HYDROLOGIC BUDGET ANALYSIS

WHITES POINT QUARRY LITTLE RIVER, DIGBY COUNTY, NOVA SCOTIA

Prepared For:

Bilcon of Nova Scotia

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TABLE OF CONTENTS

<u>Page</u>

1.0	INTR	ODUCTION	1
	1.1	BACKGROUND	1
	1.2	STUDY OBJECTIVES	1
2.0	METH	HODOLOGY	2
	2.1	MODEL DESCRIPTION	2
	2.2	HYDROLOGY	2
	2.3	SOILS/COVER INFORMATION	3
	2.4	LAND USE	3
	2.5	MODELING AND ANALYSIS	4
	2.5.1	RUNOFF	4
	2.5.2	POND AREAS	4
	2.5.3	WATER DEMAND	4
3.0	RESU	LTS	5
4.0	CON	CLUSIONS	5
5.0	REFE	RENCES	6

LIST OF FIGURES (Following Text)

FIGURE 1	SITE LOCATION MAP
FIGURE 2	MEAN MONTHLY PRECIPITATION AND TEMPERATURE DATA
FIGURE 3	CONTRIBUTING DRAINAGE AREA
FIGURE 4	AVERAGE WATER SUPPLY AND DEMAND - YEAR 0 (EXISTING)
FIGURE 5	AVERAGE WATER SUPPLY AND DEMAND – YEAR 5
FIGURE 6	AVERAGE WATER SUPPLY AND DEMAND - YEAR 10
FIGURE 7	AVERAGE WATER SUPPLY AND DEMAND - YEAR 15
FIGURE 8	AVERAGE WATER SUPPLY AND DEMAND - YEAR 20
FIGURE 9	AVERAGE WATER SUPPLY AND DEMAND - YEAR 30
FIGURE 10	AVERAGE WATER SUPPLY AND DEMAND - YEAR 40
FIGURE 11	AVERAGE WATER SUPPLY AND DEMAND – YEAR 50 (RECLAIMED)

LIST OF TABLES (Following Text)

TABLE 1	LAND USE SUMMARY
TABLE 2	SUMMARY RESULTS
TABLE 3	DETAILED SUMMARY TABLE - YEAR 0 (EXISTING)
TABLE 4	DETAILED SUMMARY TABLE – YEAR 5
TABLE 5	DETAILED SUMMARY TABLE - YEAR 10
TABLE 6	DETAILED SUMMARY TABLE – YEAR 15
TABLE 7	DETAILED SUMMARY TABLE – YEAR 20
TABLE 8	DETAILED SUMMARY TABLE - YEAR 30
TABLE 9	DETAILED SUMMARY TABLE – YEAR 40
TABLE 10	DETAILED SUMMARY TABLE - YEAR 50 (RECLAIMED)

LIST OF APPENDICES

APPENDIX A	SUMMARY MODEL OUTPUT DATA
APPENDIX B	QUARRY CONCEPT PLANS

1.0 INTRODUCTION

Conestoga-Rovers and Associates (CRA) (formerly MGI Limited) was requested to carry out a hydrologic budget analysis on behalf of Bilcon of Nova Scotia (Bilcon), for the proposed Whites Point Quarry Project. This report summarizes the methodology used and presents the results of the analysis.

Please note that the initial analysis and Preliminary Results were submitted by MGI Limited while MGI was still 50% owned by CRA. As of October 1, 2005, MGI is 100% owned by CRA and therefore this report is presented to your office as a CRA document.

1.1 <u>BACKGROUND</u>

The proposed Whites Point Quarry site is located along the Digby Neck at Whites Point, near the community of Little River, Digby County, Nova Scotia. A location map is provided as Figure 1.

The project involves the construction and operation of a basalt quarry, processing facility and marine terminal. Year-round extraction and processing activities are expected to take place on 300 acres of land, with approximately 40,000 tonnes of aggregate produced for ship loading each week, totaling two million tonnes per year.

The intent is to ship washed aggregate from the site, utilizing only surface water runoff collected on site to make-up for losses in the washing process. The runoff would be collected in a series of sedimentation ponds.

1.2 <u>STUDY OBJECTIVES</u>

The purpose of this study was to carry out a hydrologic budget analysis of the proposed quarry site and contributing drainage basin. Study objectives were as follows:

- Assess surface water hydrology for the site, based on average historic climate records for the area;
- Estimate losses in the hydrologic budget such as evapotranspiration, and storage pond evaporation and seepage losses;
- Determine average expected moisture surplus available at the site (i.e. runoff) on a monthly basis; and,
- Estimate water storage volumes required to satisfy make-up demand during deficit periods.

2.0 <u>METHODOLOGY</u>

A hydrologic budget is essentially a climate-based accounting of the water gains and losses at a location or region. Temperature and precipitation records are used to develop the water budget, tabulating the additions, losses, and changes in water storage at a location. A simple water budget model was used for this analysis.

2.1 <u>MODEL DESCRIPTION</u>

The water budget model maintained and operated by the Meteorological Service of Canada (MSC), Environment Canada, was used for this analysis. The model is based on the Thornthwaite and Mather water balance procedure, and accounts for temperature, precipitation, snow storage and melt, evapotranspiration, and soil water holding capacity for the basin. Model input consists of mean daily temperature and precipitation data for the station and period of interest, station latitude, and site soil and vegetation cover information (used to estimate soil water holding capacity). The model generates a monthly water balance tabulation, from which total runoff is determined. Model background and additional details can be found in Johnstone and Louie (1983).

The Thornthwaite and Mather water balance procedure is commonly used for a wide variety of water resource planning applications, given its simplicity and basic data requirements. The MSC model improves on the procedure, by using daily temperature and precipitation data (as opposed to monthly), which permits better modeling of snowmelt and improves the accounting of snow storage (Johnstone and Louie, 1983). This is particularly important for applications in colder climates such as Canada. The model was considered appropriate for the level of analysis required.

