

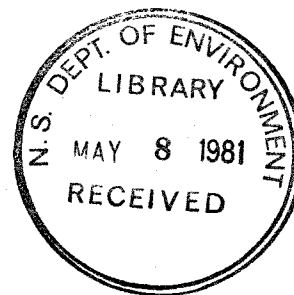
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GROUNDWATER SURVEY
FOR
THREE BROOKS
PICTOU COUNTY
NOVA SCOTIA

NOVA
SCOTIA
DEPARTMENT

PROVINCE OF NOVA SCOTIA
DEPARTMENT OF THE ENVIRONMENT

PROVINCE OF NOVA SCOTIA
DEPARTMENT OF THE ENVIRONMENT
WATER PLANNING AND MANAGEMENT DIVISION
PRELIMINARY REPORT



**GROUNDWATER SURVEY
FOR
THREE BROOKS
PICTOU COUNTY
NOVA SCOTIA**

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by:

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GROUNDWATER SURVEY FOR
THE THREE BROOKS AREA, PICTOU COUNTY
NOVA SCOTIA

A B S T R A C T

Sand and gravel deposits covering a small area have been delineated in the Three Brooks community. Test drilling and pumping on such a deposit located at the MacCarthy property indicate an excellent potential for high yields. The quality of the water from these deposits is generally good and they could be used for water supplies.

Several of the residents obtain their water supply from shallow, dug wells constructed in till. Most of these wells are subject to surface contamination and, in periods of prolonged drought, often fail to provide adequate yields for domestic supplies. The proper construction of dug wells in areas of sandy till and sand and gravel deposits should improve this situation.

The groundwater from bedrock aquifers such as shale, siltstone and sandstone located east of Highway 106, is of poor quality due to the occurrence of excessive amounts of chloride salts. Those located west of Highway 106, however, contain water of suitable quality. Although groundwater potential from bedrock aquifers for a large supply is small, sufficient volume is available for domestic purposes.

I N T R O D U C T I O N

PURPOSE AND SCOPE OF THE INVESTIGATION

The residents of the Three Brooks area have been experiencing unusually high chloride concentrations in their well water supply systems. In response to this problem, the Nova Scotia Department of the Environment initiated a hydrogeological study during 1974 and 1975. The primary purpose of the study was to determine the areal extent and seriousness of the chloride problem, and to evaluate the quality and quantity of the groundwater resources in the Three Brooks area. A water quality survey provided basic information on the groundwater chemistry of the bedrock and surficial aquifers. A comprehensive test drilling and pump testing program was used to assist in the geochemical interpretation, and in the location and evaluation of potential aquifers for use as an alternative groundwater supply.

LOCATION

The Three Brooks area is located in the northwestern section of Pictou County, on the westernmost extent of the Caribou Peninsula. The Three Brooks community is situated four miles northwest of the Town of Pictou along Highway 6 (Map 1 in pocket). The map area is included in the northeast portion of the New Glasgow map sheet 11-E-10 west half and 11-E-10 east half.

CLIMATE

The mean annual precipitation for Pictou is about 42.0 inches based on 30 years (1940-1970) of records. About 37 percent of this falls during the growing season. Total mean annual precipitation consists of 31.9 inches of rain and 80.9 inches of snow (Hennigar, 1968, p.3).

The mean annual temperatures range from a low of

-11.1° C in February to a high of 23.9° C in July. The overall mean temperature for Pictou is 6.1° C. The growing season in this area ranges from 180 to 190 days and the frost-free period from 100 to 120 days (Hennigar, 1968, p.3).

DRAINAGE AND PHYSIOGRAPHY

A watershed area of approximately eight square miles is drained by a brook system known as Three Brooks (Map 1). The central and largest of the three brooks is called Sheriff Brook, while the remaining two are unnamed. All three brooks run from the west-southwest to east-northeast and empty into Caribou Harbour. High tides reach inland to a point 1200 feet north of the Three Brooks Road and cross the MacKenzie Road, 0.6 mile north of the MacKenzie Road-Three Brooks Junction (Map 1). Topographic elevation ranges from a high of 250 feet in the western extent of the drainage area, to sea level in the east, along the Caribou Harbour.

G E O L O G Y

STRUCTURAL GEOLOGY

The structural trend of northwestern Pictou County is east northeast to northeast, which conforms with the trend of the northeastern Appalachian geosyncline and orogenic belt. A broad northeast plunging Scotsburn anticline and a number of high angle faults are the main structural elements of the map area (Map 1).

Dips on the limb of the Scotsburn anticline range from 25° to 55° to the southeast and from 20° to vertical and slightly overturned to the north. To the northeast, the structure plunges under the Northumberland Strait (Gillis, 1964, P. 96).

The Three Brooks area lies on the northern limb of the Scotsburn anticline. The Pictou-Riversdale contact lies north of the Three Brooks road striking southeast and crossing the Three Brooks road, approximately two miles east of the Three Brooks-Route 6 Junction. The strata of the Riversdale Group strike east-southeast and dip 13° to 18° north-northeast. The overlying Pictou Group sediments strike easterly and dip approximately 8° north-northeast.

LITHOLOGY AND STRATIGRAPHY

In the northwestern Pictou County area the Boss Point Formation conformably overlies the Millsville conglomerate both of the Riversdale Group. The Boss Point-Millsville contact is transitional with the conglomerates of the Millsville grading upward into the sandstones of the Boss Point Formation. Angular discordances occur between the moderately-dipping sandstones and siltstones of the

Riversdale Group and the overlying low-dipping basal pebble conglomerate of the Pictou Group (Gillis, 1964, p. 53-57).

Detailed stratigraphical logs were prepared for the Three Brooks area based on continuous sampling of drill cuttings over five foot intervals and E-log records of two test wells. Graphical representation of detailed logs are shown in Figure 1 (in pocket).

Of a total of 888 feet of bedrock drilled, shale comprised 63% of the vertical section, siltstone 19% and sandstone 18%. Specifically, dark brown, red-brown and minor amounts of green, slightly calcareous, brittle to muddy textured shale predominated. Brown, red-brown and green interbedded sandstone and siltstone composed the remaining bedrock constituents. Individual layers ranged from a few inches to several feet in thickness.

Hydrocarbons and fossiliferous carbonaceous material was evident at various depths in the stratigraphic column.

E-log records of well #6 indicate a marked change in resistivity values at a depth of approximately 215 feet. The lower resistivity values between 215 feet and 410 feet coincide with a change in bedrock conditions from interbedded shales, siltstones and sandstones to mainly shales. More likely, however, the low resistivities are due to a change in water chemistry from a fresh or brackish water to a highly saline water, lower in the water column. This is discussed in a later section of this report.

Drill cuttings of the test wells indicate a bedrock type similar to the primary constituents of the Boss Point Formation of Riversdale Group. However, detailed petrological studies were not conducted on the cutting samples, nor was any of the fossiliferous material dated. Therefore, it is not known whether or not drilling operations have actually penetrated any bedrock constituent belonging to a sedimentary group other than Riversdale, i.e., Windsor Formation. There was no evidence in the drill cuttings to suggest the presence of salt deposits within the limits of the drill holes.

The presence of trace amounts of gypsum stringers are probably a result of groundwater dissolution, along fracture or bedding planes.

SURFICIAL DEPOSITS

Detailed well logs indicate the surficial deposits at the Three Brooks area consist of sandy till, silty till, clay till and stratified sand and gravel deposits, with an overall thickness ranging from 22 to 167 feet. Of a total of 376 feet of overburden drilled, 51% of the vertical section consisted of a silty till having varying amounts of cobbles and pebbles set in a compact, brown, silt and clay matrix. Sandy till comprised 25% and consisted of a mixture of fine gravel and red-brown, loosely consolidated sand and silt matrix. Clay till, encountered in test hole #3, accounted for 5.3% and consisted of a 20-foot thick compact mixture of boulders, cobbles and pebbles in a red-brown clay matrix.

Stratified sand and gravel deposits 1.5 to 30 feet thick, generally occur at 8 to 45 feet below ground surface. These deposits were found overlying bedrock in test wells

#4, 5 and 6. The extent of the sand and gravel deposits are not known, however, the presence of these deposits in well logs #3, 6, 18 and 22 (Table 1) and in test holes #1, 4, 5 and 6, suggest they occur throughout the area. The absence of these deposits in test holes #2 and 3, suggest these deposits are not laterally continuous.

H Y D R O L O G Y

WELL INFORMATION

Records of 26 drilled and 6 dug wells have been compiled and verified for reference (Table 1). The drilled wells are set in shale and sandstone to depths ranging from 82 feet to 265 feet. Well yields are reported to range from 2.5 to 10 igpm with water levels averaging 20 feet below ground surface. Casing lengths vary from 28 feet to 85 feet. The dug wells are assumed to be set in the overburden; however, it is possible that some of them may be bottomed in bedrock. They range in depth from 18.5 feet to 24 feet and are rocked to the surface with the exception of well #34 which is tiled to the surface. Well yields may be classified qualitatively as adequate or inadequate based on information obtained from the well owners.

The dug wells that are reported to go dry during the summer months are assumed to have a lower yield relative to those dug wells that maintain an adequate supply year-round. However, well depth and construction details are probably the major contributing factors (Table 1). Low yields suggest that wells #1, 4 and 28 are set in a silty till, whereas those wells with high yields (#39 and 8) are probably set in a sandy till.

During detailed hydrogeological investigations of the Three Brooks area, six test wells were drilled by the Nova Scotia Department of the Environment (Map 1, Figure 1, Table 2). Of these, five were drilled into bedrock and one drilled into sand and gravel deposits within the overburden. The well depths range from 64

to 410 feet below ground surface with casing lengths ranging from 52-300 feet below ground surface. Well yields range from less than 0.5 to 5 igpm with water levels varying from 11 to 32 feet below surface. Further water level monitoring programs are being conducted. However, for the purpose of this report, the data is not included.

PUMP TESTS

Three short 10-hour pump tests were conducted on test wells #2, 4 and 5. Step drawdown tests were conducted prior to each pump test. The purpose of the pump tests were (1) to approximate the safe yield of the wells, (2) to observe water chemistry response to pumping stress and (3) to examine the relationships between groundwaters within bedrock and overburden aquifers. The test data are shown in Tables 3, 4 and 5. Graphical representation and interpretation of the test analyses are given in figures 2, 3 and 4 and the results are listed in Table 6. The coefficient of transmissibility of 15.1 igpd/ft in test well #4 and 44.7 igpm/ft in test well #2, indicate that the deep bedrock wells should yield between 1 and 2 igpm for 20 years of continuous pumping. Due to minor technical problems, interpretation of the drawdown curve for pump test #2, well #5, is difficult. The determined 20 years safe yield of 0.3 igpm should be considered conservative, due to the fact that the well reached equilibrium after only 210 minutes of pumping at a rate of 0.5 igpm. The sand and gravel aquifer was developed by a high pressure air jet for approximately 4 hours. It is expected that further development of this aquifer over a long period, perhaps 24 hours, will increase the present well yield to as much as 5 igpm.

SALT SOURCES

Extensive folding, faulting and fracturing of the bedrock during the formation of the Scotsburn Anticline may have provided a mechanism for salt water intrusion to occur in the underlying bedrock of the Three Brooks area.

According to the Ghyben-Herzberg coastal aquifer relation, the water table and/or piezometric surface (a) must be above sea level and (b) slope downward toward the ocean. Without these conditions, sea water will advance directly inland. Given conditions (a) and (b), the fresh/salt water interface occurs at approximately 40 times the height of the fresh water above sea level (Todd, 1959).

Preliminary information indicates that the piezometric surface in the Three Brooks area lies approximately 50 feet above the mean sea level and slopes toward the ocean. This suggests the salt/fresh water interface, if present, lies at a depth in excess of 1,500 feet.

Gillis (1964) suggests that the Windsor Group sediments appear to be in fault contact with the Boss Point Formation of Riversdale Group sediments in the northern part of Pictou County. The depths at which the contacts lie are not known. It is possible that saline water originating from Windsor bedrock has penetrated Riversdale sediments by fault contact, fractures, solution, salt diapir development or by some other mechanism. In addition, it is also possible that Riversdale Group sediments may contain salts.

C H E M I S T R Y

The chemical analyses indicate that of 26 domestic, drilled wells sampled during the survey, 10 have chloride concentrations greater than 250 mg/l. Of the remaining 16, 10 have chloride concentrations greater than an assumed background level of 60 mg/l. Of the six test wells, chemical analyses indicate that with the exception of test well #5, all have concentrations of chloride exceeding 250 mg/l (Table 8) the acceptable limit suggested in the Canadian Drinking Water Standards and Objectives, 1968. Interpretation of water samples taken from the dug wells was complicated and difficult due to interference from highway salts, animal wastes and stagnant water conditions. The location and reference numbers of these samples are shown in Map 1.

