.M.Brown of Atomic Energy of Canada Ltd., Chalk River, Ontario.

The locations of the wells and chemical analyses are shown in figures 2 and 3. The well data and field chemical data is summarized in Appendix 1. Lab chemical analyses are summarized in Appendix 2.

In October and December 1975, 31 backhoe testpits and 2 drilled testholes were logged in the area (Figure 3 and Appendices 3 and 4).

LOCATION AND PHYSIOGRAPHY

The Plymouth area is located on the east side of the East River near Stellarton (Figure 1) and lies in the Carboniferous Lowlands region of Nova Scotia. Land elevations in the study area range from sea level to 300 feet. The study area lies within the drainage basin of the East River.

CLIMATE

Based on 20 years of record, the average total precipitation is 40.70" annually, with 32.96" as rain and 77.40" as snow. The maximum precipitation was 55.32" (1964), the minimum was 26.69" (1965). Total runoff accounts for about 2/3 of the precipitation.

The mean annual daily temperature is 43.4° F, with a mean daily maximum of 52.3° F.

The average number of frost free days is 112, with a range of 89 to 135 days. The average length of the growing season is 135 days.

GEOLOGY

Bedrock (Figure 4)

The northern part of the study area is underlain by gray, red and mottled shale, sandstone and conglomerate, and minor coal of the Stellarton Series of Pennsylvanian age.

Exposures along the East River in the Plymouth area consist of alternating hard red sandstone, gray siltstone, and shale. The bedding strikes northwest-southeast and dips northeast at 13 to 25°. Major joint sets strike parallel to the bedding and dip northeast and southwest, generally at an angle greater than 50°. There is also a prominent set striking perpendicular to the bedding and dipping from 65 to 90°.

In the southern part of the area (near Ferrona Junction), there is hard red and gray sandstone of the Windsor Group of Mississippian age. The bedding strikes almost north-south and dips about 50° west. There is a faulted contact with limestone just south of this area.

The main structural elements in the area are the Plymouth and South Faults, and a northeast striking anticline axis. Two small faults parallel the Plymouth Fault.

Elevations of the bedrock surface from well log data (Figure 5) indicate a steep dropoff in a westerly direction towards the East River. In the Park, the bedrock elevation is about 25 feet below sea level.

The following description, from the southern to northern part of Figure 4, is summarized from Bell (1940) and Fletcher (1892).

Windsor material outcrops upstream of the South Fault, consisting of reddish, flinty, slaty or prismatic sandstones and argillites with veins of quartz and ankerite. A diorite dyke cuts across the Windsor in this section. This sequence is succeeded upstream by blue-grey limestone. One outcrop of Windsor material, just east of the Plymouth-Churchville Road, consists of jointed sandstone with quartz crystals coating the faces. Conglomerate occurs on Mac Gregors Mountain and in the Churchville area.

The South Fault, trending N75E, separates Windsor and Canso strata. The Stellarton Series are downthrown several thousand feet against the older rocks in the area east of the East River.

The Canso-Pictou strata contact on the East River north of McKay Brook is marked by a thin basal gray conglomerate of the Skinner Brook Member, which lies unconformably on brownish-red sandstone of the Canso Group. The basal conglomerate is overlain by brownish red sandstone, then gray, flaggy, rippled 3.

sandstone to 420' above the contact, then 15' of blackish grey and brown mudstone and grey argillaceous shale. This sequence, representing 4800 feet downstream from McKay Brook, strikes essentially parallel to the river and dips eastward. The rocks then swing into an anticline. The higher beds consist of brownish-red sandstone and siltstone and a thin red conglomerate. The rocks are then concealed for 1600 feet, in which the Plymouth Fault occurs (downthrown on the north side). This fault accounts for the loss of several thousand feet of strata belonging to Division 1 of the Stellarton Series. There is also a minor fault 500 feet south of this, trending S76E and with a downthrow on the northern side. 4.

Between the pumping station and Plymouth Bridge, 520 feet of the Plymouth Member is exposed – a brownish red siltstone and fine argillaceous sandstone, some gray mottled. In the coarser beds, green slate or argillite from Ordovician rocks is present. The lower part of this section to the bridge contains a few bands of blackish-gray slickensided mudstone. A small fault at the bridge strikes S65E, with a downthrow on the north side. North of the fault are exposed brownish red and mottled red and gray siltstone overlain by gray argillaceous siltstone and a thin calcareous bed.

Surficial (Figure 6)

The surficial deposits consist mainly of sandy and clayey glacial tills, and sands and gravels. The visible thicknesses in the field are indicated in Figure 6. The thicknesses from well logs are shown in Figure 7. Generally, the till thicknesses exceed 10 feet, and reach almost 100 feet in several places. Dept. of Highways boreholes (Appendix 5) and observations of outcrops in the East River (Figure 6) indicate that the stratified sands and gravels along the river are generally less than 10 feet thick.

Thirty-one backhoe testpits were dug to determine the type and thickness of surficial materials. The locations of these holes are shown on Figure 3, and summaries of the logs in Appendix 4.

Glacial History

Work in the Northumberland Strait by Kranck (1972) has shown that preglacial drainage off the East River trends northeast along Cape George. After deglaciation, sea level was lowered by 300 feet. The Strait was inundated at about 11,800 B.P. Off the East River, there are two terrances, at 45-55 meters to the northeast, and 18-23 meters to the north. The terraces were formed during the last postglacial transgression of the sea. The shallowest (youngest) terrace has been dated at 5000-5500 years B.P. The present average rise in sea level in this area is more than 25 centimeters/100 years. Hence in the East River area, sea level has risen gradually from the Pleistocene to the present and there should be no residual saline groundwater due to higher sea levels from this time period.

GROUNDWATER FLOW

The water table elevation in the Park (Figure 8) indicates a northwesterly flow of groundwater in the surficial material towards the East River. The regional contours (Figure 9) also indicate a general northwesterly flow in the bedrock, following the bedrock and surface topography. The main recharge area is MacGragor Mountain, the main discharge area the East River. A local recharge area (piezometric elevation 55') occurs just east of the Park, with a discharge area to the southeast and northwest. A local discharge area also occurs along the old River Road.

The water levels in dug wells are generally higher than those in adjacent drilled wells where information is available, indicating a vertical component of flow from the surficial materials to the bedrock.

Evidence of groundwater discharge is also provided in the many seepages (Figure 6). Some of these, especially those in the Ferrona Junction area, were flowing at 1/2 to 1 gpm. The seepages marked on Figure 6 were present after about 1 1/2 months of no rain and hence should represent perennial discharge. Unfortunately the iron concentrations were high enough to cause a bright orange precipitate of iron oxide or hydroxide and hence these springs would not be suitable for a domestic water supply.

Wells with high yields, i.e. greater than 5 gpm, appear to be related to faults and to Windsor Group materials (Figure 4). Several wells in Windsor conglomerate yield 10-40 gpm.

Water level fluctuations in the two N.S.D.O.E. test holes were monitored monthly from January to July 1976 (Figure 20). If it is assumed that the two wells are analogous to piezometers, then the results suggest that the interval area of the river is a groundwater discharge area during most of the year when water levels are relatively high, but converts to a recharge area during the groundwater recession in summer. Further monitoring is required to substantiate this.

GROUNDWATER QUALITY

The field results and complete chemical analyses (Appendices 1 and 2) indicate a fairly serious problem in the area, with respect to chloride, iron, manganese and fluoride (Table 1).

TABLE 1

Field data:

Cl>50mg/1	37/118	31.4%
Cl>250mg/I	12/118	10.2%
Reported sulphi	4.2%	
Hardness>120 n	ng/l 40/118	34.0%

Complete Analyses:	DUG WELLS		DRILLED WELLS		TOTAL	
	No.	%	No.	%	No. %	
CI > 250 mg/I	3/17	17.6	11/40	27.5	14/57 24.6	
Fe > 0.3 mg/l	5/17	29.4	13/40	32.5	18/57 31.6	
Mn > 0.05 mg/l	11/17	64.7	25/40	62.5	36/57 63.2	
F > 1.2 mg/l	0	0	16/40	40.0	16/57 28.1	

Salt

The values of chloride are shown in Figures 12 and 13. There is essentially no relationship between CI and well depth (Figure 10); however, it is noteworthy that all drilled wells (except the two circled) with greater than 100 mg/l CI are from the localized area of the Park. The well waters have also undergone a considerable amount of ion exchange and natural water softening, as indicated by Figure 11. A trilinear plot (Figure 18) indicates that most drilled well waters in the study area are of the Na-HCO₃ or Na-CI type. Most drilled wells in the Park area contain Na-CI type waters. 7.

The natural softening of water usually occurs in shales and other sediments originally laid down under marine conditions or affected by marine incursion after deposition. At this time, a large number of Na ions are adsorbed on ion exchange sites. When fresh water recharge occurs, generally with Ca-rich waters, the Ca is preferentially adsorbed and the Na is released, resulting in high Na/Cl and Na/Ca ratios. The drilled wells outside the park show this relationship (Figure 11). The drilled wells in the Park show high Na/Ca ratios, but low Na/CI ratios due to the Na and CI, respectively, contributed from salt (NaCl). Some possible reasons for this are: 1) regional groundwater discharge; 2) the bedrock surface here forms a depression and may contain residual or incompletely flushed saline brines; 3) the Plymouth Fault to the south and the small fault to the north of the Park may have acted as barriers to groundwater flow and caused entrapment of meteoric waters in a stagnant condition; 4) incomplete flushing of original saline pore water. The latter is unlikely in view of the isotope results to be discussed later. The most reasonable explanation is slow flushing due to the large number of shale beds, some of which are reported as sticky and clay-like; such beds may act as barriers and also as membranes.

One well high in sulphate (index no. 65) is likely affected by gypsum of the Windsor Group.

Most dug wells are of the $Ca-HCO_3$ or Ca-Cl type. High values of chloride in these wells appear to be related to road salt.

8.

Fluoride

Fluoride values were found to exceed the suggested limit of 1.2 mg/l in sixteen wells.

Origin

The main possible sources of Fluoride are: 1) from sea water during the original deposition of a marine bed which has not been completely flushed out, 2) volcanic emanations, 3) weathering or solution of fluoride-bearing minerals such as fluorite, apatite, tourmaline, topaz, vesuvianite, lepidolite, phlogopite, and glauconite (LaMoreaux, 1948).

Fluoride levels up to 3.4 mg/l have been found in Alabama (LaMoreaux, 1948 and Carlston, 1942) to have the following relationships: 1) fluoride more than 1 mg/l found exclusively in deep wells, 2) high fluoride is found in soft groundwaters (less than 60 mg/l total hardness) high in HCO₃. A direct correlation exists between fluoride and HCO₃, 3) high fluoride is correlated with phosphatic material, pyrite, lignite and abundant glauconite. Pyrite in association with organic material could be expected to decompose and produce H_2SO_4 , which in turn could attack the more insoluble fluoridebearing minerals (LaMoreaux, 1948). Glauconite alone was not found to produce high fluoride levels, but was the chief base exchange agent causing natural water softening; 4) high fluoride was found in deeper wells in discharge areas, hence the fluoride concentration may be related to depth of formation and distance to outcrop, and hence to the extent of groundwater circulation and length of contact time. In Florida, Toler (1967) found apatite group minerals in phosphatic sediments to produce groundwaters high in fluoride.

Handa (1975) found that well waters high in fluoride were: 1) associated with low Ca, which he attributed to the low solubility of fluorite, 2) associated with high HCO_3 and sometimes NO_3 , 3) often saturated with respect to calcite and fluorite.

In the Plymouth study area, high fluoride values were found to be associated with: 1) deeper wells (Figure 14), 2) high chloride (Figure 15), 3) high HCO₃ (Figure 16) and soft waters, 4) often higher values of NO3 and PO₄ than wells with lower fluoride values (Appendix 2), and 5) a groundwater discharge area, possibly regional. Three wells were found to be saturated with respect to fluorite (Figure 17), and most were also found to be saturated with calcite and fluorapatite (as computed by program WATEQF). This supports a primary mineral source for the fluoride. Also, the strong positive correlation between fluoride and hydroxyl concentrations and pH indicates that fluoride is not simply exchanging for hydroxyl on clay mineral sites.