2.2 <u>HYDROLOGY</u>

Model input consisted of daily temperature and precipitation data for the Weymouth Falls climate station, operated by the MSC (ID# 8206275), for the 35 year period from 1963 – 1997. The station is located approximately 16 km southeast of Whites Point at Weymouth Falls (44° 24'N, 65° 57'W) at an elevation of 11 m. The station was selected based on its proximity to the site and length of record. Any data gaps were filled with data from nearby stations, such as Meteghan River (ID# 8203500). Figure 2 shows the mean monthly precipitation and temperature data for the 35 year period.

Total contributing basin area was delineated for the project, based on 1:10,000 topographic mapping obtained from Service Nova Scotia and Municipal Relations, with 5 m contour interval (Map #10444450066100). The contributing area is shown

superimposed on the Concept Quarry Plan (Year 1 - 5) provided by Bilcon, which utilizes the same base mapping. The plan is reproduced here as Figure 3. Total contributing area was measured at 143 ha, and includes the entire topographic basin to the north of Whites Cove Road, and west and south of the natural topographic divide above the property line. The basin rises from sea level to an elevation of approximately 100 m at the topographic divide. Note that the property area to the south of Whites Cove Road was not included in the contributing drainage area, as it was assumed that runoff from this portion of the property would not drain across the road and would not be captured for use.

2.3 <u>SOILS/COVER INFORMATION</u>

Basin soils information along with vegetation cover was required to estimate soil water holding capacities required for model input. Soils information was obtained from soils surveys and mapping for the Digby County area (Hilchey *et. al.*, 1962). Additional soils information was also obtained from the Canadian Soil Information System (CanSIS) website and database.

The soil for the entire basin area is the Rossway Series, which is described as a very stony, sandy loam, and well drained with medium to rapid internal drainage (Hilchey *et. al.*, 1962). Based on a site visit and communication with Bilcon, it is apparent that soil cover along the steeper portions of the basin is extremely shallow, with frequent bedrock outcrops. Existing vegetation cover is predominantly forest of spruce, maple, fir, birch and poplar. Soil water holding capacities in the range of 100 – 250 mm were used given the soil type and cover information.

2.4 <u>LAND USE</u>

The contributing basin area was subdivided into varying land uses at the end of 5 or 10 year intervals over the 50 year project life, as delineated in Concept Quarry Plans provided by Bilcon (included here in Appendix B). Table 1 summarizes the varying land uses and their measured areas. Time steps of 0 (existing conditions), 5, 10, 15, 20, 30, 40 and 50 (reclaimed conditions) years were assessed in the analysis. Areas with different land use and cover characteristics were assigned different soil water holding capacities, giving slightly different model surplus water tabulations. Note that quarry areas, roads and other areas without soil were assigned a minimal water holding capacity of 25 mm.

2.5 <u>MODELING AND ANALYSIS</u>

Detailed monthly water budget output was obtained from the MSC water budget model for the Weymouth Falls climate data and various soil water holding capacities. Summary model output data is included in Appendix A.

2.5.1 <u>RUNOFF</u>

Monthly runoff amounts for each land use area with a different soil water holding capacity were calculated, based on surplus water determined from the model results. Surplus water is defined as the excess moisture available after the evapotranspiration demands of the surface have been met and soil water storage has been returned to the water holding capacity level. Individual runoff amounts were then summed for the entire basin area. Following the convention of the Thornthwaite and Mather method, it is assumed that 50% of the surplus water for any given month is detained in the watershed and contributes to runoff the following month.

2.5.2 <u>POND AREAS</u>

For sedimentation pond areas, the total direct monthly input was calculated as the sum of rainfall and snow melt over the ponds, as determined from the model. Evaporation losses for the ponds were estimated using lake evaporation data for the Kentville CDA climate station (ID#8202800), which is the closest MSC station for which lake evaporation data exists. The station is located approximately 150 km northeast of Whites Point, near Kentville, NS (45° 4′N, 64° 28′W). The data is based on 1971 – 2000 climate normals.

Pond seepage losses were estimated using Darcy's Law. The ponds will be excavated along the western edge of the property, in an area characterized by beach gravels and silt. Hydraulic gradient and conductivity values were estimated representative of pond location. Seepage estimates were kept constant for the analysis, however it is likely that seepage rates would decline over time as fines settle in the ponds and seal larger voids.

2.5.3 <u>WATER DEMAND</u>

Based on information obtained from Bilcon, process demand for aggregate washing operations is estimated to be approximately 5000 igpm (0.38 m³/s) for 16 hours per day, 264 days per year (i.e. 44 weeks x 6 days/week). It is assumed that 5 percent will be lost in the recycle process, or roughly 24,000 m³/month. This constitutes the plant make-up demand.

3.0 <u>RESULTS</u>

It is assumed that all runoff from the contributing drainage area (Figure 3) can be directed to the sedimentation ponds for collection and storage. This water plus the water collected directly by the ponds (i.e. rain plus melt above the ponds) constitutes the total available water for the basin.

Table 2 presents a summary of the results for the analysis, employing the information and assumptions discussed. The table presents the average *net* monthly water surplus volume once all losses and process demand have been accounted for. Values were calculated for basin conditions existing at the end of each time step, as outlined in Table 1. A negative value indicates a water deficit for that month, so that storage would be required to meet demand. The sum of consecutive deficit months indicates the total storage requirements for the time step, based on average climatic conditions. The results indicate that a net surplus of water exists for all months except August and September. The minimum storage requirements to satisfy demand during these months ranges from approximately 20,000 to 22,000 m³.

Detailed results for each time step considered are presented in Tables 3 through 10. The tables show monthly runoff volumes for the quarry and watershed areas and net water volumes collected directly by the ponds. Pond evaporation and seepage loss estimates are also shown.