Tables 7, 8 and 9 summarize the chemical concentrations for the major ions for all the sample analysis in both mg/l and meq/l. The data indicates that the major portion of chlorides are associated with sodium. The remaining chloride is closely associated with calcium and magnesium.

Test drilling results indicate that there is an increase with depth of all major ions, with the exception of alkalinity. Alkalinity decreases slightly with increasing depth. Figures 5 to 9 (in pocket) show a plot of the major ion concentrations expressed in meq/l, versus well depth in test wells #1, 2, 3, 4 and 6. These graphs suggest the presence of NaCl, CaCl₂ and MgCl₂ with the major salt being NaCl.

The fact that chloride concentrations increase with increasing depth suggest that the salts are derived from a source within the bedrock and not from a surface source such as road salt. Additionally, test well #3 (maximum chloride concentration 2520 mg/l) is at least 1100 feet from highway #6 and 850 feet from the Three Brooks Road, the nearest source of highway salt. It is unlikely that road salt from these highways would travel such long distances to affect this well.

Test well #5 penetrated sand and gravel deposits between 48 and 64 feet below surface. Chemical analyses (Table 9) of groundwater contained in the sand and gravel indicated an average chloride concentration of 120 mg/l. The average concentrations of iron (0.6 mg/l), manganese (1.0 mg/l), colour (25 TCU) and turbidity (15 JTU), have slightly exceeded the recommended limits of 0.3 mg/l for iron, 0.05 mg/l for manganese, 15 TCU for colour and 5 JTU for turbidity in the Canadian Drinking Water Standards and Objectives, 1968. The high colour is probably associated with the excess iron and manganese in the groundwater. Excess turbidity may be associated with the inorganic suspended material. With minor treatment, the water contained in the sand and gravel deposits can be brought to within the acceptable limits outlined in the above-mentioned standards, and therefore, made suitable for human consumption.

The sandy till in front of Mr. L. MacCarthy's residence provides groundwater of sufficient quality to permit the development of a domestic water supply which will at least provide sufficient quantity for drinking and cooking. The water is of good chemical quality, suitable for drinking purposes (Table 7, #38).

Trilinear plots (after Piper, 1944) of the water analyses are given in figures 10 and 11. In these diagrams, the major cations in groundwater (calcium, magnesium and sodium plus potassium) are given as per cents of total meq/l in one triangular field; in the other, the major anions (carbonate plus bicarbonate, chloride and sulphate) are given as per cents of total meq/l; and the combined chemistry is plotted in the diamond-shaped field (Trescott, 1968).

Figure 10 represents the trilinear plot of the water chemistry of those samples taken from the domestic drilled and dug wells. The plot indicates a marked difference in water types between those wells located west of highway 106 and those located east of it. The wells west of the highway exhibit a groundwater similar to that of a freshwater type as opposed to that of a saline type east of the highway.

Figure 11 represents a trilinear plot of the water chemistry of those samples taken during the pump tests conducted on test wells #2, 4 and 5. The chloride concentration in test well #4 remained relatively constant throughout the test, decreasing only slightly from a high of 4130 mg/l at 0 minutes to 3880 mg/l at 600 minutes. The water is classified as one having "primary salinity" (after Palmer, 1911).

Chloride concentrations in test well #2 varied from a high of 1250 mg/l at 0 minutes decreasing to a low of 186 mg/l at 600 minutes. This substantial change in chloride concentrations suggests a mixing of two or more groundwater types, one characterized by primary salinity, the other by primary alkalinity.

It is apparent that the fresh water is higher in the stratigraphic column than the saline water. Since the pump was set at a depth of 180 feet below ground surface the first samples at 0 and 5 minutes were drawn from this depth range. With increasing drawdown, the fresh water higher in the water column was drawn toward the intake. It must be considered, however, that density stratification in the well may have taken place. Further to this, however, the results of chemical analyses of water samples taken during drilling operations, indicated an increase in chloride concentrations with increasing depth. At no time was there an opportunity for stratification to occur within the water column in the well during drilling operations, adding support to the conclusion that fresh water lies higher in the stratigraphic column.

The change in chemical composition further implies that test well #2 has penetrated both fresh and saline groundwater aquifers or that dilution, dispersion and/or density stratification of the water column has occurred throughout the bedrock and that separate confined aquifers are not present. The decrease in chloride concentration with decreasing depth probably reflects processes of upward dispersion and dilution effects from near surface, local fresh water flows.

Analytical results of the pump test samples of test well #5 indicate a consistent chemical composition characterized by primary alkalinity with strong salinity influence. The average chloride concentration of 120 mg/l is higher than the assumed background levels (Trescott, 1968, P. 151). However, it is relatively low in comparison to bedrock groundwaters. The presence of high

chlorides suggests that some mixing between the water contained within the sands and gravels and that within the bedrock has taken place.

Analyses of groundwater samples collected in zones of sea water intrusion may show a chemical composition differing from a simple proportional mixing of sea water and groundwater. Modifications in composition of sea water entering an aquifer can occur due to: (a) base exchange between the water and the minerals of the aquifer (b) sulphate reduction and substitution of carbonic or other weak acid radicals, and (c) solution and precipitation (Todd, 1959).

Revells (1941) recommended the chloride bicarbonate ratio as the criterion to evaluate sea water intrusion. It was indicated that the chloride-bicarbonate ratio, as well as the total salinity will increase as the source of the chloride, in this case, the coast, is approached.

Similar results were obtained from analyses done of groundwater sampled from selected wells in the Three Brooks area. Table 10 indicates an increase in the chloride/(carbonate + bicarbonate) ratio and total salinity (as NaCl) as the coastline along Caribou Harbour is approached. Well depth considerations were not taken into account, however, the depth range varies only slightly from 90 to 125 feet. The pattern of increase is not entirely true for all wells in the Three Brooks area. For example, well #29 has a $\text{Cl}/(\text{CO}_3 + \text{HCO}_3)$ ratio of 3.4; however, there is generally an increase in this ratio from west to east. There is significant increase in the

$\text{Cl}/(\text{CO}_3 + \text{HCO}_3)$ ratio and total salinity between those drilled wells located west of highway 6 relative to those located east of the highway. The increase in salinity toward the coast suggests that the source of the salts is a result of salt water intrusion of the bedrock. However, an examination of the $\text{Cl}/(\text{CO}_3 + \text{HCO}_3)$ ratio with increasing depth in test well #6, is shown in Table 11. It can be seen that the $\text{Cl}/(\text{CO}_3 + \text{HCO}_3)$ ratio and total salinity increases rapidly with increasing depth. The high ratios of sample #5 - 7 suggest the source of the saline water is at a relatively shallow depth. From this it can be concluded that deep wells drilled west of highway 6 may possibly encounter saline groundwater.

Primarily, high concentrations of salts in bedrock groundwater in Nova Scotia are often associated with Windsor sediments. Groundwater within these sediments is known to contain salts of NaCl , CaCl_2 and CaSO_4 and alkalinities are generally high. In other areas of the Province in which Windsor bedrock is predominant, sulphates (SO_4) are often present in anomalous concentrations (Trescott, 1968, P. 82). Chemical data in tables 8 and 9 indicate an absence of SO_4 and alkalinities are generally low, possibly a situation more characteristic of salt water intruded bedrock. The occurrence of hydrocarbons and fossiliferous carbonaceous material is indicative of a strong reducing environment. It is possible then, that sulphates have been reduced. Also, their concentrations may have been diluted by fresh groundwater moving through a formation salt source. Therefore, it is likely that the saline characteristics of the groundwater of the Three Brooks area is due to the presence of salt deposits within the Riversdale or Windsor sediments and not a result of salt water intrusion of the bedrock. To arrive

at definite proof, further studies are necessary.

C O N C L U S I O N

1. Groundwater aquifers in the underlying bedrock in the Three Brooks area contain high concentrations of dissolved chloride salts. Chemical analyses indicate that of 26 domestic drilled wells sampled, 10 have chloride concentrations greater than 250 mg/l. Of the remaining 16, 10 have chloride concentrations greater than assumed background levels.

2. Analyses show that where chloride values are high, sodium concentrations are correspondingly high. Therefore, the greater part of the chlorides are associated with sodium. The remaining chloride is associated with calcium and magnesium.

3. Chemical analyses of water samples taken during test drilling operations indicate that chloride concentrations increase with depth. This suggests that the salt is not likely derived from a surface source such as highway de-icing salt. Also, the high chloride concentrations in test well #6, suggest the source of salts may be at a relatively shallow depth.

4. With minor treatment, the water contained in the sand and gravel aquifers can be brought to within the acceptable limits outlined in the Canadian Drinking Water Standards and Objectives, 1968.

5. The sandy till in front of Mr. L. MacCarthy's residence provides groundwater of sufficient quality to permit the development of a domestic water supply which will at least provide sufficient quantity for drinking and cooking. The water is of good chemical quality,

suitable for drinking purposes (Table 7, #33).

6. Drilled wells located to the west of highway 106 indicate a water similar to that of an alkaline type and are relatively free of excessive chloride concentrations.

7. Pump test results indicate that the coefficient of transmissibility of the bedrock aquifer ranges from 15.1 igpd/ft to 44.7 igpd/ft. It is expected that bedrock wells in the order of 100 to 150 feet in depth should yield between 1 and 2 igpm for 20 years of continuous pumping. With proper development the sand and gravel deposits are expected to yield at least 5 igpm.

8. Available information suggests that there are two possible sources of saline water in the bedrock aquifers of the area:

- (1) salt deposits contained within the underlying bedrock, and
- (2) salt water intrusion of the bedrock.

Sodium chloride is probably derived from a salt bed within the Boss Point Formation, or from the underlying deposits within the Millsville Formation, both of the Riversdale Group. However, the salts within the Riversdale Group may originate from a deeper source such as the underlying salt formations related to Windsor Group. Fault contact with underlying Windsor sediments is another possibility. However, the chemical data suggests the absence of typical Windsor sediments due to the lack of sulphates (SO_4) and low alkalinity.

R E C O M M E N D A T I O N S

1. Future domestic groundwater supplies for the Three Brooks Community should be obtained from the following groundwater reserves:

- (a) sand and gravel deposits contained in the overburden;
- (b) sandy till exposed at or near ground surface;
- (c) the bedrock aquifers situated west of highway 106.

2. This could be best achieved by:

- (a) the proper construction and development of a screened well drilled into the underlying saturated sand and gravel deposits contained in the overburden;
- (b) the proper construction of a dug well in a suitable location, preferably away from the Three Brooks Road and other possible sources of contamination, such as a septic field and agricultural wastes. The sandy till is better suited for dug well construction, due to the higher yield of this material;
- (c) the proper construction of a bedrock well located west of highway 106 and drilled to a depth not to exceed 150 feet below ground surface.

3. The Municipal Planning Board of the County of Pictou should restrict future rural development along that

portion of the Three Brooks Road outlined in the study area, unless suitable resources can be located and properly developed. Future development in this area depends upon the availability of suitable groundwater reserves.

4. The Nova Scotia Department of the Environment, Water Planning and Management Division, should carry out further hydrogeological investigations into occurrence of groundwater with high salt concentrations. Results from such studies carry economic, mineralogical and hydrogeological implications and enable the Department to further develop and document an important groundwater phenomenon.

A C K N O W L E D G E M E N T S

On behalf of the Nova Scotia Department of the Environment, I would like to express my thanks to the residents of the Three Brooks Community for their kind co-operation and assistance during the survey period.

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This paper was critically reviewed by Dr. C.L. Lin, P.Eng., of the Nova Scotia Department of the Environment and Mr. Ross F. McCurdy of the Nova Scotia Department of Health.