Most dug wells in the study area contained less than 0.5 mg/l fluoride, as found by Handa (1975), due either to absence of fluoride-bearing minerals in the overburden or rapid groundwater circulation.

The fluoride source in the Plymouth area could possibly be correlated with pyrite and lignite, since coal seams and coal shale are common. Unfortunately no cores were available to check for phosphatic or tuffaceous layers in the

bedrock. The latter occurrence is a possibility, since high fluoride values in the Moncton area are thought to be associated with a volcanic ash unit in the Pictou Group which has been identified in a few deep wells (Dyck et al, 1976). The natural water softening could be a result of natural base exchange, as explained earlier, or a shale membrane mechanism. The latter works on a reverse osmosis principle, whereby shales or clay layers act as sieves or membranes, with a driving force provided by hydrodynamic or permeability gradients. According to White (1965) and vanEverdingen (1968), the low pressure side of the membrane generally has a higher Na/Ca ratio, higher fluoride, pH > 7, and low Cl as compared to the high pressure or input side. This hypothesis fits the chemistry of the high fluoride waters in the study area with the exception of the high Cl values (Figure 15), which may be the result of such factors as stagnation in bedrock depressions, proximity to Windsor bedrock and proximity to fault zones. As shown by Figure 19, the driving force could be a combination of regional hydroynamic pressure and permeability gradients produced by alternating shales and sandstone. Figure 19 also suggests the presence of an old channel deposit of the East River in the vicinity of well 45 this may contain materials of high permeability and hence create a low fluid pressure area.

To ensure that entrapped sea water from pre-Pleistocene times or recent salt water intrusion was not causing the salt, Dr. R.M.Brown kindly carried out tritium and deuterium analyses on selected samples. The results (Appendix 7) indicate that all wells deeper than 75 feet contain water more than 20 years old. This supports the idea of stagnant groundwater associated with a regional 11.

flow system, or incomplete flushing of saline water associated with nearby Windsor rocks or faults. The possibility of a bedrock knoll (Figure 19) as suggested from water well logs could account for the stagnation and membrane filtration effects; however, depth to bedrock from the well log data is not conclusive because of the soft shales present, which make it difficult in some cases to ascertain the bedrock-overburden contact.

Health Implications

Fluoride values in municipal water supplies in Nova Scotia are maintained at about 1.2 mg/l, the amount theoretically required for strong teeth in children. Excessive amounts of fluoride may cause mottling of tooth enamel and may have toxic effects on the bone structure of the body. The use of such water generally affects children less than 8 years old whose permanent teeth have not yet formed. The mottling is a permanent effect.

As a followup to our sampling, N.S.Dept. of Public Health resampled wells with more than 1.2 mg/l fluoride. The values agreed with the previous sampling to within 0.2 mg/l. A dental survey was then carried out, but fortunately no serious fluorosis problems were found as a result of fluoride in the well water (Appendix 8).

Economic Implications

Dyck et al (1976) found that a band of high values of fluoride, uranium, helium, radon, alkalinity and conductivity exists along the Northumberland Strait from the New Glasgow area, N.S. to Cape Tormentine, N.B. in the Pictou Group bedrock. They suggest that this may be analogous to a "roll front", of the type that has produced economic uranium ore deposits in the United States. Circulating groundwaters are presently leaching the deposits. A uranium anomaly has been found in the Plymouth area (G.S.C.Open File 340), possibly due to stagnation of groundwater in this area.

TESTHOLE RESULTS

Surficial

Backhoe testpits were dug to determine the type of surficial materials, and if there were any sand and gravel deposits suitable for a screened well or infiltration gallery along the East River. Appendix 4 summarizes the logs.

The pits indicated a fairly consistent pattern from top to bottom of silt or till, stratified sand, gravel and boulders, and clay or bedrock. The top sands and silts in many cases represent recent alluvium deposited on the flood plain of the East River. The stratified materials are generally only 2 to 5 feet thick except at P12, which is at a higher elevation. The sands and gravels on the interval area are likely a central bar deposit, built up due to change in river slope just upstream and to rising sea level. Above the 20 foot contour, the slope is about 15°, but increases to 20° between 20 and 10 feet due to bedrock control. From 10 to 5 feet, the slope decreases to 12°, resulting in a critical slope on the border between meandering and braiding. The meander length-channel width relationship indicates a disequilibrium, with increase in channel width or decrease in meander length being desirable. The small gravel terrace in the vicinity of P12 is likely an outwash remnant. 13.

The lower clay layer is of two types: 1) a hard compact clay containing angular gravel and a few rounded pebbles, and 2) a soft plastic clay with minor thin laminae of silt and fine sand, and containing minor organic material. The former is likely a glacial till, while the latter likely represents a quiet depositional gene environment that might exist in an old cutoff channel or swale on the flood plain.

The sand and gravel in several of the pits contained appreciable quantities of groundwater; however, this only occurred just near the gravel-clay contact and represents perched water. The saturated thickness was less than 1 foot, and the sand and gravel would likely not be saturated on a perennial basis.

Bedrock

Logs of the two N.S.D.O.E. and the N.S.D.M. holes on the interval are contained in Appendix 3. The location of the N.S.D.M. hole is not certain but it is thought to be from 200-400 feet north of INT-1-75. The depths to bedrock in the three holes are 70, 39 and 24 feet. The sand and gravel may be saturated in the lower 5 feet for most of the year, however the groundwater is perched on clay and gravelly clay, hence there is no apparent extensive buried channel network. The yields of the two N.S.D.O.E. holes were 5-8 gpm and 1-2 gpm from the section of the hole below 20 feet. The quality of this water is poor (Appendix 2), with high values of salt, iron and manganese. It is possible that a shallow drilled well screened from 15-25 feet could supply more than one home; however, the yield would likely not be sufficient to serve the needs of the Park area.

CONCLUSIONS

The results of the study indicate a fairly serious problem of water quality in drilled wells in the Park area and the area east of the Park to the Churchville Road. Many dug wells in the Park either have problems of surface water contamination, as indicated by salt, or experience water shortages in summer.

The main problems of salt and fluoride in the drilled wells are likely due to slow flushing or stagnation of meteoric water. The iron, manganese, and hydrogen sulphide problems are likely related to coal and other organic matter in the subsurface.

Test hole results indicate that the sands and gravels in the area are generally too thin or the saturated thickness insufficient to provide an alternate water supply for the area. The groundwater is perched somewhat by the underlying clay, and hence drains rapidly, i.e. storage is small. The potential for high capacity bedrock wells could exist southeast of the Park area in association with faults and Windsor conglomerate. The water quality from these wells is generally good also, although slightly excessive iron and manganese values may occur.

RECOMMENDATIONS

We would recommend that an alternate water supply be obtained for the area of the Park and east of it to the Churchville Road. About 50-60 homes are involved. We would suggest the following options:

serve the area from either the New Glasgow or Stellarton systems
consider a well field in the bedrock in the MacGregor Mountain area. This

option would involve a test drilling and pump testing program. If groundwater of sufficient quantity and acceptable quality were obtained, then a pipeline of at least a mile would be involved.

In both cases, water and sewer lines would have to be installed.

From an academic viewpoint, there are interesting projects which could stem from this work, such as:

 a detailed analysis of some of the well waters in the Park area for uranium.
The Geological Survey of Canada sampling for uranium suggests an anomaly in the Plymouth area.

2) diamond drilling to obtain cores for petrologic study, to determine the overall mineral composition, and the minerals providing the fluoride source and base exchange mechanism .

3) coring might help to establish if any fault zones are present at depth through which mineralized groundwaters from the Windsor Group could enter the Pictou Group rocks in the area.

4) installation of piezometer nests to determine accurately the regional groundwater flow pattern.

BIBLIOGRAPHY

- Bell, W.A., 1940, The Pictou coalfield, Nova Scotia: Can. Geol. Survey, Memoir 222.
- Carlston, C.W., 1942, Fluoride in the groundwater of the Cretaceous area of Alabama: Geol. Surv. Alabama, Bull. 52.
- Dyck, W., Chatterjee, A.K., Gemmell, D.E. and Murricane, K., 1976, Well water trace element reconnaissance, Eastern Maritime Canada, presented at the regional meeting of the Association of Exploration Geochemists, Fredericton, N.B., April 1976.
- Fletcher, H., 1892, Report on geological surveys and explorations in the counties of Pictou and Colchester, N.S.: Can.Geol.Surv. Ann.Rept., vol.V, pt.P, 193p.
- Handa, B.K., 1975, Geochemistry and genesis of fluoride-containing ground waters in India: Ground Water, vol. 13, no. 3, May-June.
- Hem, J.D., 1970, Study and interpretation of the chemical characteristics of natural waters: U.S.Geol. Surv. Water Supply Paper 1473.
- Kranck, K., 1972, Geomorphological development and post-Pleistocene sea level changes, Northumberland Strait, Maritime Provinces: Can. J.Earth Sci., vol.9, no.7, July, pp.835–844.
- LaMoreaux, P.E., 1948, Fluoride in the ground water of the Tertiary area of Alabama: Geol. Surv. Alabama Bull. 59.
- Toler, L.G., 1967, Flupride in water in the Alafia and Peace River Basins, Florida: Fla. Geol. Surv. Rept. of Invest.46.
- Unesco, 1975, Studies and reports in hydrology no.7 Ground water studies, Chapt.10 - Nuclear techniques in ground water hydrology.
- Van Everdingen, R.O., 1968, Mobility of main ion species in reverse osmosis and the modification of subsurface brines: Can.J. Earth Sci., vol. 5, p. 1253.
- White, D.E., 1965, Saline waters of sedimentary rocks, in Amer. Assoc. of Petroleum Geologists Memoir 4 – Fluids in subsurface environments, pp. 342–366.

FIGURES



CONTOUR INTERVAL 50 FEET Elevations in Feet above Mean Sea Level ÉQUIDISTANCE DES COURBES 50 PIEDS Élévations en pieds au-dessus du niveau moyen de la mer

Figure 1. Location map.



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Figure 2. Sample locations, Park area.



TABLE OF FORMATIONS TO ACCOMPANY FIGURE 4

CARBONIFEROUS PENNSYLVANIAN

9

8

7

6

STELLARTON SERIES

Grey, red and mottled shale and sandstone, conglomerate, coal seams

CUMBERLAND SERIES

Brownish-red sandstone and shale, grey sandstone, red and grey conglomerate, 8a, New Glasgow Formation: conglomerate

CANSO SERIES

Brownish-red sandstone and shale, grey sandstone and shale, limestone conglomerate

MISSISSIPPIAN

WINDSOR SERIES

Red shale, sandstone, conglomerate, limestone, gypsum; 6a, basic lava

SILURIAN

ARISAIG SERIES

5

Grey shale and sandstone, calcareous shale and sandstone











Figure 8. Water table elevations, Park area.





Figure 10. Chloride as related to well depth.




Figure 12. Chloride values, Park area.

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Figure 14. Fluoride as related to well depth.





Figure 16. Fluoride as related to alkalinity.





Figure 18. Trilinear plot of groundwater chemical composition.



Figure 19. Cross section A-B.