Figures 4 through 11 show the distribution of surplus water from month to month and also present a simple mass diagram (Rippl plot) for each time step which indicates the cumulative supply and demand over the year and required storage during deficit periods. The mass diagram indicates excess supply when the slope of the supply curve is equal to or greater than the slope of the demand curve. Demand exceeds supply when the slope of the supply curve is less than that of the demand curve. Storage is determined by the maximum distance between the line parallel to the demand curve (drawn tangent to the supply curve) and the supply curve. The Rippl plot represents a visual indication of storage requirements, and storage values indicated in the figures correspond to those presented in Table 2 (i.e. 20,000 to 22,000 m³).

4.0 <u>CONCLUSIONS</u>

The results of the analysis indicate that little variation in the hydrologic budget exists for the various quarry phases, based on average climate data and given the abundant precipitation and size of contributing basin. Based on the above analysis it is evident that generally a net surplus of water is available, with the exception of the months of August and September, for each time step. For these months, storage of approximately 22,000 m³ would be required to satisfy demand.

As indicated earlier, the results represent average expected conditions, based on historical data for the Weymouth Falls climate station. It is recognized that actual water supply during the year and from year to year will fluctuate, so that sufficient supply may not always exist, depending on the size of storage facilities incorporated into the final site design.

5.0 <u>REFERENCES</u>

Canadian Soil Information System (CanSIS) - http://sis.agr.gc.ca/cansis/

Hilchey, J.D, Cann, D.B. and MacDougall, J.I. 1962. Soil Survey of Digby County Nova Scotia. Report No. 11, Nova Scotia Soil Survey, Truro Nova Scotia.

Johnstone, K. and Louie, P.Y.T. 1983. Water Balance Tabulations for Canadian Climate Stations. Hydrometeorology Division, Canadian Climate Centre, Atmospheric Environment Service.

Thornthwaite, C.W. and J. R. Mather. 1955: The Water Balance. Publications in Climatology, Vol. 8, No. 1, Drexel Institute of Technology, Centerton, New Jersey.



Figure 2 Whites Point Quarry Hydrologic Budget Average Precipitation & Temperature Weymouth Falls, NS



ZZZZ Precipitation ----- Temperature





Figure 4 Whites Point Quarry Hydrologic Budget Conceptual Layout - Year 0 (Existing)





Figure 5 Whites Point Quarry Hydrologic Budget Conceptual Layout - Year 5





Figure 6 Whites Point Quarry Hydrologic Budget Conceptual Layout - Year 10





Figure 7 Whites Point Quarry Hydrologic Budget Conceptual Layout - Year 15





Figure 8 Whites Point Quarry Hydrologic Budget Conceptual Layout - Year 20





Figure 9 Whites Point Quarry Hydrologic Budget Conceptual Layout - Year 30





Figure 10 Whites Point Quarry Hydrologic Budget Conceptual Layout - Year 40





Figure 11 Whites Point Quarry Hydrologic Budget Conceptual Layout - Year 50 (Reclaimed)





Table 1Whites Point Quarry Hydrologic BudgetLand Use / Area Summary

							Area (ha) by Year			
Area No.	Description	Land Use	WHC ¹ (mm)	0	5	10	15	20	30	40	50
1	Environmental Preservation Zone	Property buffer strip (cleared or forest)	250	0.0	11.7	11.7	11.7	11.7	11.7	11.7	11.7
2	Existing/Reclaimed Habitat	Existing use or future reclaimed areas	150	63.9	23.3	25.4	27.2	33.8	33.8	27.2	53.2
3	Existing Grubbed Area	Bare bedrock	25	3.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	Quarry Areas	Active quarrying	25	0.0	12.5	8.8	7.0	0.0 ²	0.0 ²	16.5	0.0
5	Processing Plant	Plant facilitities, aggregate piles, etc.	25	0.0	7.9	9.5	9.5	9.5	9.5	9.5	0.0
6	Sediment Ponds	Storage of runoff	-	0.8	9.6	9.6	9.6	9.6	9.6	9.6	9.6
7	Compound Area	Offices, power, fuel tanks, etc.	25	0.0	1.5	1.5	1.5	1.5	1.5	1.5	1.5
8	Roads	Roads	25	0.0	2.7	2.7	2.7	3.1	3.1	3.2	3.2
9	Sediment Disposal Area	Sediment from thickener tank	100	0.0	10.0	10.0	10.0	10.0	10.0	0.0	0.0
10	Clearcut Area	Cleared forest	75	11.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
11	Remainder of Drainage Area East of Property	Forest	250	64.2	64.2	64.2	64.2	64.2	64.2	64.2	64.2
			Total Land	142.6	133.8	133.8	133.8	133.8	133.8	133.8	133.8
			Total Pond	0.8	9.6	9.6	9.6	9.6	9.6	9.6	9.6
			Total	143.4	143.4	143.4	143.4	143.4	143.4	143.4	143.4

Notes: 1) Water holding capacity assigned based on soil type/landuse/cover.

2) Active quarrying outside of contibuting basin area during these time steps.



Month	Net Water Surplus ¹ (m ³ x 1000)												
	Year 0	Year 5	Year 10	Year 15	Year 20	Year 30	Year 40	Year 50					
Jan	125	107	107	107	106	106	107	129					
Feb	133	117	117	117	117	117	117	138					
Mar	156	140	140	140	140	140	140	164					
Apr	130	112	112	112	112	112	112	135					
May	96	69	69	69	68	68	69	92					
Jun	57	28	28	28	28	28	28	52					
Jul	34	3	3	3	3	3	3	27					
Aug	18	-12	-12	-12	-12	-12	-12	11					
Sep	16	-9	-9	-9	-9	-9	-8	13					
Oct	27	7	7	6	5	5	8	27					
Nov	74	62	61	61	59	59	62	80					
Dec	115	99	99	99	98	98	99	121					
Total	982	722	721	720	715	715	725	990					
Storage Required (m ³ x 1000)	N/A	21	21	21	22	22	20	N/A					

Table 2Whites Point Quarry Hydrologic BudgetSummary Results

<u>Notes:</u> 1) Represents available surplus water after all losses have been considered and demand satisfied. Negative values represent a water deficit.

