Aquatic Field Survey Photos



Photo 1: LaPlanche River, 5 m upstream from the bridge



Photo 2: LaPlanche River, facing tributary



Photo 3: Tributary to the right of LaPlanche River at 977m upstream from bridge, facing culvert, note: white foam in stream



Photo 4: Wooden culvert of tributary, 977m upstream LaPlanche River from bridge



Photo 5: LaPlanche River, at aboiteau area (to the right)



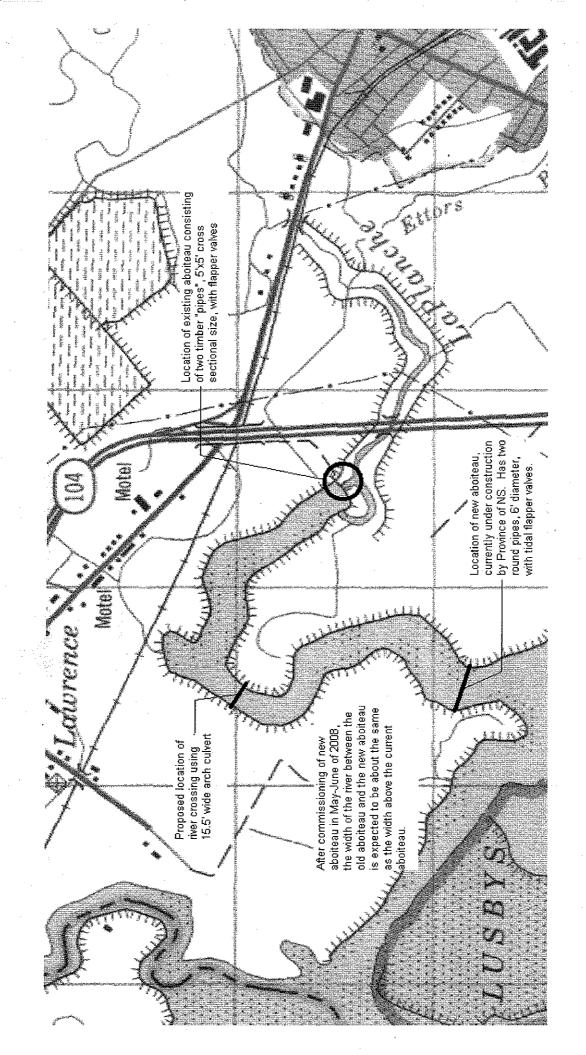
Photo 6: Estuary leading to the Bay of Fundy, other side of aboiteau from LaPlanche River