C O N V E R S I O N F A C T O R S

A N D S Y M B O L S

| | |
|---|---|
| 1 inch (in) | - 0.254 metres (m) |
| | - 2.540 centimetres (cm) |
| | - 25.40 millimetres (mm) |
| 1 foot (ft) - 12 in | - 3.048 m |
| | - 30.48 cm |
| | - 304.8 mm |
| 1 mile - 5280 ft | - 1.609 kilometres (km) |
| 1 square mile (mile ²) | - 2.390 square kilometres (km ²) |
| 1 acre - 43,560 ft ² | - 4.047 x 10 ³ square metres (m ²) |
| 1 cubic foot (ft ³) | - 0.02832 cubic metres (m ³) |
| -7.4805 U.S. Gallons(g) | - 28.317 litres (ℓ) |
| -6.233 imperial gallon (ig) | - 28,317 cubic centimetres (cm ³) |
| 1 imperial gallon (ig) - | |
| 1.2 U.S. gallon (g) | - 0.00454 cubic metre (m ³) |
| | - 4.5425 litres (ℓ) |
| | - 4542.5 cubic centimetres (cm ³) |
| 1 imperial gallon per minute (igpm) | |
| - 1.2 U.S. gallons per minute (gpm) | - 4.5425 litres per minute (ℓ/m) |
| 1 cubic foot per minute (ft ³ /min) | - 0.472 litre per second (ℓ/sec) |
| 1 cubic foot per second (ft ³ /sec or cfs) | - 28.3 litres per second (ℓ/sec) |
| 1 imperial gallon per day per foot (igpd/ft) | - 0.0149 m ² day |
| 1 imperial gallon per day per square foot (igpd/ft ²) | 0.0488 m/day |
| 1 pound per square inch (lb/in ² or psi) | - 0.0703 kg/cm ² |
| 1 pound per square foot (lb/ft ² or psf) | - 4.882 kg/m ² |
| 1 pound per cubic foot (lb/ft ³ or pcf) | - 16.02 kg/m ³ |

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APPENDIX A

FIGURES 2, 3, 4, 10, 11

FIGURE 2 PUMP TEST #1 THREE BROOKS TEST WELL #4

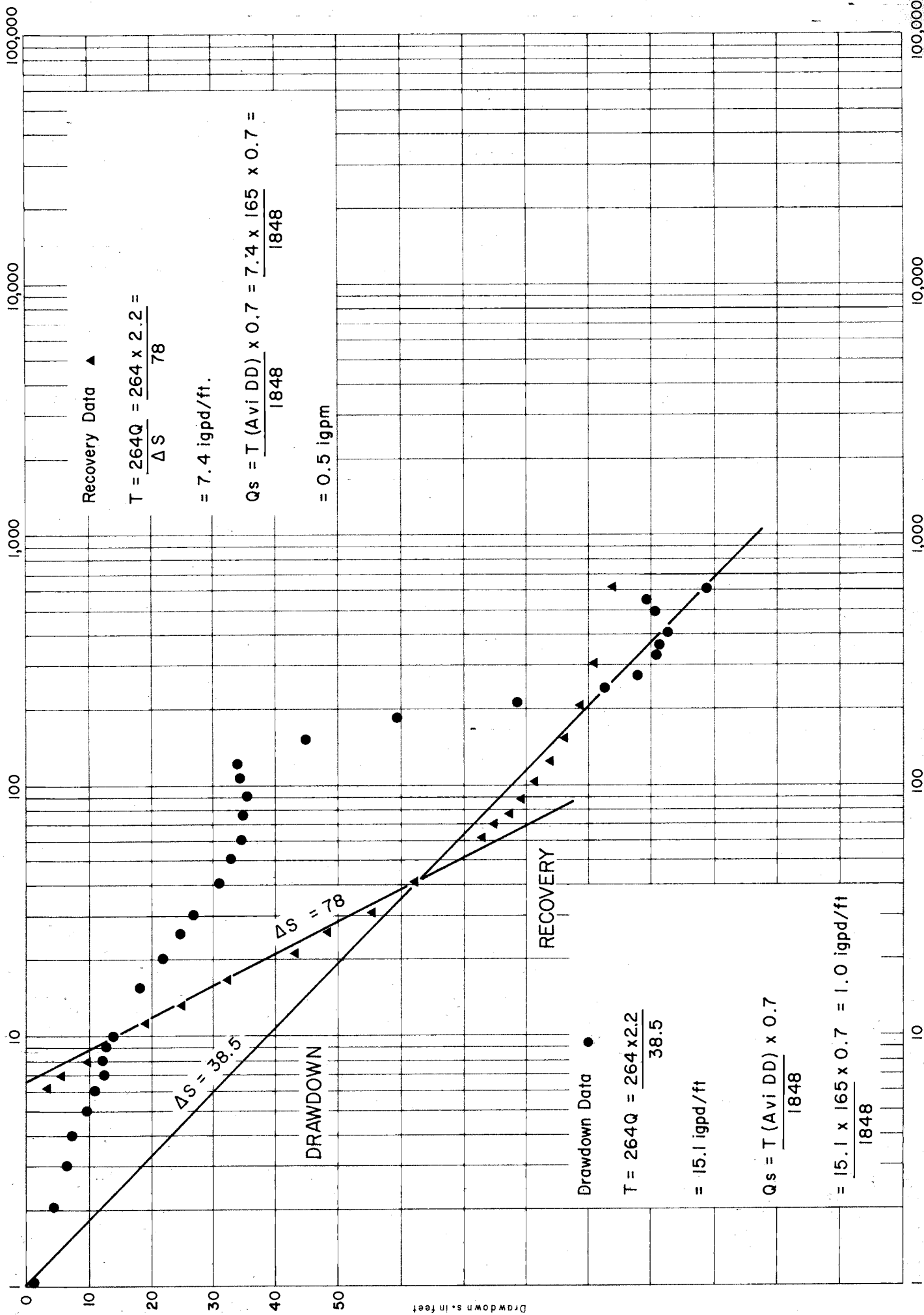


FIGURE 3 PUMP TEST #2 THREE BROOKS TEST WELL # 5

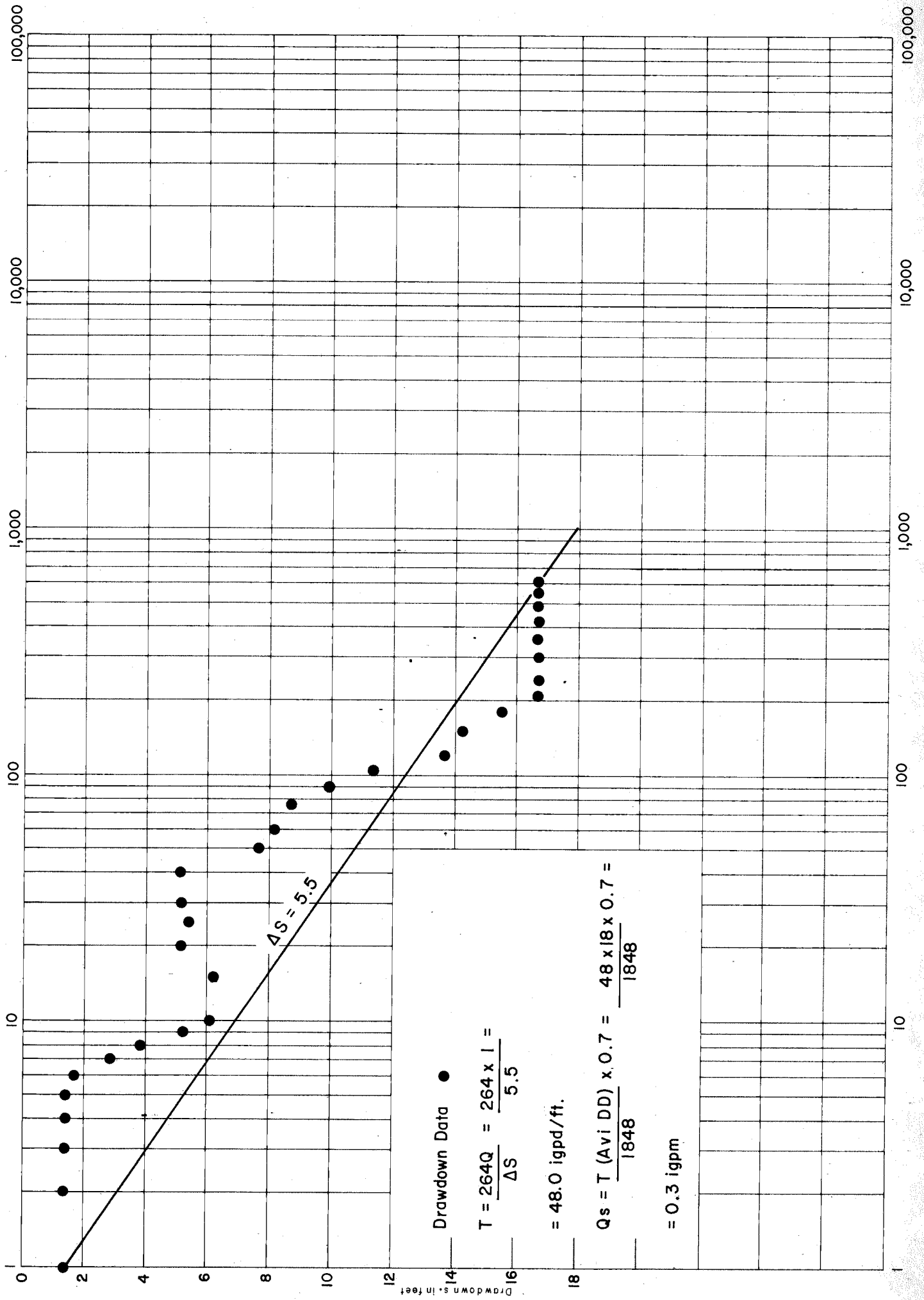
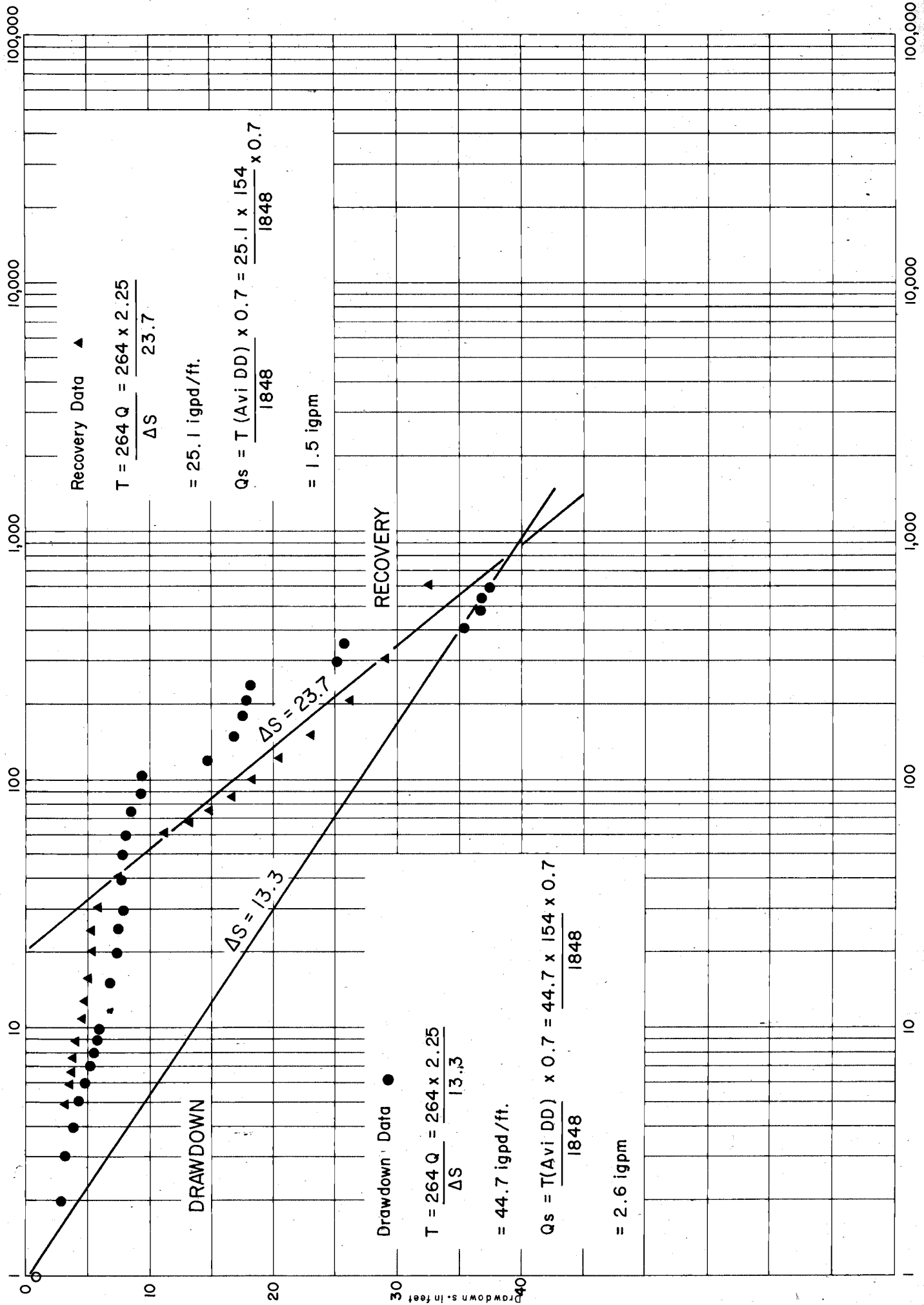
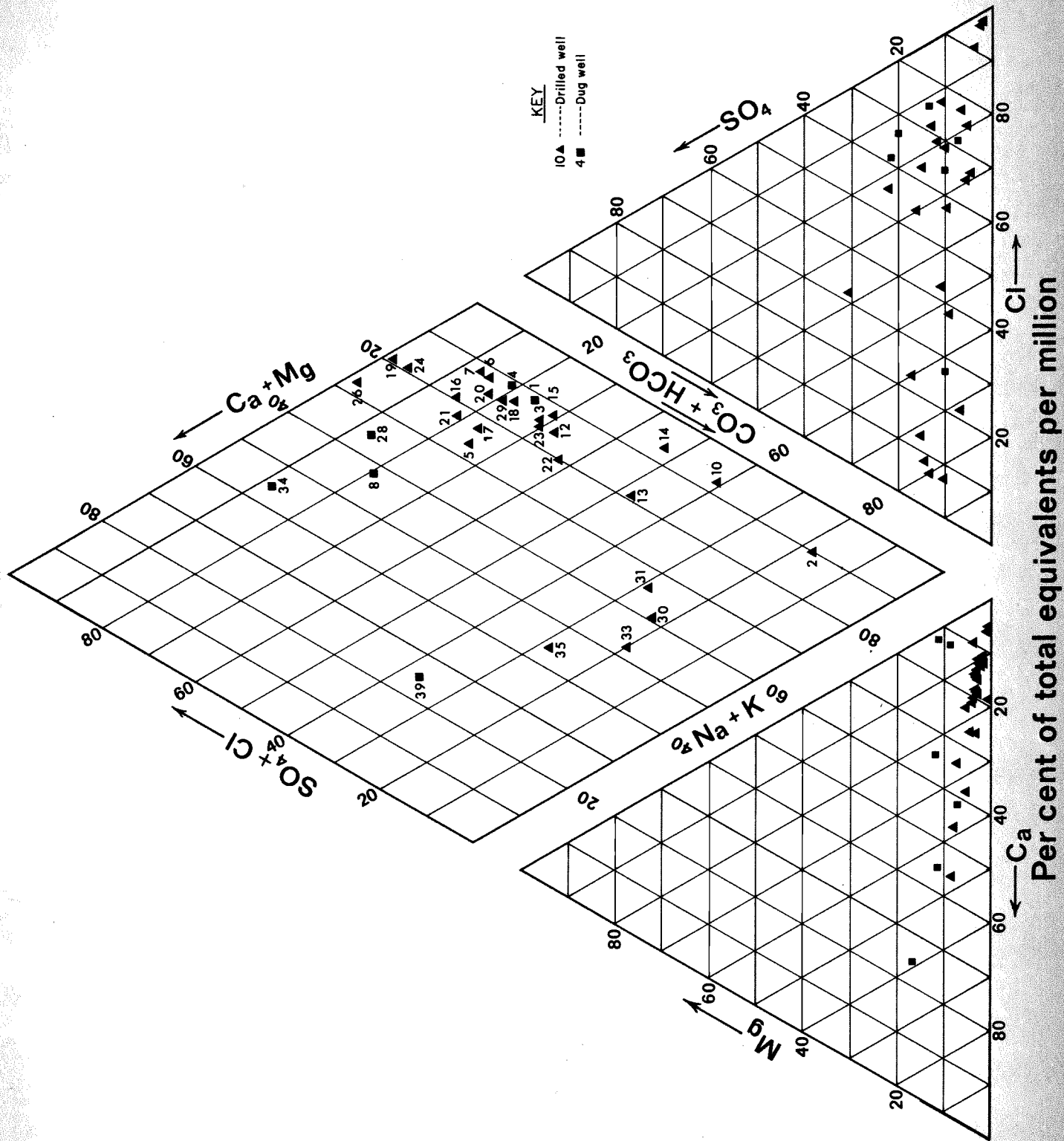