Table 3Whites Point Quarry Hydrologic BudgetDetailed Summary TableQuarry Conceptual Layout - Year 0 (Existing)

	Qua	rry and Watershed	Areas			Pond Areas			Total Available	Make-up	Not Cumplus
Month	Water Surplus ¹ (mm)	Surface Runoff ² (mm)	Runoff Volume (m ³ x 1000)	Input ³ (mm)	Evaporation (mm)	Seepage Loss (mm)	Net Input (mm)	Volume (m ³ x 1000)	Water Supply (m ³ x 1000)	Demand ⁴ (m ³ x 1000)	$(m^3 \times 1000)$
Jan	95	88	125	100	0	48	52	0.4	125	n/a	125
Feb	98	93	133	102	0	43	59	0.5	133	n/a	133
Mar	125	109	156	135	0	48	88	0.7	156	n/a	156
Apr	73	91	130	103	0	46	56	0.5	130	n/a	130
May	44	68	96	103	96	48	-40	-0.3	96	n/a	96
Jun	13	40	58	92	108	46	-62	-0.5	57	n/a	57
Jul	8	24	35	86	121	48	-83	-0.7	34	n/a	34
Aug	2	13	18	80	105	48	-73	-0.6	18	n/a	18
Sep	9	11	16	99	75	46	-23	-0.2	16	n/a	16
Oct	27	19	27	102	47	48	8	0.1	27	n/a	27
Nov	84	52	73	130	0	46	84	0.7	74	n/a	74
Dec	109	80	115	119	0	48	71	0.6	115	n/a	115
Total	688	688	980	1250	552	561	137	1	982	n/a	982

Notes: 1) Sum of water surpluses from varying land-use areas within contibuting drainage area.

2) Runoff calculated as 50% of surplus for current month plus 50% of runoff from previous month.

3) Pond input is the sum of rainfall and snowmelt over pond areas.

4) Based on 5% process loss and 16 hr/day operation, 264 days/yr.

Table 4 Whites Point Quarry Hydrologic Budget Detailed Summary Table Quarry Conceptual Layout - Year 5

	Qua	rry and Watershed	Areas			Pond Areas	Total Available	Make-up	Net Cumulue		
Month	Water Surplus ¹ (mm)	Surface Runoff ² (mm)	Runoff Volume (m ³ x 1000)	Input ³ (mm)	Evaporation (mm)	Seepage Loss (mm)	Net Input (mm)	Volume (m ³ x 1000)	Water Supply (m ³ x 1000)	Demand ⁴ (m ³ x 1000)	$(m^3 \times 1000)$
Jan	95	88	126	100	0	48	52	5.0	131	24	107
Feb	98	93	133	102	0	43	59	5.6	139	22	117
Mar	125	109	156	135	0	48	88	8.4	164	24	140
Apr	73	91	130	103	0	46	56	5.4	135	23	112
May	44	68	96	103	96	48	-40	-3.9	93	24	69
Jun	13	40	58	92	108	46	-62	-5.9	52	23	28
Jul	8	24	35	86	121	48	-83	-8.0	27	24	3
Aug	2	13	19	80	105	48	-73	-7.0	12	24	-12
Sep	11	12	17	99	75	46	-23	-2.2	15	23	-9
Oct	30	21	30	102	47	48	8	0.8	31	24	7
Nov	87	54	77	130	0	46	84	8.0	85	23	62
Dec	109	82	116	119	0	48	71	6.8	123	24	99
Total	697	697	993	1250	552	561	137	13	1006	284	722

Storage Required: 21

Notes: 1) Sum of water surpluses from varying land-use areas within contibuting drainage area.

2) Runoff calculated as 50% of surplus for current month plus 50% of runoff from previous month.

3) Pond input is the sum of rainfall and snowmelt over pond areas.

4) Based on 5% process loss and 16 hr/day operation, 264 days/yr.

CRA 821191B

Storage Required: N/A



Table 5 Whites Point Quarry Hydrologic Budget Detailed Summary Table Quarry Conceptual Layout - Year 10

	Qua	rry and Watershed	Areas			Pond Areas		Total Available	Make-up	Not Cumplus	
Month	Water Surplus ¹ (mm)	Surface Runoff ² (mm)	Runoff Volume (m ³ x 1000)	Input ³ (mm)	Evaporation (mm)	Seepage Loss (mm)	Net Input (mm)	Volume (m ³ x 1000)	Water Supply (m ³ x 1000)	Demand ⁴ (m ³ x 1000)	(m ³ x 1000)
Jan	95	88	126	100	0	48	52	5.0	131	24	107
Feb	98	93	133	102	0	43	59	5.6	139	22	117
Mar	125	109	156	135	0	48	88	8.4	164	24	140
Apr	73	91	130	103	0	46	56	5.4	135	23	112
May	44	68	96	103	96	48	-40	-3.9	93	24	69
Jun	13	40	58	92	108	46	-62	-5.9	52	23	28
Jul	8	24	35	86	121	48	-83	-8.0	27	24	3
Aug	2	13	19	80	105	48	-73	-7.0	12	24	-12
Sep	11	12	17	99	75	46	-23	-2.2	15	23	-9
Oct	30	21	30	102	47	48	8	0.8	31	24	7
Nov	86	54	77	130	0	46	84	8.0	85	23	61
Dec	109	81	116	119	0	48	71	6.8	123	24	99
Total	696	696	992	1250	552	561	137	13	1005	284	721

Storage Required: 21

Notes: 1) Sum of water surpluses from varying land-use areas within contibuting drainage area.

2) Runoff calculated as 50% of surplus for current month plus 50% of runoff from previous month.

3) Pond input is the sum of rainfall and snowmelt over pond areas.