APPENDICES

0 611517177	REPORTED QUALITY PROBLEMS	ry occasionally		oter hard		alt and Iron tuste			ulfur odor, salt, iran, sediment and artasian	p sample due to heavy cover. Bored eff on property not used due to iron oblems.		ossible surface runoff from neighbour's nk drain	ssible surface runaf and ail contamin- lian.	acuted 20 ft. and 1 ft. downstope from	rilted by Dept . of Highways since dug ell had road salt. Dritled well has sulfur dat.			delf in basement	ocated 4 ft. from and level with road.	ocoted in besement and used for drinking.		
	CONSTRUCTION	Crocked, unsealed, no apron, D	Wooden cover	Crocked, unsealed, no apron	Crecked to 1.1 ft. above ground, no aprov		Cracked to 0.75 ft. above ground, iren cover	Grocked to 3 feet above ground			Crocked to 1.9 ft.above ground, coment apran	<u> </u>	Crocked Located 15 ft. from 22 and 1-2 ft.below road level. at	Crocked to ground level	<u> </u>	Crocked to 1.3 ft. above ground, no apron	Well later reamed out and gravel packed from 122-260 fr. Flow reduced to 1 1/2 gpm.	~~~~	Crocked to 0.3 ft. abave ground L		Crocked to ground level	Crocked to 2.0 ft. abave base- ment level
	Temper rature *F					88		8				68			5	49			43		58	
LYSES	Total hardness mg/1 as CoCO3	511	3	40	20	-13	6	69	0	S S	50	300	80	100	0	80	\$	180	157	130	77	340
FIELD ANA	Chloride mg/l	3	35	35	12	1120	95	115	571	4 10	25	240	35	\$\$	246	22	740	2	42	0	24	165
	Alkoimity mg/1 as CoCO3	85	Q.	15	ŝ	192	12	0	8	9	8	4 8	22	8	483	8	585	175	001	105	128	1 20
	GEOLOGIC LOG					Bedrack conglomerate, soft at finish					0-26 sand, clay, gravel & lorge boulders						0-85 mixed clay and gravel 83-260 soft conglamerate with bands of red shale	-				
REPOR-	TED YIELD GPM					1.5-2											3.5					
WATER	LEVEL FEET BELOW GROUND	5,6		6.9	7.6	10.0	6.9	5.9			7.75		4.7	8.75		7.25	4 0,	3,4	11.3	4.0	11.0	****
	DIAM- ETER	2,5		1.5	2.0		1.75	2.5			2.75		2.3	2.0	4	5.0		2.5	2.0	2.0	2.0	3.0
	CASING LENGTH FEET					20.3							-				8					
	WELL DEPTH FEET	9.25		10.5	11.2	147	9.7	8.75		12-14	26		0	12.5	213	6.61	260	8.2	21.3	\$	22.5	٥. ²
	TYPE OF WELL	Dug	Drilled	Dug	520	Dulled	5~0	Dug	Drilled	6nQ	6n Q	Spring	б ^л О	Drig	Orilled	Dug	Dilled	Dug	0ng	0 ng	Dug	540
	OWNER	David McKay	William Malloy	Albert McKay	Helen McKenzie	C.Urghort	C. Urqhart	Allan McKay	Roy MacQuarrie	Russell Henderson	Henry Heighton	R.Cunningham	Roland Norin	Elaine Rhyno	John Cillis	John Gillis	Gardon Fraver	Gardon Frater	Debruyn	G. Froser	Scott McDanald	Mrs. Glen
		T																				

Appendix

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COMMENTS A	REFORTED CUALITY PROBLEMS	Dry occasionally				Sediment	Top sample.		•••••••••••••••••••••••••••••••••••••••		Not used because of adour and taste			Abundant water supply	Dry in summer	Dry in summer	Kust, odour	Dry accasionally	Dry occasionaily	40 ft. from and level with road - possible saft contamination		Sulfur adar, mineral taste	
-	CONSTRUCTION	In basement						Extends 0.75 H. above ground, wooden cover	Drilled through an old 3 ft. diameter dug viell	Cracked to 1.5 fb. above ground wooden cover	Crecked, no opron, 3 ft. down- slope from road	Clocked to 0.75 ft. above ground, no apron,steet cover		Top 2.7 ft. above ground		Crocked to 0.9 ft, above ground, no apron, tin cover	Crocked to 1.6 ft. above ground no opron	Top 1.5 ft. above ground. Well grovel-packed		Cracked to 2.5 ft, abave graund, no upron	Top 0.6 ft. obove ground		
	Tempe- roture e E			8	26	58	67		•	8	28	\$	56	8	8	49	ន	8	56	25	23	28	\$\$
SES	Total rdness ng/1 as aCO3	8	0	œ	\$	ŝ	56	g	8	25	8	8	53	0	R	55	8	5	Q	N.	8	0	S2
ANALY	1/1 ho	2	25	12	25	78	65 31	01 01	10	5. 57	83	<u>.</u>	35	9	7.5	27.5	01	10 21	35	5 23	25 10	53	8
FIELD	2 HO	-		-			~~~~				<u>ب</u> م		ίΩ							¥		ei 	ž
	Alkolinity mg/1 as CoCO3	40	125	485	357	393	120	8	021	8	132	15	360	10	õ	20	8	200	150	153	8	220	584
	CEOLOGIC LOG		-		Grovel , then bands of conglome - ate , shale , and red sandstone	0–60 clay, 60–90 fine sand Bedrock – fine grained siltstane								Encountered sand & gravel when Atomian	Bur SS m			-					0-50 mud & sond, 50-90 mud, send & red shale, 100-175 red shale
REPOR-	YIELD GPM				ę																		5
WATER	FEET BELOW	4.7	MO		ę			8'8		8.7	2.5	6.7		2.0	9.7	9.11	ч თ	5	2.9	7.7	é.5	400-00 ve	46
	UAM- ETER	2.5	3.0	; *	: *1			2.0	÷	2.6	1.75	1.75		2.0	2.0	2.0	1.549	1.5	.5	1.75	2.0		ż
C A CINIC	FEET		····		60	8								19997- "L- B	****		na an a			*			8
WELL	PEET	7.7	24	66	143	150		19.7	24	14.9	3.75	10.75	8	12.3	14.9	16.93	15.25	16.25	7.5	14.2	13.75	128-140	175
TVDC	WELL	Dug	Dug	Drilled	Drilled	Drilled	Dug	Dug	Dulled	Dug	Dug	0 ng	Drilled	ნიმ	Dug	6nd	Sng	Dug	Dug	5ng	ნიქ	Drilled	Drilled
	OWNER	Hugh Pussell	J.Robertson	Raymond McKay	C.V.Ranscar	A.McMillon	A.McMillan	L.Urquhari	T. Stroud	E.Kellock	E. Kullock	E. Cariter on	G. Naugler	B. Taylor	J. Duncan	L. Dunber	W. Clark	8, Allen	V. Taylar	H. Convey	J. Taylar	S. Stewart	R. Fcote
	NO.	22.	23.	24.	23.	26.	27.	28.	28	Q		32.	33.	34.	35.	35	à	Ŗ	39.	ę	41.	42.	. .

Appendix 1 (continued).

	COMMENTS B	REPORTED QUALITY PROBLEMS		Gossy	Fillad with town water — 1 week before sompting.			Previous analysis, Jan.12/72: hard 165 mg/1, aik 150, Fe 0.5, C1 20, SO30, NOT-N 3, pH 7,8		Dry in summer.			Water softener installed.		Well overflows in spring.	Two old diilled wells exist = 35 6-385 ft. hit sait water.			1971 onalysix hard 176 mg/l, alk. 175 mg/l, Fe 0.11, CI 27,504 7, NO ₃ N 5.6, pH 7.7	
		CONSTRUCTION			Crocked to 2 ft. above ground	Crocked to 2.3 ft. above ground	Crocked to 6.5 ft, above ground			Rocked to ground level, wooden cover				3-4 tile crocks with cover, in batement	Galvanized crock to 4 feet above ground	Crocked to 0.5 ft, abave ground, wooden cover	Covered with cement then sod . Considerable gravel around well	Crocked to 1.7 ft. above base- ment flace.		Crocked to 0.4 ft, above ground,
		Tempe- rature	8	28		52	48	ŝ	62	49	62	S	62	63				54		53
	ALTOES	herdness mg/L as CoCO3	8	138	8	130	08	8	6.3	15	92.1	150	1	120	S	ç	8	35	145	68
	LICEU AN	Chloride mg/l	2002	2670	(r)	7.5	15	¥	8 0	7.5	7.5	ŝ	2	7.5	7.5	0	ŝ	12.5	5	17.5
		Aikolinity mg/1 as CaCO3	628	465	20	130	20	212	303	20	165	170	225	100	30	52	8	S	130	50
		ecoroeic roe	0-8 ovbn,8-16 gravei, 16-45 soft red sh, 45-62 block coal sh, 67- 85 soft red sh, 85-102 soft grey sh, 102-158 red sh	0-108 cloy & gravel, 108-120 red sh, 160-200 gray sh, 200-240 red sh					0-105 gravel & bidrs, 105-194 red ss, 194-245 gray sh, 245-217 red sh		0-18 mud & bidrs, 18-123 red shale	0-54 ovbn, 54-120 haid red 35 120-130 gray 35,130-160 red 35	0-30 ovbn, 30-70 mud, bidts, grave 70-90 red sh, 90-135 red ss		Clay and same shale		Red clay		0-12 clay, tand, bldrs. Gravel vein with water at 12 feet.	
2000	TED	VIELD GPM	2	ç					-		ŝ		th						****	
WATER	LEVEL	BELOW	ŝ	8		5.0	0.11 11.0		8	10.0	e	35	.		7.0			0.9	4.9	0.7
	DIAM-	ETER	- 	*9 67	2.5	1.75	2.0	÷o	ţ.	2.0	ŝ	ŝ	*		2.5	2.0	5.0	1.2		0.9
	CASING	FEET	105	6				001	107		5	5	72							
	WELL	FEET	158	240	٦٨	\$ 1	19.5	247	247	13.6	123	160	135	12	50	4	ž.	10.75	16.25	14.6
	TYPE	WELL	Driffed	Driffed	ნიმ	Dug	0n0	Palling	Drilled	Dvg	Drilled	Dilled	Dilled	⁵ O	640	âng	3	6ng	5n Q	Dug
	OWNED		R. Rochk	J. Wadden	J. Derroch	J.McDoneld	W.Frater	G . Atwater	R. Polson	A. Ross	M. Conway	R. MocDonald	A. Welr	L. Rogers	C. Ramtcar	8. Nelson	G. Adamson	s. Young	H. Doucette	J. Stawort
	INDEX	NO.	4	4) म	4¢.	47.	48,	49,	S	5	52.	53.	х.	55.	ş		3 3	\$.	·09	41.

Appendix 1 (continued).

	REPORTED QUALITY PROBLEMS								-	Supplies approximately 13 trailers (Hemlack Trailer Court).							Nat used for drinking.							Presently using a 300 foot drilled well.	
	CONSTRUCTION	Spring		One cement crock to 0.9 ft. above ground, 1.0 ft. below		Cracked to 0.4 ft. abeve ground, wooden cover		Level with ground	·			Crocked to 4.7 ft. phove ground				-		5 crocks on bed of brook	Crocked ta 2.3 ft. above base- ment floor.	Drilled 16 ft, through a 20 ft, dug well in the basement		Recked to ground, woodsn caver, Lacated behind barn.			Gracked, iran caver
	Tempe- rature ° F	3	ţş	55	52	52	56	53	55	58	56	53	63	56	59				3	83	63	52	ŝ	5	55
YSES	Total Ing/1 as CaCO3	20	135	125	478	140	95	120	011	145	140	35	30	8	120	135	140	115	00	05	59	4¢,	\$	8	8
TELO ANA	Chloride mg/i	7.5	ŝ	50	20		ŝ	7.5	10	15	c,	7.5	0	ŝ	0064	15	20	40	25	14.5	62	25	33	01	27.5
	Alkatin'ty mg/1 as CaCO3	8	165	ŝŝ	139	5	991	110	22	00	8	80	01	8	300	8	8	105	100	200	\$	252	235	ş	8
	SEOLOGIC LOG								0-9 overburden, 9-84 red limestone				0-11 mud,11-139 red & gray shale, 139-149 green shale, 149-155 red shale, 155-168 green shale, 168- 183 red shale	0-7 mud & boulders, 7-148 red shale			-	Fine grained sand near bottom							
REPOR-	TED VIELD GPM								2				7	n											
WATER	FEET BELOWIC			8.25		9.2			12			8.3	0	10		م نسبون			¢.0			12.0		4.8	5.3
	DIAM- ETER			2.0		2.0			*			2.5	ю.	ŝ					2.0			5.5		~	2.5
	FEET								16				36	51											
1	DEPTH FEET	s	123	11.5		20.1			84		8	9.6	183	148	2100	25		15	-	36		25	78	14.4	10
1	WELL	Bnd	Drilled	6° 0	Driffed	ტოვ	Dilled	Dug	Drilled	Dailled	Drilled	Brid	Dailled	Drilled	Drilled	Dug	Dug	Dug	5nd	Drilled	Dug	brig	Drilled	Dug	Dug
	OWNER	R. Jackson	J.C'Haggen	G. Correcon	M. Williams	F. Machnesh	W. Murphy	W. Murphy	L.Delmatte	H.Sutherland	A. Boudaux	J.MacKay	f .MacDonald	G.Vickers	C , Poulain	C.Poulain	E.Kellock	6.61lh	D.Gould	W.J.Conway	D . Anderson	A.J.Post	G. Blampson	Plymouth School	S .MacFarlane
	NO.	62.	63.	3	65.	66.	67.	68.	64.	70,	.17	72.	C	74.	75.	76.	77.	78.	74.	80°		82.	33.		34,