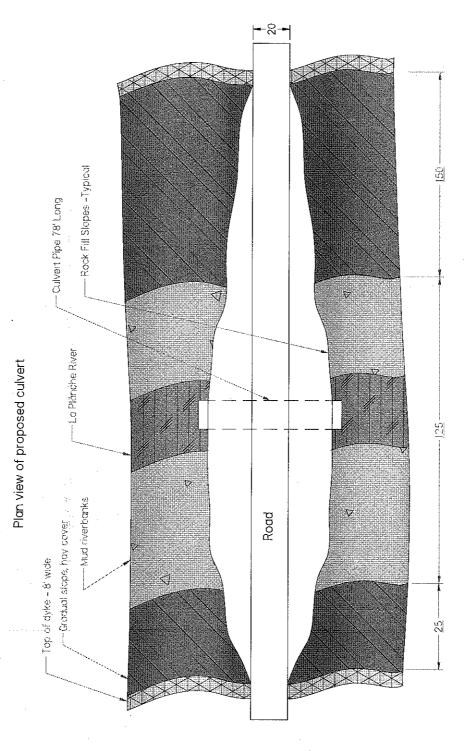


Photo 7: Tributary of LaPlanche River

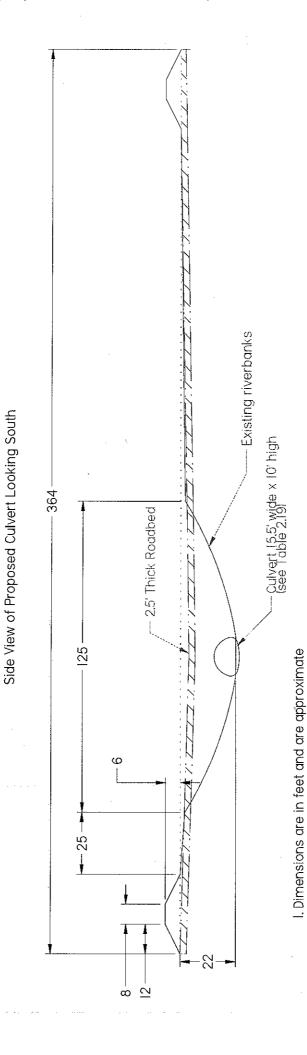


Photo 8: Tributaries of LaPlanche River



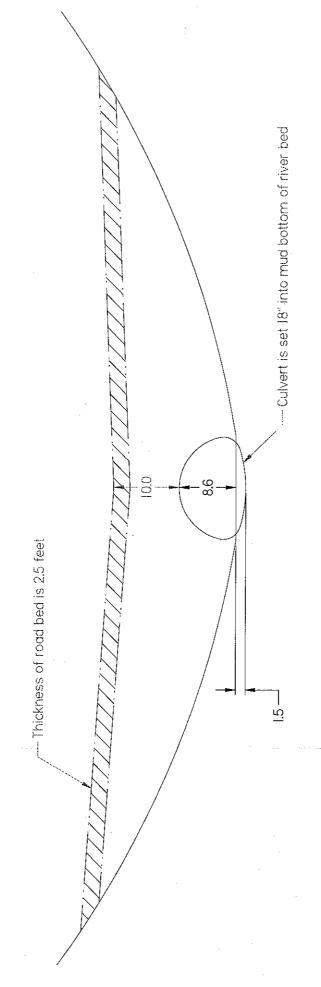


I. Distances are in feet and are approximate.



3. Dykes are no longer required, and will be removed

2. Dykes are same size and shape



Side View Culvert Detail

I. All units in feet unless otherwise specified

Figure 4. Rating Curve Plot for Crossing: Culvert arch pipe

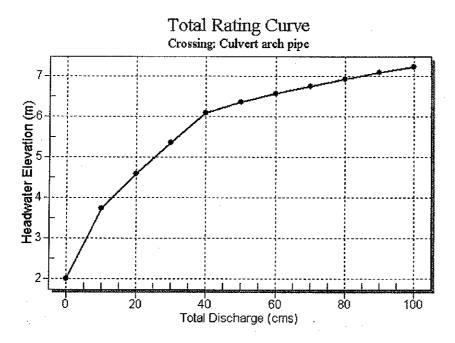
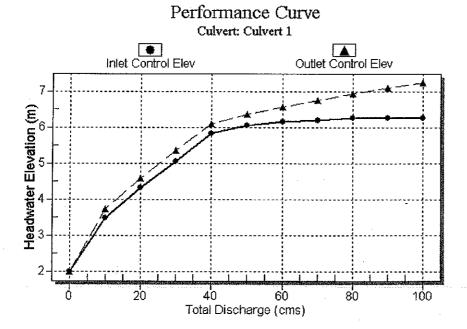


Figure 5. Culvert Performance Curve Plot



HY-8 Culvert Analysis Report

1. Project Units: SI Units (Metric)

2. Summary of Culvert Flows at Crossing: Culvert arch pipe

Headwater Elevation (m)	Total Discharge (cms)	Culvert 1 Discharge (cms)	Roadway Discharge (cms)	Iterations
2.00	0.00	0.00	0.00	1
3.73	10.00	10.00	0.00	1
4.58	20.00	20.00	0.00	1
5.36	30.00	30.00	0.00	1
6.09	40.00	39.05	0.94	8
6.36	50.00	41.44	8.57	4
6.57	60.00	42.43	17.56	4
6.75	70.00	42.78	27.22	4
6.93	80.00	43.26	36.74	4
7.09	90.00	43.31	46.69	4
7.23	100.00	43.32	56.68	4