4) Based on 5% process loss and 16 hr/day operation, 264 days/yr.

Table 6Whites Point Quarry Hydrologic BudgetDetailed Summary TableQuarry Conceptual Layout - Year 15

	Qua	rry and Watershed	Areas			Pond Areas		Total Available	Make-up	Not Cumplus	
Month	Water Surplus ¹	Surface Runoff ²	Runoff Volume	Input ³	Evaporation	Seepage Loss	Net Input	Volume	Water Supply	Demand ⁴	wet Surplus
	(11111)	(1111)	(m x 1000)	(1111)	(11111)	(1111)	(11111)	(m [*] x 1000)	(m x 1000)	(m x 1000)	(m x 1000)
Jan	95	88	125	100	0	48	52	5.0	131	24	107
Feb	98	93	133	102	0	43	59	5.6	139	22	117
Mar	125	109	156	135	0	48	88	8.4	164	24	140
Apr	73	91	130	103	0	46	56	5.4	135	23	112
May	44	68	96	103	96	48	-40	-3.9	93	24	69
Jun	13	40	58	92	108	46	-62	-5.9	52	23	28
Jul	8	24	35	86	121	48	-83	-8.0	27	24	3
Aug	2	13	19	80	105	48	-73	-7.0	12	24	-12
Sep	10	12	17	99	75	46	-23	-2.2	15	23	-9
Oct	30	21	30	102	47	48	8	0.8	30	24	6
Nov	86	53	76	130	0	46	84	8.0	84	23	61
Dec	109	81	116	119	0	48	71	6.8	123	24	99
Total	695	695	990	1250	552	561	137	13	1003	284	720

Storage Required: 21

Notes: 1) Sum of water surpluses from varying land-use areas within contibuting drainage area.

2) Runoff calculated as 50% of surplus for current month plus 50% of runoff from previous month.

3) Pond input is the sum of rainfall and snowmelt over pond areas.

4) Based on 5% process loss and 16 hr/day operation, 264 days/yr.



Table 7Whites Point Quarry Hydrologic BudgetDetailed Summary TableQuarry Conceptual Layout - Year 20

	Qua	rry and Watershed	Areas			Pond Areas		Total Available	Make-up	Not Cumplus	
Month	Water Surplus ¹ (mm)	Surface Runoff ² (mm)	Runoff Volume (m ³ x 1000)	Input ³ (mm)	Evaporation (mm)	Seepage Loss (mm)	Net Input (mm)	Volume (m ³ x 1000)	Water Supply (m ³ x 1000)	Demand ⁴ (m ³ x 1000)	(m ³ x 1000)
Jan	95	88	125	100	0	48	52	5.0	130	24	106
Feb	98	93	133	102	0	43	59	5.6	138	22	117
Mar	125	109	156	135	0	48	88	8.4	164	24	140
Apr	73	91	130	103	0	46	56	5.4	135	23	112
May	44	68	96	103	96	48	-40	-3.9	92	24	68
Jun	13	40	58	92	108	46	-62	-5.9	52	23	28
Jul	8	24	35	86	121	48	-83	-8.0	27	24	3
Aug	2	13	19	80	105	48	-73	-7.0	12	24	-12
Sep	10	11	16	99	75	46	-23	-2.2	14	23	-9
Oct	28	20	28	102	47	48	8	0.8	29	24	5
Nov	85	53	75	130	0	46	84	8.0	83	23	59
Dec	109	81	115	119	0	48	71	6.8	122	24	98
Total	691	691	986	1250	552	561	137	13	999	284	715

Storage Required: 22

Notes: 1) Sum of water surpluses from varying land-use areas within contibuting drainage area.

2) Runoff calculated as 50% of surplus for current month plus 50% of runoff from previous month.

3) Pond input is the sum of rainfall and snowmelt over pond areas.

4) Based on 5% process loss and 16 hr/day operation, 264 days/yr.

Table 8 Whites Point Quarry Hydrologic Budget Detailed Summary Table Quarry Conceptual Layout - Year 30

	Qua	rry and Watershed	Areas			Pond Areas		Total Available	Make-up	Not Cumplus	
Month	Water Surplus ¹	Surface Runoff ²	Runoff Volume	Input ³	Evaporation	Seepage Loss	Net Input	Volume	Water Supply	Demand ⁴	Net Surplus
	(mm)	(mm)	(m ³ x 1000)	(mm)	(mm)	(mm)	(mm)	(m ³ x 1000)			
Jan	95	88	125	100	0	48	52	5.0	130	24	106
Feb	98	93	133	102	0	43	59	5.6	138	22	117
Mar	125	109	156	135	0	48	88	8.4	164	24	140
Apr	73	91	130	103	0	46	56	5.4	135	23	112
May	44	68	96	103	96	48	-40	-3.9	92	24	68
Jun	13	40	58	92	108	46	-62	-5.9	52	23	28
Jul	8	24	35	86	121	48	-83	-8.0	27	24	3
Aug	2	13	19	80	105	48	-73	-7.0	12	24	-12
Sep	10	11	16	99	75	46	-23	-2.2	14	23	-9
Oct	28	20	28	102	47	48	8	0.8	29	24	5
Nov	85	53	75	130	0	46	84	8.0	83	23	59
Dec	109	81	115	119	0	48	71	6.8	122	24	98
Total	691	691	986	1250	552	561	137	13	999	284	715

Storage Required: 22

Notes: 1) Sum of water surpluses from varying land-use areas within contibuting drainage area.

2) Runoff calculated as 50% of surplus for current month plus 50% of runoff from previous month.

3) Pond input is the sum of rainfall and snowmelt over pond areas.

4) Based on 5% process loss and 16 hr/day operation, 264 days/yr.