FIGURE 4 PUMP TEST #3 THREE BROOKS TEST WELL #2





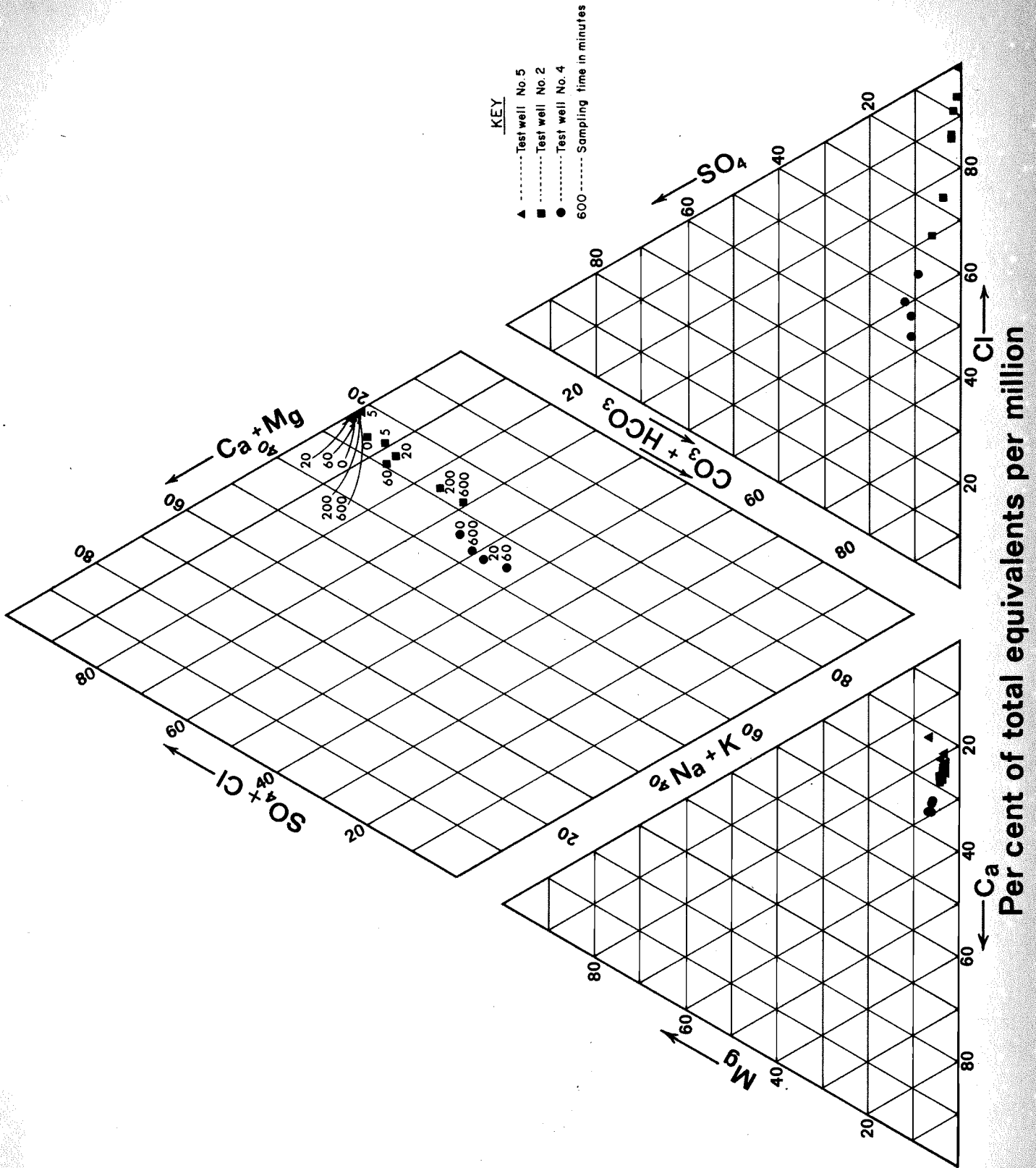


FIGURE 11

APPENDIX B

TABLES 1 to 11 inclusive

TABLE #1

11 E

Page 1

| Well No. | M.T. | Ref. Map | S.T. Map | Year Drilled | Owner | Driller Lic. No. | Well Depth (ft.) | Water Depth (ft.) | Hole Dia. (in.) | Csg. Lgth. (ft.) | Use Quality | Pump or Bail Test | Lithologic Log and Remarks |
|----------|------|----------|----------|--------------|--------------------------|------------------|------------------|-------------------|-----------------|------------------|-----------------|---|---|
| 15 | 74 | C | 10 | '68 | Heighton | 4 21 | 78 82 | 20 | 4 | 5 | D slt | 3 gpm - 1 hr DD-82' Rec - 20' | 0-30 dr 30-50 cl 50-82 sh |
| 24 | 74 | C | 10 | '73 | MacCarthy, L. | 5 | 140 | 18 | 6 | 77 | D slt | 7 gpm - 1 hr DD - 140' - 1 hr Rec - 40' - 20 mins | |
| 26 | 74 | C | 10 | '66 | MacCarthy, Jack (Tom) | 6 | 185 | 35 | 4 | 77 | D slt | 4 gpm - 1 hr | 0-80 till 80-185 bedrock (sandst.?) many different colours, cl, sd, sh |
| 3 | 74 | C | 10 | '66 | Baird, Ed. | 73 | 92 | 25 | 4 | 80 | D slt | 4 gpm | 0-92 cl, sd, sh |
| 14 | 74 | C | 10 | '52 | MacCarthy, Laurie | 73 | 109 | 20 | | | D | | |
| 19 | 74 | C | 10 | | Hayman (Sch. Hse.) | 4 | 265 | 45 | | | P slt | 3 gpm DD- 97' - 1 hr Rec - 67' - 10 mins | 167-265 sh |
| 20 | 74 | C | 10 | | Fraser, Jim | 73 | 78 | | | | D slt | | |
| 21 | 96 | C | 10 | '44 | Munro, R. | 11 | 94 | | 5 | 28 | D slt oil | 2.5 gpm | 0-32 dr 32-94 cl & ss |
| 39 | 74 | C | 10 | | MacFarlane, R. | | 107 | | 6 | | D slt | 2.5 gpm | 32-94 cl & ss |
| 5 | 96 | C | 10 | '50 | Usher | 73 | | | | | | | |
| 10 | 74 | C | 10 | | Young, S. | 21 | 98 | 10 | 4 | 47 | D | 10 gpm | 0-28 cl; 28-85s 85-98 ss |
| 12 | 74 | C | 10 | | Young, A. | | 109 | 25 | | 39 | D | | bedrk at 34' (possibly ss) |
| 13 | 74 | C | 10 | | Shanty Rest. | | | | | | | | |
| 16 | 74 | C | 10 | | MacFarlane, J. | 73 | 98 | 20 | | 65 | D slt | | |
| 17 | 96 | C | 10 | | Wilda Landry | | 99 | | 4 | 65 | | | |

| Well No. | M.T. | Ref. Map | S.T. Map | Year Drilled | Owner | Driller Lic. No. | Well Depth (ft.) | Water Depth (ft.) | Hole Dia. (in.) | Csg. Lgth. (ft.) | Use Quality | Pump or Bail Test | Lithologic Log and Remarks |
|----------|------|----------|----------|--------------|---------------|------------------|------------------|-------------------|-----------------|------------------|-------------|---|---|
| 18 | 96 | C | 10 | 73 | Williams, N. | 2114 | 5 | 4 | 34 | | | 5 gpm - 1 hr Rec 40' - 1 min DD-50' - 1 hr | 0-8 mud; 8-22 gra 22-50 red sh 50-114 gr sh |
| 22 | 74 | C | 10 | 71 | Lovett, E. | 21130 | 25 | 4 | 85 | | | 3 gpm - 1 hr DD-80' - 20 mins Rec-30' - 35 mins | 0-30 cl 30-50 loose grnc 50-75 sh; 80-133 ss |
| 23 | 74 | C | 10 | | Shea, Fred | 100 | | | | | | | |
| 29 | 84 | D | 10 | | Nichol | | 96 | 20 | | | | Csg. Lgth: Shallow | |
| 30 | 75 | C | 10 | 40 | Matheson, H. | | 90 | | | 30 | | | |
| 31 | 75 | C | 10 | 40 | Matheson, R. | 2 | 70 | to | 90 | | | feet - well depth | |
| 33 | 94 | C | 10 | 69 | MacCarthy, G. | | 85 | | | | D | | |
| 35 | 94 | C | 10 | | Ross, Roy | | 200 | | | | D | | |
| 6 | 74 | C | 10 | 73 | Pitts, Paul | 2125 | 20 | 5 | 65 | | D | 4 gpm - 1 hr DD-75' - 1 hr Rec-70' - 1 min | 0-62 mud, bldrs quicksand 62-125 grey sh |
| 7 | 84 | C | 10 | 55 | Pitts, Leo | | 125 | | | 80 | D | | |
| 2 | 74 | C | 10 | 73 | George B. | | 98 | | | | D | | |

| Well No. | M.T. | Ref. Map | S.T. Map | Year Drilled | Owner | Driller Lic. No. | Well Depth (ft.) | Water Depth (ft.) | Hole Dia. (ft.) | Csg. Lgh. (ft.) | Use | Quality | Pump or Bail Test | Lithologic Log and Remark |
|---|------|----------|----------|--------------|----------------|------------------|------------------|-------------------|-----------------|-----------------|-----|----------------------------|-------------------|---------------------------|
| 21' | 96 | C | 10 | | Munro, R. | | 21 | 7 | 3 | R | D | Adequate yield | | 0-21 sandy till (assumed) |
| 8 | 96 | C | 10 | | MacKenzie | | 24 | 10 | 3 | R | D | Adequate yield | | 0-24 sandy till (assumed) |
| 1 | 74 | C | 10 | | MacCarthy, T. | | 28 | 24 | 4 | R | D | Inadequate yield | | 0-28 cl till (assumed) |
| 4 | 96 | C | 10 | | Hartling, L. | | 18 | 10 | 6 | R | D | Inadequate yield in summer | | 0-18.5 cl till (assumed) |
| 28 | 84 | D | 10 | | MacFarlane, R. | | 20 | | | R | D | Inadequate yield in summer | | cl till (assumed) |
| 34 | 94 | C | 10 | | Faulkner | | 24 | | | T | D | Adequate yield | | 0-24 sandy till (assumed) |
| <p>Legend: R = rocked T = tiled cl = clay gra = gravel sh = shale ss = sandstone sd = sand</p> <p>gpm = gallons per minute DD = drawdown Rec = recovery slt = salt</p> | | | | | | | | | | | | | | |