3. Culvert Summary Table

Total Discharge (cms)	Culvert Discharge (cms)	Headwater Elevation (m)	Inlet Control Depth (m)	Outlet Control Depth (m)	Flow Type	Normat Depth (m)	Critical Depth (m)	Outlet Depth (m)	Tailwater Depth (m)	Outlet Velocity (m/s)	Tailwater Velocity (m/s)
0.00	0.00	2.00	0.000	0.000	0-NF	0.000	0.000	0.000	0.000	0.000	0.000
10.00	10.00	3.73	1.482	1.734	3-M2t	2.193	0.958	1.350	1.320	1.863	1:041
20.00	20.00	4.58	2.326	2.583	3-M2t	3.152	1.417	1.804	1.774	2.709	1.240
30.00	30.00	5.36	3.063	3.356	3-M2t	3.152	1.783	2.131	2.101	3.441	1.373
40.00	39.05	6.09	3.830	4.088	3-M2t	3.152	2.069	2.395	2.365	4.033	1.476
50.00	41.44	6.36	4.062	4.362	3-M2t	3.152	2.140	2.621	2.591	3.981	1.561
60.00	42.43	6.57	4.164	4.570	7-M2t	3.152	2.170	2.820	2.790	3.868	1.634
70.00	42.78	6.75	4.199	4.754	7-M2t	3.152	2.181	2.999	2.969	3.793	1.699
80.00	43.26	6.93	4.250	4.932	4-FFf	3.152	2.195	3.152	3,134	3.755	1.756
90.00	43.31	7.09	4.254	5.088	4-FFf	3.152	2.196	3.152	3.286	3.759	1.809
100.00	43.32	7.23	4.256	5.231	4-FFf	3.152	2.197	3.152	3,427	3.760	1.857

4. Downstream Channel Rating Curve (Crossing: Culvert arch pipe)

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Numbe
0.00	2.00	0.00	0.00	0.00	0.00
10.00	3.11	1.11	1.40	0.07	0.30
20.00	3.50	1.50	1.67	0.09	0.32
30.00	3.78	1.78	1.85	0.11	0.33
40.00	4.01	2.01	1.98	0.13	0.33
50.00	4.20	2.20	2.10	0.14	0.34
60.00	4.37	2.37	2.20	0.15	0.34
70.00	4.53	2.53	2.29	0.16	0.34
80.00	4.67	2.67	2.36	0.17	0.35
90.00	4.80	2.80	2.43	0.17	0.35
100.00	4.92	2.92	2.50	0.18	0.35

Table 1-7 Continued. Handling Weight of Hound Corrugated Steel Pipe (152x51 mm)

(Estimated Average Masses-Not for Specification Use)

			Approximat	e Mass (kg/n	n) Balts Incl.		Periphery
Inside Diam.	Waterway Area		Specifie	d Wall Thickne	ss — mm	·	Hole Spaces
(act)	(m²)	3.0	4.0	5.0	5.0	7.0	N
6160 6470 6780	29.79 32.87 30.30	680 711 748	889 930 978	1100 1150 1210	1309 1370 1440	1519 1589 1671	84A 84N 82N
7090 7400 7710	39.48 43.01 46.70	779 809 846	1019 1060 1108	1260 1311 1370	1501 1561 1631	1741 1812 1893	100N 196N 1989
8020	50.53	B77	1149	1421	1692	1963	LOAN

Omeansions shown not for specification purposes, subject to manufacturing tolerances. $N = 244 \ \mathrm{mm}$.

4720 mm

7215

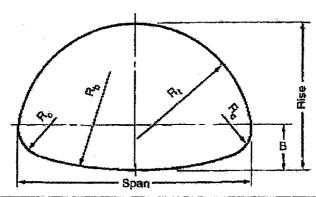
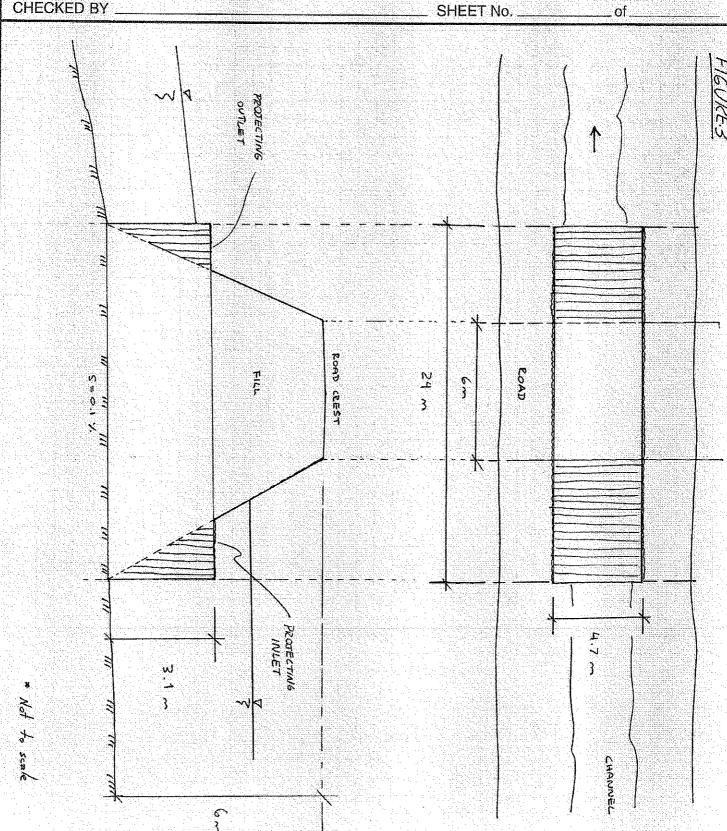