Table 9 Whites Point Quarry Hydrologic Budget Detailed Summary Table Quarry Conceptual Layout - Year 40

Quarry and Watershed Areas						Pond Areas	Total Available	Make-up	Not Sumplue		
Month	Water Surplus ¹ (mm)	Surface Runoff ² (mm)	Runoff Volume (m ³ x 1000)	Input ³ (mm)	Evaporation (mm)	Seepage Loss (mm)	Net Input (mm)	Volume (m ³ x 1000)	Water Supply (m ³ x 1000)	Demand ⁴ (m ³ x 1000)	$(m^3 \times 1000)$
Jan	95	88	126	100	0	48	52	5.0	131	24	107
Feb	98	93	133	102	0	43	59	5.6	139	22	117
Mar	125	109	156	135	0	48	88	8.4	164	24	140
Apr	73	91	130	103	0	46	56	5.4	135	23	112
May	44	68	96	103	96	48	-40	-3.9	93	24	69
Jun	13	41	58	92	108	46	-62	-5.9	52	23	28
Jul	8	24	35	86	121	48	-83	-8.0	27	24	3
Aug	2	13	19	80	105	48	-73	-7.0	12	24	-12
Sep	11	12	17	99	75	46	-23	-2.2	15	23	-8
Oct	31	22	31	102	47	48	8	0.8	32	24	8
Nov	87	55	78	130	0	46	84	8.0	86	23	62
Dec	109	82	117	119	0	48	71	6.8	123	24	99
Total	699	699	996	1250	552	561	137	13	1009	284	725

Storage Required: 20

Notes: 1) Sum of water surpluses from varying land-use areas within contibuting drainage area.

2) Runoff calculated as 50% of surplus for current month plus 50% of runoff from previous month.

3) Pond input is the sum of rainfall and snowmelt over pond areas.

4) Based on 5% process loss and 16 hr/day operation, 264 days/yr.

Table 10 Whites Point Quarry Hydrologic Budget Detailed Summary Table Quarry Conceptual Layout - Year 50 (Reclaimed)

	Qua	rry and Watershed	Areas			Pond Areas	Total Available	Make-up	Net Cumplus		
Month	Water Surplus ¹ (mm)	Surface Runoff ² (mm)	Runoff Volume (m ³ x 1000)	Input ³ (mm)	Evaporation (mm)	Seepage Loss (mm)	Net Input (mm)	Volume (m ³ x 1000)	Water Supply (m ³ x 1000)	Demand ⁴ (m ³ x 1000)	(m ³ x 1000)
Jan	95	87	124	100	0	48	52	5.0	129	n/a	129
Feb	98	93	132	102	0	43	59	5.6	138	n/a	138
Mar	125	109	156	135	0	48	88	8.4	164	n/a	164
Apr	73	91	130	103	0	46	56	5.4	135	n/a	135
May	44	68	96	103	96	48	-40	-3.9	92	n/a	92
Jun	13	40	58	92	108	46	-62	-5.9	52	n/a	52
Jul	8	24	35	86	121	48	-83	-8.0	27	n/a	27
Aug	2	13	19	80	105	48	-73	-7.0	11	n/a	11
Sep	9	11	16	99	75	46	-23	-2.2	13	n/a	13
Oct	26	19	27	102	47	48	8	0.8	27	n/a	27
Nov	83	51	72	130	0	46	84	8.0	80	n/a	80
Dec	109	80	114	119	0	48	71	6.8	121	n/a	121
Total	686	686	977	1250	552	561	137	13	990	n/a	990

Notes: 1) Sum of water surpluses from varying land-use areas within contibuting drainage area.

2) Runoff calculated as 50% of surplus for current month plus 50% of runoff from previous month.

3) Pond input is the sum of rainfall and snowmelt over pond areas.

4) Based on 5% process loss and 16 hr/day operation, 264 days/yr.

Storage Required: N/A

Tables 9 and 10

APPENDIX A

SUMMARY MODEL OUTPUT DATA

Weymout	h Fall	ls, M	1S	WATE	R BUDG	WBNRMS	D.025 ANS FOR	R THE F	PERIOD	1963-1	.997	DC20492
LAT. LONG	44 5 65	4.40 5.95	W/ LC	ATER HO DWER ZO	DLDING	CAPAC	ΙΤΥ	25 MM 15 MM	HE/ A.	AT IND	EX	29.75 .975
DATE	TEMP	(C)	PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
31- 1 28- 2 31- 3 30- 4 31- 5 30- 6 31- 7 31- 8 30- 9 31-10 30-11 31-12 AVE	-3.4 -3.5 .2 5.0 9.9 14.2 17.2 17.1 13.6 9.3 4.9 6 7.0	TTL	117 101 103 100 103 92 86 80 99 102 131 137 1251	59 53 79 97 103 92 86 80 99 102 128 98 1076	41 49 56 0 0 0 0 0 2 20 174	3 30 65 94 114 105 73 46 21 7 571	3 3 10 30 64 86 83 75 68 45 21 7 495	0 0 -1 -8 -31 -30 -5 -1 0 0 -76	97 98 125 73 44 14 9 5 20 52 20 52 106 112 755	35 34 2 0 0 0 0 0 0 1 19	25 25 25 20 12 6 17 22 25 25	491 590 695 795 898 990 1077 1157 1256 102 231 370
Weymout	th Fall	ls, I	NS	STAN	IDARD D	EVIAT	IONS F	OR THE	PERIOD	1963-	1997	DC20492
DATE	TEMP	(C)	PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	1.8 1.7 1.3 1.4 1.3 1.4 1.6 1.4 1.1 1.1 1.2 2.2		46 38 34 52 44 53 48 39 43 50	40 39 42 34 52 44 53 44 48 39 43 54	31 44 48 9 0 0 0 0 0 0 5 20	334 899 1096 554	3 3 4 9 16 33 29 14 5 4	0 0 3 12 32 13 4 0	55 60 65 33 45 22 24 12 35 36 43 52	49 37 8 0 0 0 0 0 0 4 27	0 0 9 11 10 11 7 0 0	106 106 120 141 155 172 186 190 200 39 59 91