TABLE # 2

TEST WELLS

| Well No. | M.T. | Ref. Map | S.T. Map | Year Drilled | Owner | Driller Lic. No. | Well Depth (ft.) | Water Depth (ft.) | Hole Dia. (in.) | Csg. Lgth. (ft.) | Use Quality | Pump or Bail Test | Lithologic Log and Remarks |
|---|------|----------|----------|--------------|------------|------------------|------------------|-------------------|-----------------|------------------|-------------|-------------------|----------------------------|
| Test Well # | | | | | | | | | | | | | |
| TB 1 | | | | '75 | N.S.D.O.E. | 4 | 20023 | 5 | 67 | | | B-5 gpm - 2 hrs | See Lithologic Figure 1 |
| TB 2 | | | | '75 | N.S.D.O.E. | 4 | 20027 | 5 | 71 | | | See Pump Test | " " |
| TB 3 | | | | '75 | N.S.D.O.E. | 4 | 20011 | 5 | 52 | | | B-25 gpm - 2 hrs | " " |
| TB 4 | | | | '75 | N.S.D.O.E. | 4 | 19530 | 5 | 100.3 | | | See Pump Test | " " |
| TB 5 | | | | '75 | N.S.D.O.E. | 4 | 5527 | 4 | 50 | | | See Pump Test | " " |
| TB 6 | | | | '75 | N.S.D.O.E. | 4 | 41032 | 4 | 300 | | | B-<0.5 gpm-2 hrs | " " |
| <p>Legend: N.S.D.O.E. = Nova Scotia Department of the Environment</p> <p>B = Bailed</p> | | | | | | | | | | | | | |

TABLE # 3

Time Drawdown DataThree BrooksPump Test #1

| <u>Pumping Well #4</u> | | <u>Pumping Well #4</u> | | <u>Observation Well #5</u> | |
|---|----------------------------------|---|---|--|--|
| <u>Time after</u> <u>Pumping</u> <u>Started</u> <u>(Mins.)</u> | <u>Drawdown</u> <u>(Feet)</u> | <u>Time after</u> <u>Pumping</u> <u>Stopped</u> <u>(Mins.)</u> | <u>Residual</u> <u>Drawdown</u> <u>(Feet)</u> | <u>Time after</u> <u>Pumping</u> <u>Std.</u> <u>(Mins.)</u> | <u>R = 16'</u> <u>Drawdown</u> <u>(Feet)</u> |
| 0 | 37.0 | 600 | 146.2 | 0 | 29.8 |
| 1 | 38.8 | 601 | 130.7 | 1 | 29.8 |
| 2 | 41.3 | 602 | 128.0 | 2 | 29.7 |
| 3 | 43.6 | 603 | 125.7 | 3 | 29.7 |
| 4 | 44.6 | 604 | 123.3 | 4 | 29.7 |
| 5 | 46.9 | 605 | 121.3 | 5 | 29.6 |
| 6 | 48.0 | 606 | 118.7 | 6 | 29.6 |
| 7 | 49.7 | 607 | 116.6 | 7 | 29.6 |
| 8 | 49.2 | 608 | 114.4 | 8 | 29.6 |
| 9 | 50.2 | 609 | 112.2 | 9 | 29.6 |
| 10 | 51.0 | 610 | 110.3 | 10 | 29.6 |
| 15 | 55.4 | 615 | 99.2 | 15 | 29.6 |
| 20 | 59.0 | 620 | 92.8 | 20 | 29.6 |
| 25 | 61.8 | 625 | 85.3 | 25 | 29.6 |
| 30 | 64.0 | 630 | 80.0 | 30 | 29.6 |
| 40 | 67.4 | 640 | 69.5 | 40 | 29.6 |
| 50 | 69.7 | 650 | 61.8 | 50 | 29.6 |
| 60 | 71.2 | 660 | 56.1 | 60 | 29.6 |
| 75 | 71.7 | 675 | 49.8 | 75 | 29.6 |
| 90 | 72.4 | 690 | 46.9 | 90 | 29.6 |
| 105 | 71.5 | 705 | 41.8 | 105 | 29.6 |
| 120 | 71.0 | 720 | 40.2 | 120 | 29.6 |
| 150 | 81.7 | | | 150 | 29.6 |
| 180 | 96.8 | | | 180 | 29.6 |
| 210 | 115.8 | | | 210 | 29.6 |
| 240 | 129.7 | | | 240 | 29.6 |
| 300 | 135.0 | | | 300 | 29.6 |
| 360 | 138.4 | | | 360 | 29.6 |
| 420 | 138.4 | | | 420 | 29.6 |
| 480 | 139.9 | | | 480 | 29.6 |
| 540 | 136.5 | | | 540 | 29.6 |
| 600 | 146.2 | | | 600 | 29.6 |

TABLE # 4

Time Drawdown DataThree BrooksPump Test #2

| <u>Pumping Well #5</u> | | <u>Pumping Well #5</u> | | <u>Observation Well #4</u> | |
|---|----------------------------------|---|---|--|--|
| <u>Time after</u> <u>Pumping</u> <u>Started</u> <u>(Mins.)</u> | <u>Drawdown</u> <u>(Feet)</u> | <u>Time after</u> <u>Pumping</u> <u>Stopped</u> <u>(Mins.)</u> | <u>Residual</u> <u>Drawdown</u> <u>(Feet)</u> | <u>Time after</u> <u>Pumping</u> <u>Std.</u> <u>(Mins.)</u> | <u>R = 16'</u> <u>Drawdown</u> <u>(Feet)</u> |
| 0 | 27.1 | 601 | 43.5 | 0 | 28.4 |
| 1 | 28.3 | 640 | | 1 | 28.4 |
| 2 | 28.3 | 650 | | 2 | 28.4 |
| 3 | 28.35 | 660 | 30.4 | 3 | 28.4 |
| 4 | 28.4 | 675 | 30.15 | 4 | 28.4 |
| 5 | 28.25 | 690 | 30.05 | 5 | 28.4 |
| 6 | 28.5 | 705 | 29.95 | 6 | 28.4 |
| 7 | 29.7 | 720 | 29.9 | 7 | 28.4 |
| 8 | 30.7 | 750 | 29.7 | 8 | 28.4 |
| 9 | 32.2 | | | 9 | 28.4 |
| 10 | 33.0 | | | 10 | 28.4 |
| 15 | 33.05 | | | 15 | 28.4 |
| 20 | 32.1 | | | 20 | 28.4 |
| 25 | 32.3 | | | 25 | 28.4 |
| 30 | 31.9 | | | 30 | 28.4 |
| 40 | 32.1 | | | 40 | 28.4 |
| 50 | 34.6 | | | 50 | 28.4 |
| 60 | 35.1 | | | 60 | 28.4 |
| 75 | 35.6 | | | 75 | 28.4 |
| 90 | 36.8 | | | 90 | 28.4 |
| 105 | 38.3 | | | 105 | 28.4 |
| 120 | 40.6 | | | 120 | 28.4 |
| 150 | 41.3 | | | 150 | 28.4 |
| 180 | 42.5 | | | 180 | 28.4 |
| 210 | 43.6 | | | 210 | 28.4 |
| 240 | 43.6 | | | 240 | 28.4 |
| 300 | 43.6 | | | 300 | 28.4 |
| 360 | 43.5 | | | 360 | 28.4 |
| 420 | 43.6 | | | 420 | 28.4 |
| 480 | 43.5 | | | 480 | 28.4 |
| 540 | 43.5 | | | 540 | 28.4 |
| 600 | 43.55 | | | 600 | 28.4 |

TABLE #5

Time Drawdown DataThree BrooksPump Test #3

| <u>Pumping Well #2</u> | | <u>Pumping Well #2</u> | | <u>Observation Well</u> | |
|---|------------------------|---|---------------------------------|--|------------------------|
| <u>Time After Pumping Started (Mins.)</u> | <u>Drawdown (Feet)</u> | <u>Time After Pumping Stopped (Mins.)</u> | <u>Residual Drawdown (Feet)</u> | <u>Time After Pumping Std. (Mins.)</u> | <u>Drawdown (Feet)</u> |
| 0 | 27.5 | 600 | 64.55 | Nil | |
| 1 | 28.7 | 601 | 60.00 | | |
| 2 | 30.0 | 602 | 56.3 | | |
| 3 | 30.4 | 603 | 53.5 | | |
| 4 | 30.95 | 604 | 50.4 | | |
| 5 | 31.5 | 605 | 97.7 | | |
| 6 | 32.1 | 606 | 45.55 | | |
| 7 | 32.3 | 607 | 43.9 | | |
| 8 | 32.6 | 608 | 42.0 | | |
| 9 | 32.9 | 609 | 40.5 | | |
| 10 | 33.15 | 610 | 38.9 | | |
| 15 | 34.1 | 615 | 34.8 | | |
| 20 | 34.55 | 620 | 33.3 | | |
| 25 | 34.8 | 625 | 32.7 | | |
| 30 | 35.0 | 630 | 32.8 | | |
| 40 | 35.05 | 640 | 32.4 | | |
| 50 | 35.1 | 650 | 52.0 | | |
| 60 | 35.4 | 660 | 31.7 | | |
| 75 | 35.7 | 675 | 31.75 | | |
| 90 | 36.55 | 690 | 31.15 | | |
| 105 | 36.55 | 705 | 30.8 | | |
| 120 | 42.0 | 720 | 30.65 | | |
| 150 | 44.0 | 750 | 30.30 | | |
| 180 | 44.75 | | | | |
| 210 | 45.2 | | | | |
| 240 | 45.4 | | | | |
| 300 | 52.5 | | | | |
| 360 | 52.9 | | | | |
| 420 | 62.7 | | | | |
| 480 | 63.9 | | | | |
| 540 | 64.2 | | | | |
| 600 | 64.55 | | | | |

TABLE 6

Pump Test Data

| <u>Test #</u> | <u>Well #</u> | <u>Well Depth (ft.)</u> | <u>Depth to Water (ft.)</u> | <u>Trans- missibility T(igpd/ft.)</u> | <u>Long Term Safe Pumping Rate(igpm)</u> | <u>Short Term Safe Pumping Rate(igpm)</u> |
|---------------|---------------|---------------------------------|-------------------------------------|---|--|---|
| 1 | 4 | 195 | 37.0 | 15.1 | 1.0 | 1.3 |
| 2 | 5 | 55 | 27.1 | 48 | 0.3 | 0.5 |
| 3 | 2 | 200 | 27.5 | 44.7 | 2.6 | 3.7 |