Appendix 1 (continued)

COMMENTS B	REPORTED OUALITY PROBLEMS		Dry in summer.		Supplies two houses.				8 fs. below road - pasible salt problem in winter.					Sulfur odaur.		Supplies three houses and still averflows at appraximately 2 gpm into the ditch.			Supplies two familles					
	CONSTRUCTION	Crocked to 1.6 ft above ground						3-4 crocks to 3 ft, above ground, gravel pocked	Four - 2 1/2 (t. crocks to 1.6 ft. sbove ground, wooden cover	Two dug wells connected.			Crocked to 1.7 ft. above ground	Cracked to 0.9 ft. above ground									Calvanizad crock ta 1.211. above pround, gravel pocked.	Crocked to 1.75 ft. above basemen
	Temper rature • E	55	3	20	8	56	8	85 5	35	8	62	ĸ	43		59	24	67	23	54	85	23	56		
LYSES	Total hardness mg/1 as CaCO3	001	40	264	130	100	133	8	çi Q	8	62	130	103	081	120	86	06	8	60	159	485	8	124	130
FIELD ANA	Chloride mg/l	01	2	11	52.5	ŝ	¢	0	8	ŝ	10	10	8	7.5	7.5	ŝ	7.5	0	Ś		188	0	88	65
	Alkalinity mg/Las CaCO3	20	9	261	08	120	138	22)	¢,	8	\$	8	145	8	170	8	051	140	120	326	75	8	8	100
	פבטרספוכ רספ				0-35 overburden, 35-70 red shale	0-25 mud & Boulders, 25-50 braken rock, 50-90 soft red shale, 90- 123 hard red shale						0-98 red conglamerate				0-50 mud & boulders, 50-130 red shale	0-72 much & boulders, 72-147 red conglomerate	0-25 clay & boulders, 25-118 conglomerate	0-10 clay, 10-120 red shafe	0-50 mud & boulders, 50-245 red shale	0-55 clay & baulders, 55-145 congtomerate	0-32 mud & boulders, 32-147 congtomerate		
REPOR-	TED YIELD GPM				Ś	~						5				Q 4	12		ŝ	m	n	с. С.		
WATER F	REET BELOW	6.5	4.0		•	5		Cverflow	3.4 7	1.2	Overflow	Overflow	7	11.5		Overflow	\$	8	35	8	22	50	7.0	6.1
	DIAM- ETER	2.0	2.5	3.0	<u>व</u>	• •			2.0	2.0		÷.	2.0	1.75			*9		7. 12	Ş.	· ·	:0	2.5	1.7
0,4240	LENGTH				Ŧ	\$ 5						5	·			52	9 8	33	33	55	69	44		
	VELL DEPTH FEET	8.3	7.25	4	70	123	8		6.8	4.7		88	25.3	18.9	8	8	147	811	8	245	5+1	147	00 	47.3
1	WELL	Dvg	Dug	6ng	Dilled	Dutted	Pored	Dug	ნიმ	Dvg	Spring	Drilled	5 D O	იოე	Dulled	Duilled	Duilled	Drilled	Duilled	Dilled	Drilled	Drilled	52	Dug
	OWNER	J.W.Thompson	G.DeYoung	R. Banvie	F. Blackie	R . McGrath	C. Prow	W .Laiade	G . McLelton	E. Brennon	l. Prensan	R. Grant	A. McDonald	J. Tumbuil	L. Actions	R, McKean	J.Fraser	C. Robinson	D. Mance	D.Mason	E. Penoil	L, Penoit	F. McDanald	. MeDenald
	NOEX NO.	86.	87.	88	8 9 .	ŝ	5	55.	2 3.	94.	25.	.9%	. 26	.84	.66	100.	. 101	102.	103.	104.	105.	106.	. 701	108.

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Appendix 1 (continued)

	REPORTED QUALITY PROBLEMS	Supplies 65 cattle.	tround	Sultur odor.				above Oily film on top.			above	Yigid too low .	કેલીરે જણાવાડ						
	CONSTRUCTION		Crocked to 1.25 ft. above g					Galvanized crock to 1.3 ft. ground.			Galvanized crack to 3,5 ft. pround						-		•
	Tempa- rature F	2	2	8	56	54	\$	56	53	74					56	65	99	53	8
ALYSES	Total hordness mg/1 as CaCO3	70	65	٥	20	ິ	~	123	196	75	\$			R	263	\$\$	182	ş	8
FIELD ANI	Chloride mg/l	35	12.5	ନ୍ତି	11	76	8	30	165	ŝ	7.5			5	4250	52	36	٤'n	٧J
	Alkoinity mg/1 as CoCO3	65	.9	220	240	432	370	132	127	120	50			73	419	250	155	\$11	<u>.</u>
	907 O1007039	Sand ond gravel		0-10 loose ground, 10-20 gravel, 20-35 clay, 35-60 shale, 60-83 sanidstone	0-25 overburden, 25-73 shale	0-28 averburden ,28-40 soft gray shate , 40-65 block shale , 65-200 gray shale	0-21 overburden, 21-50 shale			0-15 averburden, 15-136 coal shale		0-18 overburden, 10-25 gray shale, 21-215 red shale,	U-140 ted atale, soft bands 146-235 and shale & conglomerate	0-14 mud & boulders, 14-51 yray kinle, 51-58 red shale, 59-75 gray shale, 75-90 red shale, 90-94 gray shale	D-30 overburden ,30-70 soft rad siule,70-82 coal thale,82-87 hand se shale,87-33 soft aper shale, 93- 106 aper siste,106-112 hand red diale,112-250 sticky red shale.	0-11 averburden, 11-23 cœrt shafa, 23-27 gray shale, 27-90 cœal shale, 90-95 gray shale, 95-100 cœal shale	0-14 overburden, 14-73 red shale, 73-100 congionarate	0- 16 mud & gravel , 16-25 braken rock, 25-30 mud & kroken rock, 30- 100 red shale	0-30 clay & gravel, 30-45 gravel & huiders, 45-47 broken rock, 47-171 hurd red shale
REPOR-	TED VIELO GPM			4	4		e			1.5			<u>.</u>	\$	s.	2.5	5	8	~
WATER	RELDW BELDW GROUND		6.6	54	81	2	15	2		21	4.5	8	2	12	5	25	15	33	*
	UIAM- ETER	4.5	2.5	3 47)	5.	in z	2 87	2.5		a V	2.5	- 	r	3 **	4	ž4	-	2 ⁷	* *
CACINO	FEET			Q	8	\$	53			21		8 5	3	5	601	5	53	ç	3
wet t	DEPTH	4.5	8.75	e9 1	73	500	8	14.7		136	<u>بر</u>	<u>.</u>	(c)	54	58	8	8	ŝ	N
7405	WELL	Spring	Dug	Drittled	Drilled	Drilled	Drilled	Dug	Drilled	Dilled	Dug	Dillar		p-HHrq O-HHrq	Dellfed	Drilliod	Drilled	Dilled	Dilled
	OWNER	.McWilliam	McDanald	.Norris	. Norris	winiam.	j.McKenzie	?.Kellock	l.Fultan	elone.N	D.Wilkinson	8, Mines		J. I kay cho	, Williams	L.Mason	A.Nugent	E .McMillan	5.Kellock
		₹	_ <u></u>		hh						A. A								

Appendix 1 (continued)

COMMENTS B	REPORTED QUALITY PROBLEMS									9		Abundant supply.		- - - -						
	CONSTRUCTION									Galvonized crock to 2.2 ft. abov ground.										
	Tempe- rature ° F.	55	z	52				8	63		59									
LYSES	Total hardness mg/1 as CaCO3	ą	Ś	142				153	061	107	174	251	alle for a statement of state from balance	ne og som		 hay (M ayika)			and action of some datases in	
IELD ANA	Chloride mg/l	5.5	8	43	(s			6.7	6.7	а.с С	6.5	44							er ver vig verd værene skriver være	
1 .	Alkatnity mg/1 as CcCO3	142	150	. 23		n i germen bigen jen beg		167	16.4	155	\$61	22.8				 	 			
	CEOLOGIC LOG	0-12 mud & boulders, 12-273 red shale	0-16 mud & boulders, 16-147 conglamerate	0-60 overburden, 60-90 soft red shale, 90-175 red conglomerate		0-28 clay & boulders, 28-98 red shale	0-28 mud, clay & boulders, 28- 240 red shala				0-35 mud & broken rock, 35-119 red shale		0-40 mud & gravel, 40-70 red shole, 70-95 quartzite, 95-125 red shole				-			
REPOR-	TED YIELD GPM	5	m	e		15	3.5				¢		с,			 	 			
WATER	FEET BELOW GROUND	~	Dverflow	55		Dverflaw	50			1.9	50		63			 	 -	*	Ale al an all as to see	
	ETER	ŝ	ŝ	ب ة 19		ي. *	ۍ ۳			2.5	ะำ		ŵ							
04.04.0	FEET	33	33	56		æ	35			*	7		45	• .						
1	PEETH	273	147	175	STAKE.	86	240	20		7	611	2	125			 	 			
TVOF	WELL	Drilled	Drilled	Drilled	EN 8Y MI	Drilled	Drilled	Drilled	Drilled	6n Q	Drilled	Dug	Dolling			 	 			
	OWNER	L. Raluse	R. Boudreau	H.Wynards	NUMBER NOT GIVI	E.filtnore	B. Canway	F. Davis	J.Chemal	Plymouth Fire Dept.). Kerley	G. Purvis	A.Sutherland				 			
	NO.	126.	127.	128.	129.	130.	131,	132.	133.	134.	135.	136.	137.		- has alterden en	 	 	and states		

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Appendix 1 (continued).

: "	Antons SO ₄ CI	1.06/7.35 48.5465. 5.62 0.14 7.43 0.20	0.17 0.28 0.21 0.14 0.67 0.17	0.5615.80 70.1295.91 0.891.69 10.23 31.60	01.04 3.24 40.23 6.94 0.4215.03	30.52 3.53 10.40 3.16	0.54 2.20	0.25 6.77 0.40 0.65 90.0220 88	00.651.18 40.2011.65 50.5717.63 50.5710.28 40.2910.80	0.2721.44 10.94 4.65 10.10 2.25 50.07 1.69	
tons in med	Wa CO3	1.32 0.2 90.0 1.9 1.89 2.6	0.23 4.4	0.12 9.5 1.65 7.45 0.49 3.84 0.49 3.84	0.35 0.2 0.05 9.5 0.12 7.10	0.04 6.8	0.99 2.4	0.990.94	0.53 2.0 1.07 3.0 2.063.4 0.82 3.4 0.82 2.6	1.65 2.9 0.992.5 0.42 2.6 0.04 7.0	
	Calor: *+	4.07 18.2 4.09 18.2 4.03 3.29	3.00.85 0.321.20	25.19 0.27 94.67 4.39 1.09 1.95 13.54 1.75	1.51 1.00 6.32 0.16 21.35 0.34	1.12 0.14 2.85 0.11	0.26 0.06 2.75 6.29	2.05 4.99 0.72 2.59 0.04 0.27).86 2.59 .02 6.59 .38 10.45 .49 3.37 .67 5.49	1.62 10.25 1.13 2.89 2.30 2.05 3.95 0.10	n dan mini katalan katalan katalan ka
	S and a state	455 413	ç	41 38 19 19 19 19	66 C	380 F	36	} ; ₹ ;	4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	393 426	
	Ă	0.5 8.7 8.4	8 × 8 8	2.5 2.5 2.5 2.5 2.5	- C - C - C - C - C - C - C - C - C - C	8 2 C C	- 6.4	20.4.0	7.6.7 7.6.7 7.6.7 7.9	7.0 6.3 9.1 9.1	
	mananterinity	902 922 1254	473 308 308	27.50 10,34(3680	540	1100	86	836 351 3025	385 3190 3190 1540 1540	2530 825 495 825 825	
	HotoT PoloC Dovicesio	530% 867 910	52 180 - 54	1520 267 2014	322 924 [28]	614 740	594 3 890	695 270 1714	278 249 249 972	273 273 497	
	totol stato2	3102 870 918	28 28 28	1528	325 928 1291	619 745	89. 89.	728 275 1717	280 254 254 977	230.230	
	f,	0.0	20.04 5 0.04 2 Tr	0.000	80.34 20.00	1.0.0	0.001	20.01 20.03	1.030	0000	· .
	3	0.00	0 00	0.00 .0.0		10.0 1	1r 0.17	0.07	00000	0000	
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APPENDIX 2