Weymout	h Falls,	NS	WATE	R BUDG	WBNRMS	D.050 NS FOF	R THE F	PERIOD :	1963-1	.997	DC20492
LAT. LONG	44.4 65.9	10 WA 95 LC	TER HO WER ZO	LDING NE	CAPACI	ITY	50 MM 30 MM	HEA A.	AT IND	EX	29.75 .975
DATE	ТЕМР (С) PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
31- 1 28- 2 31- 3 30- 4 31- 5 30- 6 31- 7 31- 8 30- 9 31-10 30-11 31-12 AVE	-3.4 -3.5 .2 5.0 9.9 14.2 17.2 17.1 13.6 9.3 4.9 6 7.0 □	117 101 103 100 103 92 86 80 99 102 131 137 1251	59 53 79 97 103 92 86 80 99 102 128 98 1076	41 49 56 0 0 0 0 2 20 174	3 10 30 65 94 114 105 73 46 21 7 571	3 30 65 92 93 79 68 45 21 7 516	0 0 0 -2 -21 -26 -5 -1 0 0 -55	96 98 125 73 44 13 8 2 15 42 102 102 112 730	35 34 0 0 0 0 0 0 1 19	50 50 50 44 15 13 29 44 50	491 590 695 795 898 990 1077 1157 1256 102 231 370
Weymout	h Falls,	NS	STAN	DARD D	EVIATI	IONS FO	OR THE	PERIOD	1963-	1997	DC20492
DATE	ТЕМР (С	C) PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	1.8 1.7 1.3 1.4 1.3 1.4 1.6 1.4 1.1 1.1 1.2 2.2	46 38 43 52 44 53 44 48 39 43 50	40 39 42 34 52 44 53 44 48 39 43 54	31 44 48 9 0 0 0 0 0 0 5 20	3 4 8 9 10 9 6 5 5 4	3 4 9 10 28 28 13 6 5 4	0 0 0 4 27 30 12 3 0 0	55 665 345 23 61 35 45 52	49 37 8 0 0 0 0 0 0 4 27	0 0 12 20 20 20 20 14 0	106 106 120 141 155 172 186 190 200 39 59 91

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					1	WBNRMS	D.075					
Weymout	h Fal	ls, M	IS	WATE	R BUDG	SET MEA	ANS FOR	R THE I	PERIOD	1963-1	.997	DC20492
LAT. LONG	44 65	4.40 5.95	W/ LC	ATER HO DWER ZO	DIDING	CAPAC	ΙΤΥ	75 MM 45 MM	HE A.	AT IND	EX	29.75 .975
DATE	TEMP	(C)	PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
31- 1 28- 2 31- 3 30- 4 31- 5 30- 6 31- 7 31- 8 30- 9 31-10 30-11 31-12 AVE	-3.4 -3.5 5.9 14.2 17.1 13.6 9.3 4.9 6 7.0	TTL	117 101 103 100 103 92 86 80 99 102 131 137 1251	59 53 97 103 92 86 80 99 102 128 98 1076	41 49 56 0 0 0 0 0 2 20 174	3 30 65 94 114 105 73 46 21 7 571	3 30 65 94 103 84 69 45 21 7 534	0 0 0 -11 -21 -4 -1 0 0 -37	96 98 125 73 44 13 8 2 12 33 98 112 714	35 34 2 0 0 0 0 0 0 1 19	75 755 769 231 655 75 75	491 590 695 795 898 990 1077 1157 1256 102 231 370
Weymout	h Fa]]	ls, M	IS	STAN	IDARD D	EVIAT	IONS FO	OR THE	PERIOD	1963-	1997	DC20492
DATE	TEMP	(C)	PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	1.8 1.7 1.3 1.4 1.3 1.4 1.6 1.1 1.12 2		46 38 43 34 52 44 53 44 39 43 50	40 39 42 34 52 44 53 44 48 39 43 54	31 44 48 9 0 0 0 0 0 0 5 20	3 3 4 8 9 9 0 9 6 5 5 4	3 4 8 9 21 26 12 6 5 4	0 0 0 21 27 10 3 0	55 60 65 33 45 32 23 5 25 35 47 52	49 37 8 0 0 0 0 0 0 0 4 27	0 0 12 22 29 28 29 22 29 22 0 0	106 106 120 141 155 172 186 190 200 39 59 91

Weymout	h Falls	, NS	WATE	R BUDG	WBNRMS	D.100 ANS FOR	THE	PERIOD	1963-1	.997	DC20492
LAT. LONG	44. 65.	40 W. 95 L	ATER HO OWER ZO	DLDING	CAPAC	ιτγ1	.00 мм 60 мм	HE. A.	AT IND	EX	29.75 .975
DATE	ТЕМР (C) PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
31- 1 28- 2 31- 3 30- 4 31- 5 30- 6 31- 7 31- 8 30- 9 31-10 30-11 31-12 AVE	-3.4 -3.5 .2 5.0 9.9 14.2 17.2 17.1 13.6 9.3 4.9 6 7.0 T	117 101 103 100 103 92 86 80 99 102 131 137 TL 1251	59 53 79 97 103 92 86 80 99 102 128 98 1076	41 49 56 0 0 0 0 0 2 20 174	3 30 65 94 114 105 73 46 21 7 571	3 30 65 94 110 90 70 45 21 7 548	0 0 0 -5 -15 -3 -1 0 0 -24	96 98 125 73 44 13 8 2 9 28 92 112 700	35 34 2 0 0 0 0 0 0 1 19	100 100 100 94 79 47 36 55 83 100 100	491 590 695 795 898 990 1077 1157 1256 102 231 370
Weymout	h Falls	, NS	STAN	IDARD D	EVIAT	IONS FO	R THE	PERIOD	1963-	1997	DC20492
DATE	TEMP (C) PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$1.8 \\ 1.7 \\ 1.3 \\ 1.4 \\ 1.3 \\ 1.4 \\ 1.6 \\ 1.4 \\ 1.1 \\ 1.1 \\ 1.2 \\ 2.2 $	46 38 43 52 44 53 44 48 39 43 50	40 39 42 34 52 44 53 44 48 39 43 54	31 44 48 9 0 0 0 0 0 0 5 20	3 4 8 9 10 9 6 5 5 4	3 4 8 9 15 24 11 6 5 4	0 0 0 0 13 25 10 4 0	55 60 65 33 45 23 5 22 36 49 52	49 37 8 0 0 0 0 0 0 0 4 27	0 0 12 22 36 38 28 0	106 106 120 141 155 172 186 190 200 39 59 91