CHEMICAL ANALYSES OF GROUNDWATERS AND SURFACE WATERS IN THE THREE BROOKS AREA, NOVA SCOTIA

| Index No. | Sample No. | Grid Location | Present Owner | Depth of Sample | Depth of Well | Aquifer | Date Sampled | Analyses in mg/litre | | | | | | | |
|-----------|------------|---------------|------------------|-----------------|---------------|-----------------------|--------------|----------------------|------|------|-----|-----------------|------|------|-----|
| | | | | | | | | Ca | Mg | Na | K | SO ₄ | Cl | F | Si |
| 3 | 3 | II E10C74 | Baird | | 92 | Riversdale | Sept. 4/74 | 22.6 | 2.2 | 190 | 2.2 | 21 | 250 | 0.3 | 7.7 |
| 5 | 5 | II E10C96 | Usher | | | " | Sept. 5/74 | 39 | 5.1 | 140 | 3.6 | 48 | 215 | 0.4 | 7.1 |
| 6 | 6 | II E10C74 | Pitts, P. | | 125 | " | Sept. 5/74 | 24 | 3.4 | 250 | 3.2 | 82 | 360 | 0.9 | 7.5 |
| 7 | 7 | II E10D84 | Pitts, L. | | 125 | " | Sept. 5/74 | 31 | 4.1 | 320 | 3.9 | 82 | 475 | 0.9 | 6.9 |
| 10 | 10 | II E10C74 | Young, S. | | 98 | " | Sept. 5/74 | 7.4 | 1.0 | 140 | 1.7 | 55 | 54 | 1.6 | 6.5 |
| 2 | 2 | II E10C74 | Bennis, George | | 98 | " | Aug. 7/74 | 3.2 | 1.3 | 61 | 2.3 | 22 | 11 | 0.6 | 8.3 |
| 12 | 12 | II E10C74 | Young, A. | | 109 | " | Sept. 5/74 | 22 | 2.5 | 170 | 2.5 | 37 | 190 | 0.7 | 7.7 |
| 13 | 13 | II E10C74 | Shanty, Res. | | | " | Sept. 5/74 | 19.6 | 3 | 120 | 2.5 | 25 | 89 | 0.6 | 7.8 |
| 14 | 14 | II E10C74 | McCarthy, Laurie | | 109 | " | Sept. 5/74 | 7.4 | 0.7 | 170 | 1.7 | 38 | 117 | 1.0 | 6.7 |
| 15 | 15 | II E10C74 | Heighton | | 78 | " | Sept. 5/74 | 37 | 3.6 | 340 | 3.2 | 50 | 470 | 0.8 | 6.9 |
| 16 | 16 | II E10C74 | MacFarlane, J. | | 98 | " | Sept. 5/74 | 41 | 5.2 | 230 | 3.4 | 37 | 400 | 0.4 | 6.4 |
| 17 | 17 | II E10C96 | Landry, W. | | 99 | " | Sept. 6/74 | 30 | 4.5 | 145 | 4.4 | 65 | 136 | 0.4 | 8.3 |
| 18 | 18 | II E10C96 | Williams, N. | | 114 | " | Sept. 6/74 | 19.6 | 2.9 | 170 | 3.4 | 59 | 200 | 0.4 | 7.8 |
| 19 | 19 | II E10C74 | Hayman | | 265 | " | Sept. 6/74 | 313 | 29.5 | 1800 | 9.5 | 75 | 3600 | 1.2 | 4.3 |
| 20 | 20 | II E10C74 | Fraser, J. | | 78 | " | Sept. 6/74 | 38 | 4.7 | 300 | 3.4 | 41 | 460 | 0.6 | 7.2 |
| 21 | 21 | II E10C96 | Munro, R. | | 94 | " | Sept. 6/74 | 38 | 4.4 | 200 | 3.2 | 58 | 270 | 0.4 | 6.0 |
| 22 | 22 | II E10C74 | Lovett | | 130 | " | Sept. 6/74 | 19.4 | 2.2 | 110 | 2.2 | 81 | 65 | 0.3 | 7.9 |
| 23 | 23 | II E10C74 | Shea, F. | | | " | Sept. 6/74 | 20 | 2.2 | 170 | 2.3 | 64 | 170 | 0.8 | 7.5 |
| 24 | 24 | II E10C74 | McCarthy, Lyle | | 90 | " | Sept. 8/74 | 130 | 0.4 | 650 | 15 | 50 | 1200 | 0.6 | 6.3 |
| 26 | 26 | II E10C74 | McCarthy, T. | | 185 | " | Sept. 7/74 | 212 | 17 | 750 | 8 | 51 | 1600 | 0.4 | 5.6 |
| 29 | 29 | II E10D84 | Nichol | | 96 | " | Sept. 12/74 | 20.2 | 2.6 | 152 | 4.3 | 38 | 220 | 0.9 | 8.7 |
| 30 | 30 | II E10C75 | Matheson, H. | | 90 | " | Sept. 12/74 | 26 | 3.8 | 57 | 2.5 | 27 | 15 | 0.3 | 12 |
| 31 | 31 | II E10C75 | Matheson, R. | | 70 | " | Sept. 12/74 | 25.2 | 3.4 | 71 | 2.5 | 34 | 20 | 0.3 | 11 |
| 33 | 33 | II E10C94 | McCarthy, G. | | 85 | " | Sept. 12/74 | 18.4 | 2.0 | 27 | 2.0 | 13 | 7 | 0.3 | 11 |
| 35 | 35 | II E10C94 | Ross, Roy | | 200 | " | Sept. 12/74 | 48 | 5.2 | 15 | 3.5 | 13 | 33 | 0.1 | 13 |
| 39 | 39 | II E10C74 | MacFarlane, R. | | 107 | " | March 12/75 | 21 | 1.9 | 150 | 2.0 | 23 | 164 | 0.2 | 9 |
| 9 | 9 | II E10C96 | | | 0.5 | stream | Sept. 5/74 | 11.4 | 2.3 | 16 | 1.7 | 13 | 27 | <0.1 | 3.4 |
| 11 | 11 | II E10C74 | | | sur | spring | Aug. 7/74 | 6.7 | 2.6 | 23 | 9.2 | 13 | 45 | 0.1 | 8.5 |
| 18 | 18 | II E10C96 | | | sur | spring | Sept. 6/74 | 40 | 2.3 | 8.0 | 1.0 | 12 | 20 | <0.1 | 5.1 |
| 25 | 25 | II E10C74 | | | sur | swamp | Sept. 11/74 | 2.2 | 0.6 | 42 | 1.1 | 10 | 49 | <0.1 | 1.6 |
| 31 | 31 | II E10C75 | | | sur | spring | Sept. 12/74 | 18.1 | 2.3 | 73 | 2.4 | 38 | 28 | 0.3 | 12 |
| 32 | 32 | II E10C94 | | | 0.5 | stream | Sept. 12/74 | 12.0 | 1.8 | 12 | 1.6 | 14 | 18 | <0.1 | 4.8 |
| 37 | 37 | II E10C74 | | | sur | swamp | Sept. 12/74 | 15.9 | 4.5 | 60 | 1.3 | 34 | 145 | <0.1 | 3.8 |
| 36 | 36 | II E10C74 | | | sur | spring | Sept. 12/74 | 9.6 | 2.4 | 7.0 | 4.2 | 7 | 13 | <0.1 | 9.2 |
| 1 | 1 | II E10C74 | McCarthy T. | | 28 | clay till | Sept. 4/74 | 46 | 6.6 | 120 | 3.0 | 34 | 200 | 0.2 | 6.2 |
| 4 | 4 | II E10C96 | Hartling L. | | 18 | clay till | Sept. 4/74 | 23 | 7.1 | 100 | 9.6 | 37 | 83 | <0.1 | 4.7 |
| 8 | 8 | II E10C96 | MacKenzie | | 24 | sandy till | Sept. 5/74 | 36 | 5.4 | 70 | 3.0 | 18 | 140 | <0.1 | 3.5 |
| 21 | 21 | II E10C96 | Munro R. | | 21 | sandy till | Sept. 6/74 | 34 | 6.1 | 17 | 2.5 | 14 | 30 | 0.1 | 4.7 |
| 28 | 28 | II E10D84 | MacFarlane R. | | 24 | sandy till | Sept. 12/74 | 16.5 | 4.4 | 49 | 9.0 | 28 | 72 | <0.1 | 6.9 |
| 34 | 34 | II E10C94 | Faulkner | | 24 | sandy till | Sept. 12/74 | 41.2 | 7.6 | 42 | 13 | 29 | 130 | 0.1 | 11 |
| 38 | 38 | II E10C74 | McCarthy | | 6 | sandy till excavation | Oct. 24/74 | 22.5 | 1.5 | 27 | 11 | 7.5 | 41 | 0.2 | 9.8 |