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OUNDWATERS	1.2 	fer Doth Xd	Trey VI 29/7/75 245 11.0 2.2 0.7 432 4.8 76 3.8	22/7/75 125 1.1 23 3.4 240 4 77 0.9 17/9/75 125 1.1 23 3.4 240 4 77 0.9	riden 29/7/75 40 3.2 38 6.8 100 11 88 0.1 riden 29/7/75 48 1.5 20 2.3 60 20 62 0.1	hole 29/7/75 485 11.1 2.8 0.7 720 7.3 222 10.8	hole 29/7/75 1170 1.4 17 3.3 585 3.5 120 8.0 9.70 15/07/75 1170 1.4 17 3.3 585 3.5 120 8.2	iock 30/7/55 115 1.0 12 3.5 252 20 25 0.6 30/7/75 115 2.0 12 3.5 252 0.6	urden 30/7/75 8.7 11.1 92 8.2 261 13 17 00.1 oile 30/7/75 26 3.4 34 3.4 3.8 132 24 5 0.2	vole 30/7/75 87 5.1 52 7.0 139 200 11 0.6 15	urden 30/7/75 17 1.6 56 10 145 28 18 0.1 0	nock 30/7/75 7.4 1.7 35 11 138 14 20 0.1 0.2 eck 30/7/75 7.8 3.8 2.6 6.2 212 37 14 0.2 0.2	shole 30/7/75 165 1.4 1.5 0.4 309 73 8 1.1 2.9.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1	refer 30/7/75 110 3.8 2.8 0.8 225 33 7 0.1	ock 30/7/75 39 4.8 126 39 139 430 20 0.1 0.1	
3ROUNDWATERS	2 X X	Aquifer Date Xa Co Ka Co Ka Co Co Co So Co C	ck-grey vi 29/7/75 245 1.0 2.2 0.7 432 4.8 76 3.8	hole 22/7/75 [25 [1,1] 23 3.4 240 4 77 0.7	erburden 29/7/75 40 3.2 38 6.8 100 11 88 0.1 erburden 29/7/75 48 1.5 20 2.3 60 20 62 0.1	ed shole 29/7/5 485 11.1 2.8 0.7 720 7.3 252 10.8	ed shale 29/7/75 1170 11.4 17 3.3 595 3.5 129 10.7201	bedrock 30/7/5 115 1.0 12 3.5 252 20 25 0.6 1 K0 1	revolven 30/7/75 8.7 11.1 92 8.2 261 13 17 00.1 d'avoie 30/7/75 26 3.4 34 3.4 3.8 132 24 5 0.2	id shele $\frac{10}{20/7/55}$ B7 5.1 52 7.0 139 200 11 0.6 1	verburden 30/7/75 17 1.6 56 10 145 29 18 0.1 0	bedrock 30/7/75 7,4 11.7 35 11 139 14 60 0.1 0.2 bedrock 30/7/75 78 3.2 26 6.2 212 37 14 0.1	d 61-24-016 30/7/75 165 1.4 1.5 0.4 309 73 8 1.1 0.1 15/9/75 165 1.4 0.1	distributed 30/7/75 10.2 0.2 0.2 31 2.5 31 12 3 70.1 distribute 30/7/75 110 3.8 2.8 0.8 225 33 7 0.1 12 0.1 0.7	rediock 30/7/75 38 4.8 126 39 139 430 20 01 01	
CROUNDWATERS	12 X	Aquifer Date Na Kanalian Kanal	block-grey vi 22/7/75 245 1.0 2.2 0.7 432 4.8 76 3.8 bowwerer 22/7/75 5.4 0.1 1.0 2.1 10 1.1 1.3	shole 22/7/75 [25].1 [23] 3.4 240 [1] 77 [0.7]	overburden 29/7/75 40 3.2 38 6.8 100 11 88 0.1 overburden 29/7/75 48 1.5 20 2.3 60 20 62 0.1	red shole 29/7/75 485 1.1 2.8 0.7 720 7.3 252 10.8	red shole 22/7/75 1170 1.4 17 3.3 595 3.5 129 10.7201	bedrock 30/7/75 II5 1.0 12 3.5 222 20 25 0.6 0.4 0.1 20 4	overburden 30/7/75 8.7 11.1 92 8.2 261 13 17 00.1 red shale 30/7/75 26 3.4 34 3.8 32 28 5 0.2	red shole 20/7/75 87 5.1 52 7.0 139 200 11 0.6 1	overburden 30/7/75 17 1.6 56 10 145 23 18 0.1 0	bedrock 30/7/75 7.4 1.7 35 11 138 14 50 0.1 0.7 bedrock 30/7/75 78 3.8 26 6.2 212 37 14 0.1	red 11-10/01/25 165 1.4 1.5 0.4 309 73 8 1.1	overburden 34////3 0.1 0.2 31 2.6 31 13 3 701	bedrock 30/7/75 38 4.8 126 39 139 439 20 01 01	
OF GROUNDWATERS	5	Aquifer Date X Co No Aquifer SOA CL T	2 block-grey vi 29/7/75 245 1.0 2.2 0.7 432 4.8 76 3.8 terrescripts 29/7/75 5.4 0.4 1.1 1.5 1.6 1.4 1.1 8.5 0.1	3 shole 22/7/75 (25 1.1 23 3.4 240 4 77 0.9 	9 overburden 29/7/75 40 3.2 38 6.8 100 11 88 0.1 overburden 29/7/75 48 1.5 20 2.3 60 20 62 0.1	red shole 29/7/75 485 1.1 2.8 0.7 720 7.3 257 10.8	red shole 29/7/75 1170 1.4 17 3.3 595 3.5 1370 9.2 2	bedrock 30/7/75 II5 1.0 12 3.5 222 20 25 0.6 0.4 0.1 0.1 25 0.6	overburden 30/7/75 8.7 1.1 92 8.2 261 13 17 60.1 red shale 30/7/75 26 3.4 3.4 3.8 13 17 60.1	2 red shale 30/7/75 87 5.1 52 7.0 139 200 11 0.6 1	.3 overburden 30/7/75 17 11.6 56 10 145 28 18 0.1 0	Deckock 33/7/75 7.4 1.7 35 11 138 14 50 0.1 7 r bedrock 33/7/75 78 3.2 26 6.2 212 37 14 60 0.1	7 red 11-1 hole 30/7/75 165 1.4 1.5 0.4 309 73 8 11.1 15/9/75 155 1.4 1.5 0.4 309 73 8 11.1	5 red webviden JU/7/2 0.2 0.2 31 2.0 01 13 5 70.1 5 red webvide 30/7/25 110 3.8 2.8 0.0 225 33 7 0.1 1.0.075	5 bedrock 30/7/75 38 4.8 126 39 139 439 20 01 01	
S OF GROUNDWATERS	S	Well Aquifer Date Na K Co Ng About CL T Sr Capith Aquifer Sompled Na K Co Ng CL T Sr feet	200 block-grey vi 23/7/75 245 [1.0 2.2 0.7 432 4.8 76 3.8 howevers 237775 5.4 A.A.K. 1. 1.2 A.H. 1. 8.5 A.H.	73 thole 22/7/75 (25 1.1 23 3.4 240 4 77 0.9 0.2 17/97.75 (26 1.1 23 3.4 240 4 0.1 0.7 0.9	18 overburden 29/7/75 40 3.2 38 6.8 100 11 83 0.1 overburden 29/7/75 48 1.5 20 2.3 40 20.1 20.1	138 red thole 22/7/75 435 1.1 2.8 0.7 720 7.3 227 10.9 ref thole 22/7/75 435 1.1 2.8 0.7 720 7.3 252 10.9 ref to 0.0 1	175 red shole 29/7/75 1170 1.4 17 3.3 585 3.5 1370 8.2 1 1/201	78 bediock 30/7/5 115 1.0 12 3.5 252 20 25 0.6 0.4 0.7 K0.14	I4 overburden 30/7/75 8.7 1.1 92 8.2 261 13 17 60.1 171 red shale 30/7/75 26 3.4 3.4 3.8 13 17 60.1	245 red shole 20/7/75 87 5.1 52 7.0 139 200 11 0.6 1	25.3 overburden 30/7/75 17 1.6 56 10 145 28 18 0.1 7	30 ^{bedrock} 30/7/75 7,4 1,7 35 11 138 14 50 0.1 247 bedrock 30/7/75 78 3.8 26 6.2 212 37 14 0.1	247 red 11-15/01e 30/7/75 155 1.4 1.5 0.4 309 73 8 11.1 15/9/75 155 1.4 1.5 0.4 309 73 8 11.1 15/9/75	14 0 0 c c c c c c c c c c c c c c c c c	75 bedrock 30/7/75 38 4.8 126 39 139 439 20 01 01	
SES OF GROUNDWATERS	1 2 1	Well Aquifer Date Na K Co Ng Athered CO K SO4 CL F Sr Freet Sompled Ka K Co Ng Athered CO CL F Sr freet Sompled	200 block-grey vi 29/7/75 245 [1.0 2.2 0.7 432 4.8 76 3.8 revenues 29/7/75 5.4 0.4 [1. 1.2 1.4 [1. 8.5 4]	73 thele 29/7/55 [25 [1.1] 23 3.4 240 2 77 0.9	18 overburden 29/7/75 40 3.2 38 6.8 100 11 83 0.1 overburden 29/7/75 48 1.5 20 2.3 40 20 1	138 red shole 22/7/75 495 1.1 2.8 0.7 720 7.3 227 10.9 ref 0.17 ref 227 10.9 ref 0.17 ref 227 10.9 ref 0.17 ref	175 red shale 22/7/75 1170 1.4 17 3.3 595 3.5 1200 8.2 15/001 8.4 0.7 201	78 bediock 30/7/75 115 1.0 12 3.5 252 20 25 0.0 12 0.7 K0.14	14 overburden 30/7/75 8.7 1.1 92 8.2 261 13 17 60.1 171 red shale 30/7/75 26 3.4 3.4 3.8 33.2 24 5 0.2 6.1	245 red shale 20/7/75 87 5.1 52 7.0 139 200 11 0.6 1	d 25.3 overburden 30/7/75 17 1.6 56 10 145 23 18 0.1 0	30 bedrock 33/7/75 7,4 11,7 35 11 138 14 50 0.1 237 247 bedrock 33/7/75 78 3.8 26 6.2 212 37 14 0.1	247 redurshole 30/7/75 155 1.4 1.5 0.4 309 73 8 1.1 15/9/75 1.4 1.5 0.4 307 73 8 1.1 1.2 0.1	14 Overburden JU/7/2 0.2 U.2 31 2.0 31 1 2 0.1 1 2 0.1 1 1 2 0.1 1 1 2 0.1 1 1 2 0.1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	75 bedrock 30/7/75 38 4.8 126 39 139 439 20 01 01	
LYSES OF GROUNDWATERS	5.	Well Well Date Na Anuler Date Na Kandon Kander Son	net 200 black grey vi 29/7/75 245 1.0 2.2 0.7 432 4.8 76 3.8 textraction 29/7/75 4.4 0.4 15 14 25 4.8 5.41	73 thole 22/7/75 [25 [1.1] 23 3.4 240 2 77 0.9	ald 18 overburden 29/7/75 40 3.2 38 6.8 100 11 88 0.1 overburden 29/7/75 48 1.5 20 2.3 60 20 62 0.1	t 138 red thole 29/7/75 485 1.1 2.8 0.7 720 7.3 227 10.9 1 1 1 2 1 2 2 2 2 1 1 2 1 2 2 2 2 2 2	175 red shele 29/7/75 1170 1.4 17 3.3 595 3.5 1200 8.2 [12/0.1]	78 bedrock 30/7/5 115 1.0 12 3.5 252 20 25 0.0 12 0.7 20.14	e 14 overburden 30/7/75 8.7 1.1 92 8.2 261 13 17 60.1 ck 171 red shale 30/7/75 26 3.4 3.4 3.8 13 17 60.1	m 245 red shale $\frac{307773}{77075}$ 87 5.1 52 7.0 139 200 11 0.6 $\frac{110}{11}$ 0.5 1 0.0 1	mald 25.3 everburden 30/7/75 17 1.6 56 10 145 23 18 0.1 0	Ter 247 bedrock 30/7/75 78 1.7 35 11 138 14 50 0.1 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	247 red 15+5/01e 20/7/75 165 1.4 1.5 0.4 309 73 8 1.1 15/9/75 1.6 1.5 0.4 309 73 8 1.1 1.2 K0.1	100 14 overburden JU///2 0.2 0.2 0.2 31 2.5 31 2 7 0.1 135 reductione 30/7/75 110 3.8 2.8 0.6 225 33 7 7 0.1 1//0/75	75 bedrock 30/7/75 36 4.0 126 37 137 430 20 0.1 0.1 16/9/75 36 4.0 126 37 137 430 20 0.1 0.1	