Table 1-8 Sizes and Layout Details—Structural Plate Pipe Arches Corrugation Profile: 152 x 51 mm

	Pime:	nsions	Waterway	-	Layout Dimer	nsions man		Periphery (Hole
	Span (rum)	Rise (mm)	Area (m²)	B .	,Rę	R _c	R _b	Spaces) N
2 4	2060	1520	2.49	700	113D	660	1875	24N
	2240	1630	2.90	580	1205	660	3370	26N
	2440	1750	3.36	730	1305	685	2995	28N
	2590	1880	3.87	735	1355	710	4420	30N
	2690	2080	4.49	815	1380	785	4050	32N
	3109	1980	4.83	790	1695	685	3850	34N
	> 3400	792010	5.28	840	2000	660	3510	36N
_//	3730	2290	6,61	970	2055	710	4045	40N
	3890	2690	829	915	1975	815	6015	44N
	4370	2870	9,76	1035	2265	815	4895	48N
PS	→ 4720 5050	3070 i) a 3330		1015 1040	2425 2570	815 840	6430 7430	52N - 56N
•	5490	3530	15.10	1095	2790	840	7575	608
	5890	3710	17.07	1180	3020	840	7755	64N
	6250	3910	19.18	1120	3175	840	9630	68N
	7040	4060	22.48	1660	409D	1370	9650	74H
	7620	4240	25.27	1750	457D	1370	9650	79N





- Span	15. E. S.	2
		£
	Springline Rise	m

lable 2.19	Struc 152	X X	gated pipe ugation pr	e-arch ofile							- m -	€)			A
	Stan	idard dimensions and unit weight of structure (assembled)	and unit w	eignt or	structu	re (assem	(peq)				-		•		
		Ţ		Layout Di	Layout Dimensions	**		Requi	Required N		Unit Weight of Structure, kg/m, Bolts included	nt of Strue	cture, kg/	m, Bolts	Included
Span	Rise,	Area		lio lieu l	(to neutral axis), mm			Each			ශී	Specified Wall Thickness,	all Thick	ness, mm	
mm	mm	m²	8	ď	E,	. R _b	Top	Corner	Bottom	Total	3.0	4.0	5.0	0.0	7.0
2060	1520	2.49	200	1130	999	1875	6	S	ស	24	210	274	339	403	467
2240	1630	2.90	089	1205	999	3370	F	ഹ	ιΩ	82	232	305	373	443	513
2440	1750	3.36	730	1305	88	2995	12	Ŋ	9	83	248	323	388	473	548
5280	1880	3.87	735	1355	75	4450	7	2	ç	ස	88	343	423	203	583
5690	2080	4,49	815	1380	785	4050	\$	цņ	g.	32	582	371	458	544	630
3100	1980	4.83	790	1695	982	3850	ŧ	r,	රා	ä	\$	384	474	564	654
3400	2010	5.28	840	2000	099	3510	\$	ß	}-	8	316	412	208	8	700
3730	2290	6.61	906	SSS 285	710	4045	∞	150	42	\$	346	452	229	569	771
3830	2690	8,29	915	1975	815	6015	প্ত	'n	-	4	384	50	618	8	852
4370	2870	9.76	1035	2265	815	4895	25	ഹ	7	8	414	541	699	86	922
4720	3070	11.38	1015	2425	815	6430	27	5	15	22	445	285	719	929	993
2020	3330	13.24	1040	22.92	840	7430	99	ις.	16	99	489	929	787	936	1085
5490	3530	15.10	1095	2790	840	7575	33	ĽΩ	82	8	513	671	823	987	1145
2890	3710	17.07	1150	3020	940	7755	뚕	S	ಜ	64	224	727	897	1067	1237
6250	3910	19.18	1120	3175	840	9630	37	S	77	88	588	767	848	1128	1308
7040	4060	22.48	1660	4090	1370	9650	હ્ય	=	27	74	663	851	1050	1248	1447
7620	4240	25.27	1750	4570	1370	9650	33	11	24	79	629	887	1096	1304	1513

*Refer to diagram above this table.
NOTES: Pipe-arch structures generally require more care in design and installation than round structures, particularly in the larger sizes.
All dimensions are finside unless otherwise noted.