| Analyses in mg/litre | | | | | | | | | | | | | Ions in meq/litre | | | | | | | | | | |
|---|-------------------------|--------------------------|-------|-------|--------|--------|--------|---------------------------------------|-------------------------------------|-----------------|-----------------------------------|-----------------|---------------------|-----------------------------------|-----|-------|---------|-------|------|------|-----------------|-------|-------------------------------------|
| NO ₃ + NO ₂ as N | NH ₃ as N | PO ₄ ortho | Fe | Mn | Pb | Cu | Zn | Alkalinity as CaCO ₃ | Hardness as CaCO ₃ | Total Solids | Total Dis- solved Solids | Color T.C.U. | Turbidity J.T.U. | Conduc- tivity µmhos/ cm | pH | | Cations | | | | Anions | | |
| | | | | | | | | | | | | | | | Lab | Field | Ca | Mg | Na | K | SO ₄ | Cl | CO ₃ HCO ₃ |
| <0.1 | <0.1 | <0.1 | 0.2 | 0.07 | <0.005 | 0.01 | 0.06 | 126 | 66 | 592 | 592 | 20 | 1.8 | 1220 | 8.2 | | 1.1 | 0.2 | 8.3 | .06 | 0.4 | 7.1 | 2.52 |
| <0.1 | <0.1 | <0.1 | <0.1 | 0.3 | <0.005 | 0.03 | 0.02 | 114 | 119 | 566 | 562 | 5 | 0.23 | 1115 | 8.1 | | 1.9 | 0.42 | 6.1 | 0.04 | 1 | 6.1 | 2.28 |
| <0.1 | <0.1 | 0.1 | 0.2 | 0.06 | <0.005 | 0.06 | 0.06 | 104 | 75 | 832 | 829 | 15 | 1.1 | 1690 | 8.1 | | 1.2 | 0.3 | 10.9 | 0.08 | 1.7 | 10.2 | 2.09 |
| <0.1 | <0.1 | <0.1 | 0.1 | 0.2 | <0.005 | 0.04 | 0.02 | 100 | 94 | 1056 | 1052 | 10 | 0.82 | 2040 | 8.1 | | 1.5 | 0.3 | 13.9 | 0.1 | 1.7 | 13.4 | 2.0 |
| <0.1 | <0.1 | <0.1 | <0.1 | <0.05 | <0.005 | 0.007 | 0.03 | 189 | 23 | 403 | 400 | 5 | 0.6 | 716 | 8.6 | | 0.4 | 0.08 | 6.1 | 0.04 | 1.1 | 1.5 | 3.78 |
| <0.1 | <0.1 | <0.1 | 0.2 | 0.2 | <0.005 | <0.005 | <0.005 | 121 | 13 | 193 | 189 | 20 | 32 | 295 | 8.6 | | 0.2 | 0.1 | 2.7 | 0.06 | 0.4 | 0.3 | 2.42 |
| 0.4 | <0.1 | <0.1 | <0.1 | 0.03 | <0.005 | 0.006 | 0.07 | 146 | 65 | 810 | 809 | 10 | 0.74 | 1060 | 8.2 | | 1.1 | 0.2 | 7.4 | 0.06 | 0.8 | 5.4 | 2.52 |
| <0.1 | <0.1 | <0.1 | <0.1 | 0.07 | <0.005 | 0.03 | 0.01 | 164 | 62 | 386 | 384 | 10 | 0.5 | 716 | 8.2 | | 1.0 | 0.2 | 5.2 | 0.06 | 0.5 | 2.5 | 3.28 |
| <0.1 | <0.1 | <0.1 | <0.1 | 0.03 | 0.005 | 0.006 | 0.02 | 179 | 22 | 456 | 453 | 10 | 3.3 | 875 | 8.5 | | 0.4 | 0.06 | 7.4 | 0.04 | 0.8 | 3.3 | 3.58 |
| <0.1 | <0.1 | <0.1 | <0.1 | 0.07 | <0.005 | 0.02 | 0.04 | 250 | 107 | 1042 | 1040 | 5 | 0.84 | 2000 | 8.0 | | 1.8 | 0.2 | 14.8 | .08 | 1 | 13.3 | 5.0 |
| <0.1 | <0.1 | <0.1 | 0.3 | 0.3 | <0.005 | 0.02 | 0.07 | 110 | 124 | 836 | 832 | 10 | 2.6 | 1645 | 8.0 | | 2 | 0.4 | 10 | 0.09 | 0.8 | 11.3 | 2.2 |
| <0.1 | <0.1 | <0.1 | <0.1 | 0.09 | <0.005 | 0.02 | 0.02 | 78 | 93 | 519 | 517 | 5 | 0.46 | 1010 | 8.2 | | 1.5 | 0.4 | 6.3 | 0.1 | 1.4 | 3.8 | 1.56 |
| <0.1 | <0.1 | 0.1 | <0.1 | 0.05 | <0.005 | 0.01 | 0.02 | 100 | 61 | 8.1 | 540 | 10 | 0.55 | 1160 | 8.1 | | 1 | 0.2 | 7.4 | 0.09 | 1.2 | 5.6 | 2.0 |
| 0.3 | 0.2 | <0.1 | 0.7 | 2.7 | 0.14 | 0.22 | 6.05 | 76 | 906 | 6680 | 6620 | 5 | 44 | 15000 | 7.0 | | 15.6 | 2.4 | 78 | 0.2 | 1.6 | 101.5 | 1.52 |
| <0.1 | <0.1 | <0.1 | 2.2 | 0.3 | <0.005 | 0.006 | 0.06 | 145 | 116 | 950 | 940 | 30 | 16 | 1965 | 7.5 | | 1.9 | 0.4 | 13 | 0.09 | 0.9 | 13 | 2.9 |
| <0.1 | <0.1 | <0.1 | 0.3 | 0.3 | <0.005 | 0.01 | 0.04 | 110 | 114 | 649 | 646 | 5 | 2.0 | 1350 | 8.1 | | 1.9 | 0.4 | 8.7 | 0.08 | 1.2 | 7.6 | 2.2 |
| <0.1 | <0.1 | <0.1 | 0.1 | 0.09 | <0.005 | 0.02 | 0.06 | 107 | 58 | 365 | 362 | 0 | 1.4 | 664 | 8.1 | | 1.0 | 0.2 | 4.8 | 0.06 | 1.7 | 1.8 | 2.14 |
| <0.1 | <0.1 | <0.1 | <0.1 | 0.13 | <0.005 | 0.02 | 0.02 | 126 | 59 | 516 | 513 | 5 | 0.42 | 1035 | 7.4 | | 1.0 | 0.2 | 7.4 | 0.06 | 1.4 | 4.8 | 2.52 |
| 0.8 | | 0.1 | 0.2 | 0.02 | <0.005 | 0.01 | 0.08 | 140 | 326 | 2530 | 2505 | 35 | 20 | 4600 | 8.8 | | 6.5 | 0.3 | 28.3 | 0.36 | 1.0 | 33.8 | 2.8 |
| <0.1 | 0.2 | 0.1 | 2.2 | 0.8 | <0.005 | 0.01 | 0.08 | 57 | 600 | 2917 | 2896 | 40 | 30 | 5030 | 7.7 | | 10.6 | 1.4 | 32.6 | 0.2 | 1.0 | 45.1 | 1.14 |
| <0.1 | <0.1 | <0.1 | <0.1 | 0.02 | <0.001 | 0.01 | 0.02 | 90 | 61 | 498 | 496 | 35 | 0.88 | 582 | 8.0 | | 1.0 | 0.2 | 6.6 | 0.1 | 0.8 | 6.2 | 1.8 |
| <0.1 | <0.1 | <0.1 | 0.2 | 0.09 | 0.006 | 0.02 | 0.11 | 170 | 80 | 269 | 254 | 10 | 1.03 | 524 | 7.7 | | 1.3 | 0.3 | 2.5 | 0.06 | 0.6 | 0.4 | 3.4 |
| <0.1 | <0.1 | <0.1 | 0.1 | 0.4 | 0.008 | 0.02 | 0.05 | 170 | 77 | 280 | 270 | 5 | 0.26 | 428 | 7.9 | | 3.1 | 0.06 | 1.3 | 0.3 | 0.7 | 0.6 | 3.4 |
| <0.1 | <0.1 | <0.1 | <0.1 | 0.01 | 0.006 | 0.02 | 0.03 | 100 | 54 | 150 | 146 | 5 | 0.27 | 233 | 7.7 | | 0.9 | 0.2 | 1.2 | 0.05 | 0.3 | 0.2 | 2.0 |
| 0.5 | <0.1 | <0.1 | <0.1 | 0.1 | <0.005 | <0.005 | 0.50 | 145 | 141 | 237 | 237 | 15 | 0.42 | 257 | 7.5 | | 2.4 | 0.4 | 2.2 | 0.9 | 0.3 | 0.9 | 2.9 |
| <0.1 | <0.1 | 0.02 | 0.2 | 0.05 | 0.006 | <0.005 | 0.06 | 143 | 60 | | 470 | | | 788 | 7.9 | | 1.04 | 0.166 | 6.52 | 0.05 | 0.48 | 4.63 | 2.84 |
| <0.1 | | <0.1 | 0.1 | 0.1 | <0.005 | 0.05 | 0.02 | 24 | 38 | 130 | 125 | 60 | 1.3 | 173 | 7.3 | | 0.56 | 0.19 | 0.70 | 0.43 | 0.27 | 0.76 | 0.48 |
| 2.4 | | <0.1 | <0.1 | 0.03 | <0.005 | 0.01 | 0.05 | 13 | 28 | 139 | 138 | 5 | 0.3 | 220 | 6.2 | | 0.33 | 0.21 | 1.00 | 0.24 | 0.27 | 1.30 | 0.24 |
| <0.1 | | 1.0 | <0.1 | 0.03 | <0.005 | 0.01 | 0.02 | 92 | 110 | 160 | 154 | 10 | 0.43 | 300 | 7.8 | | 1.99 | 0.21 | 0.35 | 0.02 | 0.25 | 0.56 | 1.84 |
| <0.1 | | 0.1 | 1.1 | 0.3 | 0.01 | 0.11 | 0.03 | 27 | 8 | 188 | 184 | 240 | 2.0 | 255 | 6.7 | | 0.11 | 0.05 | 1.83 | 0.03 | 0.21 | 1.38 | 0.54 |
| <0.1 | | <0.1 | <0.1 | 2.3 | <0.005 | 0.007 | 0.01 | 190 | 55 | 290 | 290 | 5 | 3.2 | 400 | 7.9 | | 0.90 | 0.21 | 3.18 | 0.06 | 0.75 | 0.79 | 3.8 |
| <0.1 | | <0.1 | 0.2 | 0.1 | <0.005 | 0.01 | 0.03 | 25 | 38 | 118 | 118 | 55 | 3.0 | 144 | 7.1 | | 0.60 | 0.15 | 0.52 | 0.04 | 0.29 | 0.51 | 0.50 |
| <0.1 | | <0.1 | 4.6 | 5.5 | 0.06 | 0.02 | 0.06 | 13 | 58 | 369 | 233 | 120 | 1.0 | 246 | 5.5 | | 0.79 | 0.37 | 2.61 | 0.03 | 0.71 | 4.09 | 0.26 |
| <0.1 | | <0.1 | 3.6 | 0.5 | <0.005 | 0.03 | 0.01 | 36 | 34 | 141 | 120 | 1.0 | 8 | 158 | 6.8 | | 0.48 | 0.20 | .30 | 0.11 | 0.15 | 0.37 | 0.72 |
| 0.4 | | <0.1 | 0.7 | 0.06 | 0.006 | 0.13 | 0.23 | 97 | 142 | 638 | 629 | 30 | 4.1 | 1060 | 7.5 | | 2.30 | 0.55 | 5.22 | 0.08 | 0.71 | 5.64 | 1.94 |
| 1.6 | | <0.1 | 0.4 | 0.09 | <0.005 | 0.03 | 1.89 | 33 | 87 | 493 | 488 | 20 | 2.6 | 796 | 6.5 | | 1.15 | 0.58 | 4.53 | 0.25 | 0.77 | 2.34 | 0.66 |
| 6.4 | | <0.1 | 0.2 | <0.01 | 0.005 | 0.08 | 0.90 | 54 | 114 | 484 | 479 | 0 | 0.76 | 838 | 7.3 | | 1.80 | 0.44 | 3.01 | 0.08 | 0.37 | 3.95 | 1.08 |
| 2.8 | | <0.1 | 0.1 | <0.01 | <0.005 | 0.01 | 0.03 | 92 | 109 | 359 | 199 | 15 | 0.37 | 200 | 7.6 | | 1.70 | 0.50 | 0.74 | 0.06 | 0.29 | 0.84 | 1.84 |
| 9.6 | | <0.1 | <0.1 | 0.05 | <0.005 | 0.02 | 0.34 | 19 | 59 | 274 | 272 | 20 | 4.0 | 423 | 6.5 | | 0.82 | 0.36 | 2.13 | 0.23 | 0.58 | 2.03 | 0.38 |
| 7.8 | | <0.1 | 0.2 | 0.3 | 0.01 | 0.01 | 0.06 | 29 | 134 | 374 | 325 | 5 | 0.16 | 510 | 6.1 | | 2.05 | 0.62 | 1.83 | 0.33 | 0.60 | 3.66 | 0.58 |
| 2.2 | | <0.1 | <0.05 | 0.02 | <0.005 | 0.002 | <0.005 | 56 | 62 | 195 | 182 | 90 | 61 | 297 | 8.5 | | 1.12 | 0.12 | 1.22 | 0.28 | 0.156 | 1.15 | 1.12 |

CHEMICAL ANALYSES OF GROUNDWATERS FROM TEST WELLS IN THE THREE BROOKS AREA, NOVA SCOTIA

| Index No. | Sample No. | Grid Location | Present Owner | Depth of Sample | Depth of Well | Aquifer | Date Sampled | Analyses in mg/litre | | | | | | | |
|-----------|------------|---------------|---------------------------------------|-----------------|---------------|------------|--------------|----------------------|-----|------|------|-----------------|--------|------|----|
| | | | | | | | | Co | Mg | Na | K | SO ₄ | Cl | F | Si |
| TB-1-75 | 1 | 11E10C74 | Nova Scotia Department of Environment | 13 | 200 | Riversdale | 6/3/75 | 15 | 2.8 | 10.5 | 2.5 | 11 | 36 | <0.1 | 5 |
| | 2 | | " | 55 | " | " | 6/3/75 | | | 84 | | | 110 | | |
| | 3 | | " | 77 | " | " | 6/3/75 | 52 | 7.3 | 76 | 7.0 | 23 | 110 | 0.1 | 6 |
| | 4 | | " | 122 | " | " | 6/3/75 | 14 | 1.8 | 125 | 11.0 | 25 | 123 | 0.5 | 5 |
| | 5 | | " | 145 | " | " | 7/3/75 | | | | | | 240 | | |
| | 6 | | " | 200 | " | " | 7/3/75 | 260 | 24 | 1000 | 10.0 | 4.5 | 2120 | 0.4 | 5 |
| TB-2-75 | 1 | 11E10C74 | Nova Scotia Department of Environment | 87 | 200 | Riversdale | 12/3/75 | 20 | 2.5 | 51 | 3.5 | 12 | 22 | 0.2 | 1 |
| | 2 | | " | 120 | " | " | 12/3/75 | | | 78 | | | 46 | | |
| | 3 | | " | 200 | " | " | 12/3/75 | | | 150 | | | 172 | | |
| | 4 | | " | 200 | " | " | 12/3/75 | 40 | 41 | 190 | 9.0 | 9.5 | 285 | 0.3 | 7 |
| TB-3-75 | 1 | 11E10C74 | Nova Scotia Department of Environment | 69 | 200 | Riversdale | 18/3/75 | 125 | 11 | 750 | 9.6 | 3.5 | 1520 | | |
| | 2 | | " | 200 | " | " | 18/3/75 | 137 | 12 | 1000 | 17 | 4.5 | 1840 | 0.7 | 4 |
| | 3 | | " | 200 | " | " | 18/3/75 | 182 | 16 | 1210 | 12 | 6.0 | 2520 | 0.8 | 3 |
| TB-4-75 | 1 | 11E10C74 | Nova Scotia Department of Environment | 80 | 195 | Riversdale | 25/3/75 | 34 | 4.8 | 108 | 6.5 | 32 | 99 | 0.3 | 8 |
| | 2 | | " | 98 | " | " | 31/3/75 | 32 | 4.6 | 98 | 6.5 | 34 | 103 | 0.3 | 5 |
| | 3 | | " | 165 | " | " | 31/3/75 | 82 | 8.4 | 560 | | | 1180 | | |
| | 4 | | " | 195 | " | " | 31/3/75 | 398 | 36 | 1650 | | 5 | 3380 | | |
| | 5 | | " | 195 | " | " | 31/3/75 | 462 | 41 | 1920 | 15.0 | 8 | 4000 | 0.8 | 1 |
| TB-5-75 | 1 | 11E10C74 | Nova Scotia Department of Environment | 48 | 55 | Riversdale | 3/4/75 | 56 | 7.2 | 110 | 9 | 16 | 126 | 0.3 | 8 |
| | 2 | | " | 55 | " | " | 3/4/75 | 39 | 5.5 | 92 | 5.5 | 29 | 100 | 0.3 | 7 |
| TB-6-75 | 1 | 11E10C74 | Nova Scotia Department of Environment | 173 | 410 | Riversdale | 15/4/75 | 23 | 2.4 | 313 | 15 | 19 | 500 | 1.1 | 6 |
| | 2 | | " | 199 | " | " | 15/4/75 | 224 | 22 | 1200 | 28 | 10 | 2380 | 0.8 | 3 |
| | 3 | | " | 247 | " | " | 15/4/75 | 585 | 54 | 2480 | 43 | 14 | 5100 | 1.0 | 3 |
| | 4 | | " | 290 | " | " | 15/4/75 | 550 | 50 | 2140 | 33 | 8 | 4580 | 0.9 | 4 |
| | 5 | | " | 327 | " | " | 21/4/75 | 3520 | 315 | 5500 | 60 | <10 | 16,600 | 1.4 | 3 |
| | 6 | | " | 340 | " | " | 21/4/75 | 5130 | 440 | 8200 | 56 | <10 | 23,700 | 1.8 | 5 |
| | 7 | | " | 370 | " | " | 21/4/75 | 4210 | 390 | 7500 | 59 | <10 | 21,400 | 1.7 | 4 |
| | 8 | | " | 400 | " | " | 24/4/75 | 4050 | 360 | 7000 | 70 | <10 | 21,200 | 1.8 | 3 |
| | 9 | | " | 410 | " | " | 18/7/75 | 6800 | 420 | 8630 | 30 | <10 | 25,500 | 1.9 | 3 |