VALYSES OF GROUNDWATERS	5	exem Well Well Date Na K Co Na Co C L T Sr Coppilh Aquifer Sompled X K Co Na CC C L T Sr freet Sompled X K Co Na CC C L T Sr	200 black-grey 3/ 27/7/5 245 1.0 2.2 0.7 432 4.8 76 3.8 And the converse of 27/7/5 4.4 A. th. 15 14 18 5.4.1 8.5 A	arit 73 thole 29/7/75 [25 [1.] 23 3.4 240 1 77 0.9	Donald 18 overburden 29/7/75 40 3.2 38 6.8 100 11 88 0.1 derson overburden 29/7/75 48 1.5 20 2.3 60 20 62 0.1	wort [38] red shole 22/7/75 495 [1.1 2.8 0.7 720 7.3 227 10.9]	ote 175 red shale 22/7/75 1170 1.4 17 3.3 595 3.5 1200 8.2 15/07.6	Mompson 78 bedrock 30/7/75 115 1.0 12 3.5 252 20 25 0.6 0.7 20.14	anvie 14 overburden 30/7/75 8.7 11.1 92 8.2 261 13 17 60.1 ellock 171 red shale 30/7/75 26 3.4 34 3.8 32 24 5 0.2	Autom 245 red shale 20/7/75 87 5.1 52 7.0 139 200 11 0.6 1	teDonald 25.3 overburden 30/7/75 17 1.6 56 10 145 28 18 0.1 0	Tow 30 bedrock 30/7/75 7.4 1.7 35 11 138 14 50 0.1 7.4 Neworer 247 bedrock 30/7/75 78 3.2 26 6.2 212 37 14 60 0.1	stron 247 red 10+26/01 20/7/75 155 1.4 1.5 0.4 309 73 8 1.1 1.4 1.5 0.4	terminon 14 overburden 30/7/5 110 3.8 2.8 0.18 2.5 31 1 2 0.1 Ver 135 reductione 30/7/55 110 3.8 2.8 0.18 225 33 7 0.1 Ver 105 reductione 10/07/55 110 1 2.8 0.18 225 13 1 2 0.1	villiam 75 bedrock 30/7/75 38 4.8 126 39 139 439 20 01 01	
ANALYSES OF GROUNDWATERS		Present Well Aquifer Date Na K Co Ng About CL F Sr Complete Somplete K Co Ng CC CL F Sr Complete Somplete K Co Ng CC CL F Sr	a. Meisener 200 block-grey vi 27/775 245 [1.0] 2.2] 0.7] 432 [4.8] 76 3.8] andre: 200 block-grey vi 27/775 245 [1.0] 2.2] 0.7] 432 [4.8] 76 3.8]	Norit 73 thole 22/7/75 [25 [1.] 23 3.4 240 1 77 0.9	McDonald 18 overburden 29/7/75 40 3.2 38 6.8 100 11 88 0.1 Anderson overburden 29/7/75 48 1.5 20 2.3 60 20 62 0.1	Stewart [38] red shale 22/7/75 495 [1.1 2.8 0.7 720 7.3 227 10.9 [1. Foole 127 / 7/5 1170 1.4 17 3.3 595 3.5 1200 8.1 7.2 1. Foole 127 / 7/5 1170 1.4 17 3.3 595 3.5 1200 8.2 10.7 701	3.Thompson 78 bediock 30/7/5 115 1.0 12 3.5 252 20 25 0.6 12 8.5 0.6 12 25 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.	R.Bonvie 14 overburden 30/7/75 8.7 11.1 92 8.2 261 13 17 00.1 5.Kellock 171 red shale 30/7/75 26 3.4 34 3.8 132 24 5 0.2	D.Maron 245 red shale 20/7/75 87 5.1 52 7.0 139 200 11 0.6 1	A.McDonald 25.3 overburden 30/7/75 17 1.6 56 10 145 28 18 0.1 0	C.Brow 30 bedrock 33/7/75 7.4 1.7 35 11 138 14 50 0.1 G.Ahworer 247 bedrock 33/7/75 78 3.8 26 6.2 212 37 14 0.2	R.Polton 247 red 10+26/01 20/7/75 155 1.4 1.5 0.4 309 73 8 1.1 1.4 1.5 0.1	C. Adomson 14 overburden 30/7/5 0.2 0.2 0.5 31 2.5 31 3 0.1 5 0.1 A.Weir 135 red tsthole 33/7/55 110 3.8 2.8 0.8 225 33 7 7 0.1 20 2	W.Williams 75 bedrock 30/7/75 38 4.8 126 39 139 439 20 01 01	
ANALYSES OF GROUNDWATERS	S .	Present Well Mult Aquifer Date Na K Co No Co CL T Sr Complete Somplete Somp	L. Meisener 200 black grey vi 23/7/75 245 1.0 2.2 0.7 432 4.8 76 3.8 E anhor	F.Norit 73 there 22/7/75 125 1.1 23 3.4 240 1 77 0.9	F.McDonald 18 overburden 29/7/75 40 3.2 38 6.8 100 11 88 0.1 D.Anderson overburden 29/7/75 48 1.5 20 2.3 60 20 62 0.1	S.Stewart 138 red thale 22/7/73 485 1.1 2.8 0.7 720 7.3 227 10.9 1 1 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2	R.Foote 175 red shale 29/7/75 1170 1.4 17 3.3 595 3.5 1200 8.2 15/07/50 12/07	G.Thompson 78 bedrock 30/7/5 115 1.0 12 3.5 252 20 25 0.6 12 8.5 0.1 (2014)	R.Bonvie 14 overburden 30/7/75 8.7 1.1 92 8.2 261 13 17 60.1 S.Kellock 171 red shale 30/7/75 26 3.4 3.4 3.8 13 17 60.1	D. Marcar 245 red shale 20/7/75 87 5.1 52 7.0 139 200 11 0.6 1	A.McDonald 25.3 overburden 30/7/75 17 11.6 56 10 145 23 18 0.1 0	C. Brow 30 bedrock 33/7/75 7.4 1.7 35 11 138 14 50 0.1 0.2 0.7 0.6 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	R. Polion 247 red 15+5/01e 30/7/75 165 1.4 1.5 0.4 309 73 8 1.1 15/9/75 15 1.4 1.5 0.4 309 73 8 1.1 2.0.1	C. Addmison 14 overburden JU//75 0.2 U.2 31 2.5 31 1 3 U.1 A.Weir 135 reductione 30/7/75 110 3.8 2.8 0.8 225 33 7 0.1 1/0/775 110 1.4 2.8 0.1 2.7 31 1 2 0.1 V.1	M.William 75 bedrock 30/7/75 38 4.8 126 39 139 439 20 0.1 0.1	
CAL ANALYSES OF GROUNDWATERS	S 2	Imple Present Well Majuriter Date Na K Co Na Co CL F Sr Ma Construction Complete Somplete K Co Na CL F Sr Somplete K Co Na Construction Construction Solution Statement Statemen	20 L.Meisener 200 bleck grey vi 23/7/75 245 1:0 2:2 0.7 432 4.8 76 3.8	22 F.Norit 73 their 22/7/75 125 1.1 23 3.4 240 4 77 0.9	23 F.McDomold 18 overburden 29/7/75 40 3.2 38 6.6 100 11 88 0.1 24 D.Anderson overburden 29/7/75 48 1.5 20 2.3 60 20 62 20.1	25 S.Stewart 138 red thale 22/7/75 485 1.1 2.8 0.7 720 7.3 227 10.9 1 1 1 2 1 2.8 0.7 720 7.9 252 10.9 1 1 2 1 2 2 2 2 10.5 1 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	26 R.Foote 175 red shale 29/7/75 1170 1.4 17 3.3 595 3.5 1200 8.2 15/07/8 1700 1.4 17 1.3 10.7 10.0 1.2 1.0 10.7 10.7 10.7 10.7 10.7 10.7 10.7	27 G.Thompson 78 bedrock 30/7/5 115 1.0 12 3.5 252 20 25 0.6 12 8.5 0.1	28 R.Bonvie 14 overburden 30/7/75 8.7 1.1 92 8.2 261 13 17 60.1 29 S.Kellock 171 red shale 30/7/75 26 3.4 3.4 3.8 13 17 60.1	30 D.Maton 245 red shale 30/7/75 87 5.1 52 7.0 139 200 11 0.6 1	31 A.McDonald 25.3 overburden 30/775 17 11.6 56 10 145 28 18 0.1 0	32 C.Biow 30 bedrock 30/7/75 7.4 1.7 35 11 138 14 50 0.1 33 33 5.3 5.4 Microre 247 bedrock 30/7/75 78 3.8 26 6.2 212 37 14 0.1	34 R. Polton 247 red 15+5/ole 30/7/75 165 1.4 1.5 0.4 309 73 8 1.1 15/9/75 15 1.4 1.5 0.4 309 73 8 1.1 2.0.1	33 C. Addmison 14 overburden JU///2 0.1 U.2 31 2.0 31 1 2 0.1 23 0.1 23 0.1 23 0.1 23 0.1 23 0.1 20	37 M.Williams 75 bedrock 30/7/75 38 4.8 126 39 139 439 20 0.1 0.1	
MICAL ANALYSES OF GROUNDWATERS	S 3	Sample Present Well Mult Aquifer Date Na K Co Na Coll F Sr Sampled K K K Co Na Coll F Sr Sampled K K K Co Na Coll F Sr Sampled K K K Co Na Coll F Sr Sampled K K K Co Na Coll F Sr Sampled K K K Co Na Coll F Sr Sampled K K K K K K K K K K K K K K K K K K K	20 L.Meisener 200 blocktyry vi 23/7/75 245 [1:0 2:2 0.7 432 4.8 76 3.8 21 E anheisener 200 blocktyrer 23/7/75 5.4 6.4 1. 1.2 4.1 8.5 4.1	22 F.Novit 73 thele 22/7/75 [25 1.1] 23 3.4 240 4 77 0.9	23 F.McDomold 18 overburden 29/7/75 40 3.2 38 6.6 100 11 88 0.1 24 D.Anderson overburden 29/7/75 48 1.5 20 2.3 60 20 62 0.1	25 5.Stewart 138 red thole 22/7/73 485 1.1 2.8 0.7 720 7.3 227 10.8 1 0.1 1 0.14	26 R.Foote 175 red shale 29/7/75 1170 1.4 17 3.3 595 3.5 1200 8.2 1500 8.2	27 G.Thompson 78 bedrock 30/7/5 115 1.0 12 3.5 252 20 25 0.6 12 8.5 0.1	28 R.Banvie 14 overburden 30/7/75 8.7 1.1 92 8.2 261 13 17 60.1 29 S.Kellock 171 red shale 30/7/75 26 3.4 3.4 3.8 3.3 9.2 6.1 7.1 7.0 17 60.1 7.1 7.2 7.1 7.4 3.4 3.6 3.2 6.2 6.2 7.4 3.4 3.6 3.2 5.4 5 0.2 6.2 <td>"30 D. Marion 245 red shale 30/7/75 87 5.1 52 7.0 139 200 11 0.6</td> <td>31 A.McDonald 25.3 overburden 30/775 17 1.6 56 10 145 28 18 0.1 0</td> <td>32 C.Biow 30 bedrock 30/7/75 7.4 1.7 35 11 138 14 50 0.1 33 33 G.Amoler 247 bedrock 30/7/75 78 3.8 26 6.2 212 37 14 0.1</td> <td>34 R. Polion 247 red 15+5/ole 30/7/75 165 1.4 1.5 0.4 309 73 8 1.1 15/9/75 15 1.4 1.5 0.4 309 73 8 1.1 2.0.1</td> <td>33 C. Addmison 14 overburden JU///2 0.1 U.2 31 2.0 31 1 2 0 U.1 3 U.1 3 3 0.1 23 33 7 0.1 23 33 1 2 0.1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1</td> <td>37 M.Williams 75 bedrock 30/7/75 38 4.8 126 39 139 439 20 0.1 0.1</td> <td></td>	"30 D. Marion 245 red shale 30/7/75 87 5.1 52 7.0 139 200 11 0.6	31 A.McDonald 25.3 overburden 30/775 17 1.6 56 10 145 28 18 0.1 0	32 C.Biow 30 bedrock 30/7/75 7.4 1.7 35 11 138 14 50 0.1 33 33 G.Amoler 247 bedrock 30/7/75 78 3.8 26 6.2 212 37 14 0.1	34 R. Polion 247 red 15+5/ole 30/7/75 165 1.4 1.5 0.4 309 73 8 1.1 15/9/75 15 1.4 1.5 0.4 309 73 8 1.1 2.0.1	33 C. Addmison 14 overburden JU///2 0.1 U.2 31 2.0 31 1 2 0 U.1 3 U.1 3 3 0.1 23 33 7 0.1 23 33 1 2 0.1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	37 M.Williams 75 bedrock 30/7/75 38 4.8 126 39 139 439 20 0.1 0.1	
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APPENDIX 2 (continued)