Weymout	h Fall	ls, N	IS	WATE	R BUDG	WBNRMS	D.150 ANS FOR	THE	PERIOD	1963-1	.997	DC20492
LAT. LONG	44	4.40 5.95	WA LC	ATER HO DWER ZO	DLDING	CAPAC:	ITY1	50 мм 90 мм	HE A.	AT IND	EX	29.75 .975
DATE	TEMP	(C)	PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
31- 1 28- 2 31- 3 30- 4 31- 5 30- 6 31- 7 31- 8 30- 9 31-10 30-11 31-12 AVE	-3.4 -3.5 5.0 9.9 14.2 17.2 17.1 13.6 9.3 4.9 6 7.0	TTL	117 101 103 100 103 92 86 80 99 102 131 137 1251	59 53 79 97 103 92 86 80 99 102 128 98 1076	41 49 56 6 0 0 0 0 0 2 20 174	3 30 65 94 114 105 73 46 21 7 571	3 30 65 94 114 98 71 45 21 7 561	0 0 0 -1 -7 -2 -1 0 0 -11	95 98 125 73 44 13 8 2 9 26 84 110 687	35 34 0 0 0 0 0 0 1 19	150 150 150 144 129 93 73 92 124 148 150	491 590 695 795 898 990 1077 1157 1256 102 231 370
Weymout	h Fall	ls, N	IS	STAN	IDARD D	EVIAT	IONS FO	R THE	PERIOD	1963-	1997	DC20492
DATE	ТЕМР	(C)	PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
$\begin{array}{r} 31-1\\ 28-2\\ 31-3\\ 30-4\\ 31-5\\ 30-6\\ 31-7\\ 31-8\\ 30-9\\ 31-10\\ 30-11\\ 31-12\\ \end{array}$	$1.8 \\ 1.7 \\ 1.3 \\ 1.4 \\ 1.3 \\ 1.4 \\ 1.6 \\ 1.4 \\ 1.1 \\ 1.2 \\ 2.7 \\ 1.2 $		46 38 43 34 52 44 53 44 48 39 43 50	40 39 42 34 52 44 53 44 48 39 43 54	31 44 48 9 0 0 0 0 0 0 0 5 20	3 4 8 9 9 10 9 6 5 5 4	3 4 8 9 10 17 9 6 5 4	0 0 0 0 4 17 6 3 0 0	55 60 65 33 45 23 52 21 36 53	49 37 8 0 0 0 0 0 0 0 4 27	0 0 12 22 42 48 51 39 7 0	106 106 120 141 155 172 186 190 200 39 59 91

Weymout	h Falls,	NS	WATE	R BUDG	WBNRMS	D.250 ANS FOR	THE	PERIOD	1963-1	.997	DC20492
LAT. LONG	44.4 65.9	10 WA 05 LC	ATER HO DWER ZO	DLDING	CAPAC	ΙΤΥ2 1	50 мм 50 мм	HE. A.	AT IND	EX	29.75 .975
DATE	ТЕМР (С) PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
31- 1 28- 2 31- 3 30- 4 31- 5 30- 6 31- 7 31- 8 30- 9 31-10 30-11 31-12 AVE	-3.4 -3.5 .2 5.0 9.9 14.2 17.2 17.1 13.6 9.3 4.9 6 7.0 □	117 101 103 100 103 92 86 80 99 102 131 137 1251	59 53 79 97 103 92 86 80 99 102 128 98 1076	41 49 56 0 0 0 0 0 2 20 174	3 30 65 94 114 105 73 46 21 7 571	3 3 10 30 65 94 114 104 73 45 21 7 569	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	94 98 125 73 44 13 8 2 9 25 81 108 680	35 34 2 0 0 0 0 0 0 1 19	250 250 250 244 229 192 167 184 216 244 248	491 590 695 795 898 990 1077 1157 1256 102 231 370
Weymout	h Falls,	NS	STAN	DARD D	EVIAT	IONS FO	R THE	PERIOD	1963-	1997	DC20492
DATE	ТЕМР (С) PCPN	RAIN	MELT	PE	AE	DEF	SURP	SNOW	SOIL	ACC P
$\begin{array}{r} 31-1\\ 28-2\\ 31-3\\ 30-4\\ 31-5\\ 30-6\\ 31-7\\ 31-8\\ 30-9\\ 31-10\\ 30-11\\ 31-12\\ \end{array}$	$1.8 \\ 1.7 \\ 1.3 \\ 1.4 \\ 1.3 \\ 1.4 \\ 1.6 \\ 1.4 \\ 1.1 \\ 1.1 \\ 1.2 \\ 2.2$	46 38 43 34 52 44 53 44 48 39 43 50	40 39 42 34 52 44 53 44 48 39 43 54	31 44 48 9 0 0 0 0 0 0 0 5 20	3 4 8 9 10 9 6 5 5 4	3 4 8 9 10 9 6 6 5 4	00000072200	57 60 65 33 45 32 23 5 21 36 55	49 37 8 0 0 0 0 0 0 4 27	0 0 12 22 44 58 62 51 21	106 106 120 141 155 172 186 190 200 39 59 91

APPENDIX B

QUARRY CONCEPT PLANS









Buxton & Kern