| Analyses in mg/litre | | | | | | | | | | | | | Ions in meq/litre | | | | | | | | | | | |
|--|----------------------------|--------------------------|------|------|--------|--------|--------|---------------------------------------|-------------------------------------|-----------------|--------------------------------|-----------------|---------------------|-----------------------------------|-----|-------|---------|-------|--------|-------|-----------------|--------|--|------|
| NO ₃ + NO ₂ as N | NH ₃ as N | PO ₄ ortho | Fe | Mn | Pb | Cu | Zn | Alkalinity as CaCO ₃ | Hardness as CaCO ₃ | Total Solids | Total Dis- solved Solids | Color T.C.U. | Turbidity J.T.U. | Conduc- tivity µmhos/ cm | pH | | Cations | | | | Anions | | | |
| | | | | | | | | | | | | | | | Lab | Field | Ca | Mg | Na | K | SO ₄ | Cl | CO ₃ + HCO ₃ | |
| 0.3 | 0.2 | 0.02 | 0.3 | 0.6 | 0.006 | 0.03 | <0.05 | 14 | 50 | | 116 | 20 | | | 6.8 | | 0.748 | 0.23 | 0.46 | 0.64 | 0.23 | 1.02 | 0.28 | |
| <0.1 | | | | | | | | 152 | | | | | | | | | | | 3.65 | | | | 3.10 | 3.04 |
| 0.1 | <0.1 | <0.02 | 0.2 | 0.9 | 0.006 | 0.02 | <0.005 | 159 | 160 | | 391 | 20 | | | 7.3 | | 2.59 | 0.6 | 3.31 | 0.178 | 0.48 | 3.10 | 3.18 | |
| | 0.2 | <0.04 | <0.1 | 0.1 | <0.005 | 0.02 | 0.01 | 145 | 42 | | 439 | | | | 8.4 | | 0.7 | 0.15 | 5.43 | 0.28 | 0.52 | 3.46 | 2.9 | |
| <0.1 | 0.4 | 0.02 | 0.6 | 1.4 | <0.006 | 0.03 | 0.009 | 73 | 750 | | 3842 | 20 | | | 7.3 | | 12.97 | 1.97 | 43.5 | 0.26 | 0.09 | 59.81 | 1.46 | |
| 0.1 | <0.1 | 0.02 | 0.4 | 0.7 | <0.005 | 0.006 | 0.02 | 144 | 59 | | 209 | | | 355 | 7.5 | | 1.0 | 0.21 | 2.22 | 0.09 | 0.25 | 0.62 | 2.88 | |
| | | | | | | | | | | | | | | | | | | | 3.39 | | | 1.29 | | |
| | | | | | | | | | | | | | | | | | | | 6.53 | | | 4.85 | | |
| 0.03 | 0.1 | 7 | 0.3 | 0.2 | <0.005 | <0.006 | 0.06 | 130 | 116 | | 630 | | | 1880 | 8.1 | | 2.0 | 0.34 | 8.27 | 0.23 | 0.2 | 8.04 | 2.6 | |
| <0.1 | | | | | | | | 58 | 354 | | | | | 4520 | 7.8 | | 6.24 | 0.90 | 32.62 | 0.25 | 0.07 | 42.87 | 1.16 | |
| <0.1 | 0.4 | 0.02 | 1.8 | 2.0 | 0.009 | <0.005 | | 62 | 393 | | 3470 | 60 | | 5400 | 7.7 | | 6.84 | 0.99 | 43.5 | 0.43 | 0.94 | 51.9 | 1.24 | |
| | 0.4 | 0.02 | 0.5 | 0.8 | 0.007 | 0.04 | | 53 | 510 | | 4480 | 70 | | 7020 | 7.6 | | 9.08 | 1.32 | 52.64 | 0.31 | 0.12 | 71.09 | 1.06 | |
| <0.1 | 0.1 | 0.05 | 0.1 | 0.4 | 0.005 | 0.005 | <0.005 | 155 | 105 | | 187 | 15 | | 626 | 7.8 | | 1.69 | 0.39 | 4.7 | 0.17 | 0.67 | 2.79 | 3.1 | |
| 0.1 | 0.4 | <0.02 | 0.1 | 0.7 | 0.01 | 0.02 | 0.01 | 143 | 99 | | 398 | | | 684 | 7.8 | | 1.59 | 0.38 | 4.26 | 0.17 | 0.71 | 2.91 | 2.86 | |
| | | | | | | | | | | | | | | | 7.6 | | 4.09 | 0.69 | 24.36 | | | 31.25 | | |
| 0.1 | 0.6 | 0.02 | 0.3 | 1.9 | 0.01 | 0.008 | 0.005 | 38 | 1325 | | 7442 | 35 | | 11880 | 6.9 | | 19.86 | 2.96 | 71.77 | | 0.10 | 95.34 | | |
| | | | | | | | | | | | | | | | | | 23.05 | 3.37 | 83.52 | 0.38 | 0.17 | 112.84 | 0.76 | |
| 0.1 | <0.1 | 0.08 | | | | | | 178 | 170 | | 424 | | | 972 | 8.1 | | 2.79 | 0.59 | 4.78 | 0.23 | 0.33 | 3.55 | 3.56 | |
| <0.1 | <0.1 | 0.06 | 0.4 | 0.9 | <0.005 | <0.005 | <0.008 | 184 | 121 | | 382 | 15 | | 648 | 8.2 | | 1.95 | 0.45 | 4.0 | 0.14 | 0.60 | 2.82 | 3.68 | |
| 0.1 | 0.3 | <0.02 | 0.9 | 0.9 | <0.005 | 0.008 | 0.005 | 90 | 67 | | 962 | | | 1890 | 8.5 | | 1.15 | 0.2 | 13.62 | 0.38 | 0.4 | 14.11 | 1.8 | |
| <0.1 | 0.6 | <0.02 | 0.1 | 0.5 | <0.005 | 0.008 | <0.005 | 49 | 653 | | 4248 | | | 6480 | 7.7 | | 11.18 | 1.81 | 52.9 | 0.72 | 0.21 | 67.14 | 0.98 | |
| 0.1 | 0.9 | 0.02 | <0.1 | 1.2 | <0.005 | 0.01 | <0.005 | 39 | 1687 | | 9016 | | | 12420 | 7.8 | | 29.19 | 4.44 | 107.88 | 1.1 | 0.29 | 143.87 | 0.78 | |
| <0.1 | 0.8 | 0.03 | <0.1 | 1.4 | <0.005 | 0.005 | 0.009 | 44 | 1585 | | 8038 | | | 11990 | 7.6 | | 27.44 | 4.11 | 93.09 | 0.84 | 0.17 | 129.20 | 0.88 | |
| 0.1 | 1.5 | 0.4 | 2.9 | 11.0 | <0.005 | 0.02 | 0.02 | 12 | 10,100 | | 24,380 | | | 39360 | 7.3 | | 175.64 | 25.91 | 239.25 | 1.53 | | 468.29 | 0.24 | |
| <0.1 | 2.0 | 0.04 | 0.6 | 18.4 | <0.005 | 0.03 | 0.03 | 9 | 14,600 | | 41,940 | | | 54000 | 6.9 | | 255.99 | 36.19 | 356.7 | 1.43 | | 667.6 | 0.18 | |
| 0.1 | 1.8 | 0.04 | 1.8 | 10.0 | <0.005 | 0.04 | 0.01 | 7 | 12,120 | | 37,780 | 10 | | 51840 | 7.2 | | 210.08 | 32.06 | 326.25 | 1.51 | | 603.69 | 0.14 | |
| 0.1 | 1.8 | 0.04 | 1.1 | 10.7 | 0.005 | 0.03 | 0.02 | 12 | 1280 | | 40,670 | | | 50760 | 6.9 | | 202 | 29.6 | 304.5 | 1.79 | | 598.05 | 0.24 | |
| <0.1 | 2.5 | 0.05 | 12 | 26.8 | 0.02 | 0.54 | 0.15 | 30 | 18,750 | | 43,380 | | | 56000 | 6.6 | | 339.32 | 34.55 | 375.4 | 0.77 | | 719.0 | 0.6 | |

CHEMICAL ANALYSES OF GROUNDWATERS PUMP TEST RESULTS IN THE THREE BROOKS AREA, NOVA SCOTIA

TABLE 7

| Index No. | Sample No. | Grid Location | Present Owner | Depth of Sample | Depth of Well | Aquifer | Date Sampled | Analyses in mg/litre | | | | | | | |
|-----------|------------|---------------|---------------------------------------|-----------------|---------------|------------|--------------|----------------------|-----|------|-----|-----------------|------|-----|----|
| | | | | | | | | Ca | Mg | Na | K | SO ₄ | Cl | F | Si |
| TB-2-75 | 0 | IIEIOC74 | Nova Scotia Department of Environment | | 200 | Riversdale | 1/5/75 | 160 | 16 | 590 | 6.8 | 9.0 | 1250 | 0.3 | 6 |
| | 5 | " | " | | " | " | " | 102 | 10 | 405 | 5.5 | 9.0 | 835 | 0.3 | 6 |
| | 20 | " | " | | " | " | " | 76 | 8.4 | 302 | 4.8 | 10 | 602 | 0.3 | 6 |
| | 60 | " | " | | " | " | " | 73 | 8.2 | 242 | 4.6 | 9.5 | 542 | 0.3 | 7 |
| | 200 | " | " | | " | " | " | 45 | 5.5 | 160 | 3.8 | 13 | 272 | 0.2 | 9 |
| | 600 | " | " | | " | " | " | 38 | 4.4 | 125 | 3.0 | 19 | 186 | 0.3 | 9 |
| TB-4-75 | J | IIEIOC74 | Nova Scotia Department of Environment | | 200 | Riversdale | 23/4/75 | 460 | 39 | 1950 | 12 | <10 | 4130 | 0.8 | 5 |
| | 5 | " | " | | " | " | " | 370 | 98 | 2150 | 12 | <10 | 4360 | | |
| | 20 | " | " | | " | " | " | 509 | 43 | 1850 | 11 | <10 | 3760 | | |
| | 60 | " | " | | " | " | " | 480 | 43 | 1950 | 12 | <10 | 4180 | 0.8 | 4 |
| | 200 | " | " | | " | " | " | 451 | 39 | 1900 | 11 | <10 | 3930 | | |
| | 600 | " | " | | " | " | " | 452 | 36 | 1900 | 11 | <10 | 3880 | 0.8 | 4 |
| TB-5-75 | 0 | IIEIOC74 | Nova Scotia Department of Environment | | 55 | Riversdale | 30/4/75 | 42 | 5.6 | 115 | 4.4 | 27 | 163 | 0.2 | 7 |
| | 20 | " | " | | " | " | " | 40 | 5.4 | 97 | 5.3 | 27 | 121 | 0.3 | 7 |
| | 60 | " | " | | " | " | " | 39 | 5.2 | 98 | 4.6 | 26 | 106 | 0.2 | 8 |
| | 600 | " | " | | " | " | " | 39 | 5.1 | 96 | 3.8 | 28 | 89 | 0.2 | 8 |

TABLE # 10

Total Salinity and Ratio of
Chloride/Carbonate + Bicarbonate from
Selected Well Water Supplies

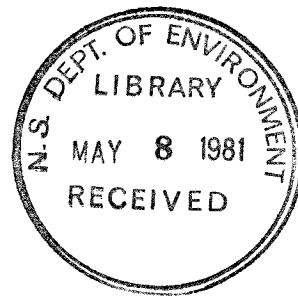
| Well Number | Sample Number | Distance from Coast (in feet) | Cl/CO ₃ +HCO ₃ (ppm) | Total Salinity as NaCl |
|-------------|---------------|-------------------------------|--|------------------------|
| 30 | 30 | 10,000 | 0.12 | 23.4 |
| 10 | 10 | 6,000 | 0.396 | 87.8 |
| 16 | 16 | 3,000 | 5.14 | 596.7 |
| 7 | 7 | 1,500 | 6.7 | 783.9 |

TABLE # 11

Total Salinity and Ratio of
Chloride/Carbonate + Bicarbonate of Test Well #6

| Test Well #6 | Sample Number | Sample Depth | Cl/CO ₃ +HCO ₃ | Total Salinity as NaCl |
|--------------|---------------|--------------|--------------------------------------|------------------------|
| #6 | 1 | 173 | 7.8 | 823 |
| | 2 | 199 | 68.5 | 3921 |
| | 3 | 247 | 184.4 | 8404 |
| | 4 | 290 | 146.81 | 7547 |
| | 5 | 327 | 1951.2 | 27354 |
| | 6 | 340 | 3788 | 39054 |
| | 7 | 370 | 4312 | 35264 |
| | 8 | 400 | 2491 | 34935 |

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