APPENDIX 3

SUMMARY LOGS OF WELLS DRILLED ON THE STELLARTON INTERVAL, NOVA SCOTIA DEPARTMENT OF THE ENVIRONMENT AND NOVA SCOTIA DEPARTMENT OF MINES.

INT - 1 - 75 (Dec. 9-15, 1975, N.S. Dept. of the Environment testhole)

Total Depth:	100 feet
Diameter:	8inches to 20 feet, 6 inches to 100 feet
Casing:	21 feet 10 inches of 6 1/4 inch ID casing, to approximately 20 feet
-	below ground.
Water at:	20 feet - 2+5 gpm; 25-30 - ≥ 5 gpm
Water level:	at finish approximately at ground level
Log:	0–5 silt & fine sand
	5–20 stratified sand, gravel and boulders
	20–35 silty to clayey till
	35–45 fine sand & gravel
	45–75 find sand, silt & clay
	75–80 green grey siltstone & sandstone
	80-100 mainly red brown siltstone & fine grained sandstone,
	minor hydro carbon
	Bedrock at approximately 75 feet

INT - 2 - 75 (Dec. 15-16, 1975, N.S.Dept. of the Environment testhole)

Total Depth:	50 feet
Diameter:	8 inches to 20 feet, 6 inches to 50 feet
Casina:	22 feet, driven to 21.0 feet below ground
Water at:	11 feet
Loa:	0–6 silt & clay
	6-15 stratified sand, gravel & pebbles
	15–25 gravel and clay
	25-39 mainly clay; possibly thin gravel bed 32-35 ft.
	39-50 bedrock - alternating, soft & hard grey shale, minor hydrocarbon

N.S.DEPT. OF MINES testhole (June 9, 1964)

0-1 topsoil
1-4 fine to medium grained sand
4-10 gravel
10-20 sand, gravel & clay (fine sand; fine gravel)
20-24 blue-grey clay
24-50 gray shale
50-60 carbonaceous shales. Thin coal bed (1") at 52 feet
60-90 silty shale

APPENDIX 4

SUMMARY LOGS OF BACKHOE TESTPITS, September 29 - October 1, 1975

#p]

0-2 till, silt-fine sand, dry & compact.
2-9 till, sandy to gravelly
9-12 coarse gravel and silt. Boulder layer at 11 feet
12-13 gravel and boulders
13-14 clay and gravel
14 greyish green, friable siltstone. Water at 13 feet.

[#]P2

0-4 sandy till with coarse gravel lenses 4-6.5 coarse sand, gravel and boulders. Water 6.5 greenish grey, hard siltstone.

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0-1 silt

1-4.3 stratified sand, gravel and boulders. Water at 3.0 feet

4.3- 5 gravel

5-7 weathered bedrock (red sandstone)

#p4

0-2 sandy till 2-5 sand and gravel. Water 5-7 very coarse gravel and boulders 7 bedrock - red sandstone.

[#]P5

0-3.5 silty to clayey, red brown till
3.5 -4 sand, gravel and boulders
4-6 large boulders and clay
6-6.5 well rounded pebbles, sand and gravel with minor clay
6.5 Bedrock ?

#p6

0-4 silty to clayey till. Gravel lens at 2 feet 4-6 sandy, gravelly till 6-7 boulders 7 bedrock – red sandstone

#p7

0-3 silt and clay, possibly till
3-7 sand, gravel and boulders. Water at 7 feet
7-8.5 stratified clay and gravel. Clay hard and compact
8.5-9.5 clay with minor gravel.
9.5 bedrock ?

#P8

0-2 silt
2-6.5 stratified clay, sand, gravel and pebbles
6.5 - 7 clay
7-7.5 gravel, clay
7.5 - 8 clay
8-8.5 coarse gravel
8.5-10 hard, compact clay with gravel
10-13.5 hard clay
13.5 possibly bedrock

#p9

0-6.5 silt 6.5 - 8.5 coarse sand and fine gravel 8.5 - 11.5 pebbles and sand. Water at 8.5 - 9 feet 11.5-12 hard clay

#P10

0-4.5 coarse gravel and boulders . Water at 1-2 feet 4.5-7.5 hard clay and silt, minor sandy lenses 7.5 Too hard to dig further

#P11

0-4.5 sand, silt and clay 4.5 -8 sand, gravel and pebbles 8-15 sand, gravel and clay 15 either hard clay and boulders or bedrock

[#]P 12

0-2 fine sand and silt
2-13 stratified sand, gravel and pebbles
13-16 medium to coarse sand and coarse sand to fine gravel layers.

#₽ 13

0-3 silt 3-5.5 clayey gravel and boulders 5.5-6 boulders 6-8.5 stratified medium sand and clay

#P 14

0-3 clayey gravel and boulders
3-7 coarse gravel and boulders
7-7.5 boulder layer
7.5-8 clayey gravel.
8-10 quicksand, with minor clay layers
10-10.5 soft, laminated clay and silty clay.

[#]P 15

0-4 sandy gravelly till with fine gravel lenses 4-6.3 stratified sand, gravel, pebbles 6.3-10.5 hard green clay and silty clay 10.5 bedrock or boulders

[#]P 16

0-2 silty till 2-5.5 stratified gravelly sand and pebbles 5.5-7 loose gravel and boulders 7-9 stratified sand, gravel and pebbles 9-11 fine sand and silt 11-15 soft, laminated silt and clay

#P 17A

0-2 sandy till
2-5 stratified sand and silt
5-6 gravel and pebbles, caving due to water inflow

[#]P 17B

0-1 topsoil 1-4.5 stratified sand, gravel and pebbles 4.5-7.5 gravel and pebbles 7.5 - 8 silty clay 8-11 clay and silty clay, minor sand and gravel 11-13 hard clay with gravel 13 hard - either bedrock or boulder layer

#P 18

0-2 sandy silt 2-7 stratified sand, gravel, boulders 7-12.5 laminated silt and clay 12.5 hard layer

#P 19

0-4.5 gravel and boulders 4.5 - 14 laminated fine sand, silt and clay 14 hard layer

#p 20

0-2.5 sandy silt 2.5 -8 coarse sand, gravel and boulders, crudely stratified 8-15 layered soft clay and silt

[#]P 21

0-5 stratified sand (fine) and silt 5-6 coarse sand and fine gravel 6-10 stratified gravel and boulders 10-11 boulder layer, some sand.

[#]P 22

0–1.5 sandy silt

1.5-4 stratified sand and silt

4-10.5 crudely stratified coarse sand, gravel, and pebbles. Boulder layer at 7 feet. Water at 10 feet.

10.5-15 clay and clayey silt, soft, laminated

[#]P 23

0-3 crudely stratified coarse sand, gravel and boulders. Water at 3 feet. 3-8.5 hard clay with gravel.

#P 24

0-5 silty sand 5-11.3 stratified sand, gravel and silt 11.3-11.5 clay 11.5-14.5 sandy silt

#P 31

0-1.5 stratified sand, gravel and boulders
1.5-4 hard clay with gravel
4-6.5 soft clay
6.5 hard layer - possibly bedrock

[#]P 25

0-4.3 sandy silt 4.3-5 coarse sand and fine gravel 5-7 layered fine to medium sand and silt 7-11.5 gravel and pebbles 11.5 hard layer – boulders or bedrock

#P 26

0-3.5 silty sand and pebbles 3.5-7 stratified fine sand and sandy silt 7-11 stratified gravel, pebbles and clayey sand 11-13 hard clay with gravel 13 hard layer

[#]P 27

0-5 silty sand 5-8 stratified sand and gravel 8-10 boulder layers 10-15 laminated soft clay and silt

#P 28 0-4 hard clay with gravel.

#P 29
0-3.5 stratified sand, gravel and boulders
3.5-5 laminated soft clay with minor silt

#P 30 0-1 clay till 1-3.5 sandy silt 3.5-11.5 clayey gravel and boulders

APPENDIX 5

NOVA SCOTIA DEPARTMENT OF HIGHWAYS BOREHOLE RECORDS

#H 1

 $\overline{0}$ -2 sand and gravel with small cobbles

2-4 brown stiff sandy clay with small stones

4-7 hard brown sandy clay with small stones

7-13.5 hard dark clay with broken shale

13.5-18.5 bedrock - soft dark shale

#H 2

0-4 loose brown silty sand with small cobbles

4-7 loose brown silty sand with wood and organic fibres

7-10 hard dark broken slate shale rock

10-12 hard dark brown shale rock

12-17 shale bedrock

#H 3

0-2 sand, gravel and small cobbles

2-4 brown fine sand with small stones

4-6 brown fine sand with stones and broken shale

6-9 hard dark clay with broken shale

9-11 broken soft shale

11-15 hard dark clay with layers of shale

15-30 shale bedrock

∜H 4

0-2 sand, gravel and small cobbles

2-4 brown silty clay with small stones

4-6 stiff brown silty clay with small stones

6-12.5 hard dark clay with layers of broken shale

12.5-18 bedrock - shale

#H 5

0-2 loam with sand and organic fibres 2-4 sand with small stones and clay 4-11 brown silty clay with small stones

11-16.5 hard dark clay with layers of shale

16.5-36 bedrock

#H 6

 $\overline{0-5}$ loose brown fill with small cobbles

5-8 stiff brown silty clay with small stones

8-12 loose brown silt with silty clay and small stones

12-17 dark grey clay with small stones and broken rock

17-20 dark arey broken layers of soft shale

20-26 bedrock - black shale

Holes H 1 to H 6 are from the STELLARTON INTERVAL BRIDGE over the East River.

#H 7

0-2 boulders and gravel 2-7 clay 7-12 clay and gravel 12-17 clay, gravel and broken shale 17-19 broken shale 19-24 harder shale bedrock

[#]H 8

0-4 gravel 4-8 silt 8–13 gravel and some clay 13–18 broken shale and clay 18–27 broken shale 27–33 harder shale bedrock

#H 9

0-9 sand and gravel 9-14 sand, gravel and broken shale 14-19 sand and gravel 19 22 sand and broken shale 22-29 broken shale 29-34 harder shale bedrock

#H 10

0-2 gravel 2-12 sandy clay 12–15 sand, gravel and some clay 15–17 broken shale 17–23 harder shale bedrock

Holes H 11 to H 20 are from the TRANS CANADA HIGHWAY 104 overpass. The exact locations of the holes is not known.