Proposed Culvert Design Information

The proposed culvert would be a clear span culvert, installed in the dry (with water control in place) during a period between the middle of July and the end of September. It has been sized to ensure fish passage and will be installed in a crushed stone bed. The culvert will be embedded (30 %) to ensure confluence with the river bottom, so as not to create an impediment to fish passage. Culvert construction is planned for several months past the planned commissioning of the new aboiteau structure (currently planned for May, 2008) which would be downstream of the culvert.

The culvert design was originally proposed by Hank Kolstee, the Marshlands Administator (see attached figures) and was confirmed by Jacques Whitford, based on existing available flow information for LaPlanche River, namely a report done by Con Desplague (1983). Following the construction of the new aboiteaux, flow modelling will be conducted to confirm assumptions regarding the river and watershed characteristics utilized in the design of the culvert (flow data from 1983). Should the characteristics differ from assumptions used; current river characteristics established through flow modelling will be used to modify design.

The proposed culvert is a structural plate pipe arch (span 4720 mm, rise 3070 mm) with a length of 24 m and a bottom slope of 1% (based on client feedback). The geometric characteristics of the culvert are attached.

In addition, a new aboiteau structure will be commissioned downstream from the proposed culvert location. As a consequence, the Department of Fisheries and Oceans (DFO) made a request to the client to verify that the culvert size is appropriate.

Field data and required assumptions

All the available background information and assumptions are indicated below. These were made based on client feedback, aerial photographs, maps, and established hydraulic therories and practices.

The design flow was obtained from a report done by Mr. Con Desplague (1983). The document indicates that due to the large storage capacity within the LaPlanche River watershed, the 1:100 year peak flow is attenuated to a flow of 10 m³/s. The culvert was analyzed for both flows (design flow of 10 m³/s and maximum flow of 100 m³/s).

As indicated previously, the proposed culvert has dimensions of 4720 mm x 3070 mm (span x rise) with a length of 24 m. The channel slope for the LaPlanche River was calculated based on the Desplague report that indicates a drop in elevation of 3.3 m in a distance of 7530 m for an average slope of 0.000438 (0.0438%). Since the report indicates variations in slope along the channel, a slope of 0.001 (0.1%) was assumed at the proposed location.

The tailwater channel was assumed to be trapezoidal with a bottom width of 2 m and a side slope of 4H:1V. The Manning's roughness coefficient was established at 0.024 and the channel bottom elevation was assumed at 2 m.

The roadway crest elevation was assumed at 6 m with a length of 50 m (approximate distance across the channel) and a top width of 6 m with a gravel surface.

Culvert characteristics were included and an inlet type was assumed (projecting inlet).

Finally, the inlet and outlet stations and elevations were also defined with a culvert slope of 0.001 (0.1)% which is considered to be appropriate for the site.

Methodology

The culvert design method requires checking for two main scenarios: inlet control and outlet control. Each flow regime has different requirements that are a function of many parameters (*i.e.*, culvert shape and size, slope, roughness coefficient, inlet type, etc).

For simple cases the design procedure can be carried out by hand with the aid of culvert design monographs and simple mathematical equations. However, due to the complexity of the culvert shape in this case is more efficient to design the culvert with the aid of computer software. The software that was utilized was developed by the U.S. Federal Highway Administration (USFHWA) and is called HY-8. The software allows for the input of all relevant parameters and calculates all possible scenarios for the specified flows.

The results of the HY-8 run for the proposed culvert are included in the following section.

Results

The rating curve and the performance curve for the culvert are attached.

Both figures indicate the expected culvert capacity under the design conditions. For a flow of 10 m³/s the headwater elevation will be in order of 3.5 m (outlet control). As the flow increases the headwater elevation also increases until the roadway is overtopped. Road overtopping happens at 6 m with a flow rate of 40 m³/s, however, the chance of overtopping can be minimized with a higher elevation of the road crest. The assumed elevation was set at 6 m, if a higher elevation is defined the culvert performance curve will be slightly different.

HY-8 also indicated that the culvert will be in outlet control between 0 m³/s and 100 m³/s, this means that the slope of the channel defines the amount of water that can flow through the culvert rather than the culvert inlet.

In summary, the culvert seems to be properly sized for a design flow of 10 m³/s. A smaller culvert is not recommended due to the uncertainty with respect to the maximum peak in the channel.

P:\envsci\100xxx\1005774 amherst wind farm\draft report for environmental assessment\Appendices\Appendix D-Bird Surveys\Proposed Culvert Design Information.doc