#H 11

0–10 coarse sand and gravel 10–18 sand, gravel and boulders 18–46 soft red clay 46–56 solid gray shale

#H 12

0-4 coarse gravel in river bed 4–38 soft red sandy clay 38–48 gray shale

#H 13

0-7 sand and fine gravel

7-21 coarse river gravel

21-39 hard red clay embedded with small stones

39-50 soft gray shale

Holes H 7 to H 10 are from the ALBION MINES BRIDGE over the East River.

#H 14

.

0-7 fine sand and silt

7-9 coarse gravel

9-30 hard red clay embedded with small stones and boulders 30-45 soft gray shale

#H 15

0-4 water
4-12 sand and gravel with small boulders (river bed)
12-34 soft clay
34-36 gravel and clay
36-42 gravel, shale and clay mixed
42-44 soft shale and clay (fault gouge)
44-55 shale

[#]H 16

0–6 soft red sand 6–16 coarse gravel 16–31 boulders, clay and gravel 31–40 soft gray shale

[#]H 17

0-7 water 7-10 boulders and gravel 10-40 soft clay 40-44 gravel and clay 44-54 shale

#H 18

0–9 very fine grained sand 9–14 gravel and clay 14–30 shale

#H 19

0-4 very soft clay 4-11 gravel and clay 11-30 very soft shale with seams of clay 30-45 shale

#H 20

0–7 clay 7–11 gravel 11–25 soft shale

APPENDIX 6

NOVA SCOTIA DEPARTMENT OF MINES BOREHOLE RECORDS

#1019
0-2 surface
2-4 blue shale
4-17.6 blue shale with limestone stringers
17.6 -52 red sandy shale with limestone stringers

#1020

0-3 surface 3-30 grey limestone 30-53 blue shale with limestone stringers

#1039

0-3 surface 3-14.6 gray limestone 14.6-48 grey limestone & red clay 48-50 fine grained red sandstone

#1040

0-10.6 surface 10.6-37 fine grained red sandstone

#1041

0-10 surface 10-18 fine grained red sandstone 18-21 grey sandstone with limestone stringers 21-27 fine grained red sandstone

#1042

0-7 surface 7-12 limestone with some sandstone bands 12-21 grey & red sandstone 21-50 red sandstone

#1043 0-10 boulders & clay 10-15 sand & boulders 15-22 red sandstone

#1044

0-20 boulders & clay 20-30 red sandstone with bands of grey clay

#1045 0-20 surface 20-40 red sandstone

[#]2466

0-55 overburden 55-65 grey shale 65-82 red sandstone 82-123 red & grey shale 123-125 grey shale with some coal 125-230 grey sandstone 230-237 grey sandstone with small conglomerate bands 237–265 red & grey sandstone 265-277 red & grey shale 277-288 red sandstone 288-330 red & grey sandy shale 330-336 black shale with lines of coal 336-368 red & gray sandy shale 368-371 gray shale with 2 inch asphalt in a calcite stringer 371-378 soft grey shale

#3108

0-49 overburden 49-59 soft gray shale 59-76 sandy gray shale 76-87 dark shale 87-96.5 black & brown oil shale 96.5-105 splint & coal 105-130 black coal, dirty sections 130-131 soft gray shale 131-145 soft gray shale, little coal 145-147.5 coal & splint 147.5-168.5 soft gray shale 168.6-172.5 coal & splint 172.5-210 shale 210-317 shale, sandy in places 317-408 gray shale, sandy in places 408-415 oil shale & coal 415-426 gray & dark shale 426-441 oil shale & coal 441-573 gray shale, sandy in places 573-593 fine-grained gray sandstone 593-616 gray shale 616-622 dark shale (oil shale) 622-649 gray shale 649-653.5 oil shale & coal

.R.	- 2	
#3584	Overburden thickness, teet 17	
#3585	20	
#3586	23	
#3587	20	
#3588	22	
#3589	15	
#3590	16	
#3591	17	
#3592	20	
#3593	21	
#3594	16	
#3595	15	
#3596	18	
#3597	15	
#3598	15	
#3599	18	
#3600	15	
#3601	18	
#3602	18	

#4135

0-13 overburden – reddish clay with small rocks & shale 13-36 dark gray soft, slaty shale 36-40 shaly red, firm conglomerate

#4136

0-10 overburden- red clay, gravel, red siltstone or shale 10-18.5 red sandy shale 18.5 - 24 red siltstone 24-41 red shale, somewhat sandy

#4137

0-13 overburden – red silt, sand & clay 13-17 red sandy shale 17-22.5 red siltstone 22.5-25 red sandy shale 25-29 red siltstone 29-41 red sandy shale

#4138

0-13 overburden - clay, sand, small rocks 13-36.5 gray & red sandy shale

#4139

0-12 overburden – red silt, dark gray clay, & gravel 12-33 gray sandy shale

#4140

0-10 overburden – red clay, gray clay, gravel & shale 10-32 shale or slate

#4141

0-10 overburden – gravelly earth & reddish shale 10-33 shale or slate

#4142

0-10 overburden – reddish clay & gravel 10-32 shale or siltstone

#4143

0-49 overburden – reddish clay & small rocks 49-72 gray slaty shale, sandy in places; minor red shale

#4144

0-14 overburden – gravel, red clay & soft gray shale 14-32 slaty shale

#4145

0-5 overburden – gravel & sand 5-13 dark gray shale 13-15.5 reddish shaly conglomerate 15.5-29 dark gray shale

#4146

0-10.5 overburden - sand, gravel, gray clay & shale 10.5-15 gray shale

#4147

0-50 overburden - reddish clay & small rocks 50-73 red & gray shale, soft in places and sandy in places

#4148

0-12 overburden – red & gray sandy clay & gravel 12-33 reddish shale

#4149

0-12 overburden - clay & small rocks 12-37 fractured reddish sandstone 37-62 red & gray shale, some soft

#4713

0-21 red clay 21-35 coal & black shale 35-54 gray shale 54-55 brown sandstone

#4714 0-21 red clay 21-35 coal & black shale

#4715

0-27 red clay 27-37 black coal shale

#4716 0-27 red clay 27-33 coal & black shale

#4717 0-29 red clay 29-35 black coal shale

#4718 0-22 red clay 22-35 coal & black shale

#4719 0-22 red clay 22-25 coal & black shale

#4720 0-21 red clay 21-36 coal & black shale #4721 0-19 red clay 19-36 coal & black shale

#4722 0-20 red clay 20-36 coal & shale

#4723 0-28 red clay 28-38 coal & black shale

#4724 0-28 red clay 28-34 coal & black shale

#4725 0-28 red clay 28-29 coal & black shale

#4726 0-28 red clay 28-35 coal & black shale

AP	PF	N	DI	Х	7	
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Chalk River, Ontario, Canada, K0J 1J0 (613) 584-3311 (via Deep River) (613) 687-5581 (via Pembroke)

> DISTRIBUTION 1C.

11 March, 1976

Miss Heather Cross, Hydrogeologist, Nova Scotia Department of the Environment, P.O. Box 2017, HALIFAX, Nova Scotia.

Dear Miss Cross:

Tritium and deuterium data for the water samples from Stellarton that you submitted last fall are listed in the attached table.

The tritium concentrations give some idea of the time scale of infiltration. The shallow samples - 16, 14 have tritium contents characteristic of precipitation of the last few years in this region. Samples 19 and 31 show the admixture of some water of the last 20-year period to older tritium-free water. All samples from below 75 ft. depth have 0 \pm 10 Tritium Units indicating more than 20 years since any of this water was in the atmosphere. Carbon-14 analyses would be required to say anything more. The negative tritium values result from the statistical distribution of counting data and are to be taken as zero tritium content.

The mean deuterium content of all the ground water samples is - 63.4 $^{\circ}/_{\circ\circ}$ with a small standard deviation of ± 2.2 $^{\circ}/_{\circ\circ}$. This concentration is quite similar to that of local precipitation of the cool part of the year. There is no significant difference in deuterium content of old and young water. Thus, the isotope data indicate that these saline waters are not entrapped or intruded marine water (0 % of b) but probably normal recharge water leaching out deposits of marine (or other) salts.

...2

H. Cross

The deuterium content of the East River reflects the presence of more summer precipitation than is present in the ground waters, presumably due to greater surface runoff from summer storms. The water in Pictou harbour must have a relatively small proportion of sea water in view of the similarity of its deuterium and tritium contents to those of the East River. The tritium and deuterium contents of water from the Northumberland Strait differ from those of true sea water $(0^{\circ}/_{\circ\circ} \delta D, 10-15 \text{ TU})$ because of the influence of continental drainage.

I did not think that ¹⁸O values would add to the information obtained from the deuterium results. They would indicate if the present ground waters had undergone significant evaporation before infiltration. However, the low D values, similar to those of local precipitation, indicate that such evaporation is unlikely. Mr. R.E. Jackson looked over the chemical and isotope data briefly when he was here a few weeks ago. You may wish to talk to him about the significance of the chemical data, although he did not have a change to go into them in great detail.

I think these results illustrate the sort of information you can get from isotope measurements. I doubt if further work at this particular site will give more information unless you want to delineate the old and the recent water more closely. I will be glad to have any comments you may have on these results and the significance of my interpretation of them.

Yours sincerely,

R.m. Srom

R.M. Brown, Environmental Research Branch.

RMB/dt Encl.

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े हेर्न्		Well	Casina	TABLE OF	SAMPLES	-	: ۲ پ ۹ پ
lumber	Name	Depth	Length	* Bedrock	Comments		63
7-C	Alex Sutherland	125	45	ŝ	Drilled well not in park, quality fairly normal, low F	-7.±6.	- 89 9 1
A-C	Plymouth School	300		S	High NaCl, F, deepest well	10±5	-63
	Scott MacDonald	22'		S	Dug well, normal, in park	55±8	-65
0	Harry Conway	14		S	Dug well, salty, in park	65±5	-64
C L	Earl Kellock	30 20 20 20 20 20 20 20 20 20 20 20 20 20		S	Dug well, 'possible road salt, in park	69±7	-64
	George MacKenzie	56		S	high NaCI, F, HCO ₃ , not in park	20±7	- 62
20	Sheldon Stewart	138		S	High Na, HCO ₃ , F, near park	- 5# 6	-63
2	Ralph Foote	175	100	S	High NaCl, F, shallower drilled well near park	-1±6	- 26
2-2	G. Thompson	78		S	Quality normal, but near boundary of problem wells	10±6	-62
.)- -	Alex MacDonald	25.2		M	Dug well over Windsor Group, Bedrock	28±5	-63
2-1 1	N. Williams	75		M	Drilled well in Windsor Group Bedrock	9∓0	-64
0-1	East River		and the second secon	S	Surface water at park bridge.	48±5	-48
1-1	Sea Water				Seawater – freshwater mixture from Pictov Harbour.	45±9	15-
V-2	Sea Water				Seawater from Northumberland Strait	2 9± 7	113
		196	7-69 Precit	oltation:	Halifax: Summer Ave. (½ year) Winter Ave.	-	- 37
; - Stel	llarton Series				Fredericton: Summer Ave.		-20
- Win	dsor Group				Cander. Summer Ave.		76- 1-94
					Winter Ave.		- 74



Mr. John F. Jones Chief, Groundwater Section Water Planning and Management Division Department of Environment Province of Nova Scotia

Dear Mr. Jones:

RE: Flouride in well water Plymouth area, Pictou County

I am writing with reference to our consultations with respect to the identification of flouride in well water in the Plymouth area of Pictou County last Fall.

As you know, the matter was referred to our Division of Dental Health Services, and since that time the Director of the Division, with the assistance of his staff has been looking into the possible ramifications of the presence of flouride in drinking water, on the basis of on-site visits and investigations.

By way of update the Dental Hygienist has now completed examinations of 77 school children at the Dr. W.A. MacLeod School in Riverton. These children, ranging in age from 5 to 12 years of age were found to be essentially free of dental fluorosis. On the basis of a scale ranging from normal through questionable, very mild, moderate, to severe, all except three were considered to be in the normal range. In three instances questionable fluorosis was identified. Individuals in this category could only be identified on the basis of examination by a highly trained examiner. Any relationship to exposure to high concentrations of flouride in these instances is also questionable.

Further attention to this situation will be maintained by the Division of Dental Health Services. Certainly at the present time there would appear to be no cause for concern.

Yours truly,

C.E. Tupper, P.Eng. Administrator Health Engineering Services

CET:bah