

PR 87-003

REVIEW OF THE EXPLORATION PROGRAM
PERFORMED BY

ONITAP RESOURCES INC.

IN THE
GOLDBOROUGH AREA, GUYSBOROUGH COUNTY
NOVA SCOTIA

DECEMBER, 1987

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MINES
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December 1987.

REVIEW OF THE EXPLORATION PROGRAM PERFORMED
BY ONITAP RESOURCES INC. IN THE
GOLDBORO AREA - GUYSBOROUGH COUNTY
NOVA SCOTIA.

INTRODUCTION:

Narex Ore Search Consultants Inc. has optioned on behalf of Onitap Resources Inc. a property of 53 claims at Goldboro, Guysborough County, Nova Scotia. The claims cover the sites of four old gold mines which have been abandoned for many years. Access to the area is excellent. Gold is known to occur in strata-bound quartz veins within the slate beds of the Goldenville Formation.

By the end of November 1987, a total footage of 37,810 ft. of diamond drilling had been completed on the property and distributed as follows:

1984: one deep 1737 ft. hole down-dip from the Boston-Richardson mine.

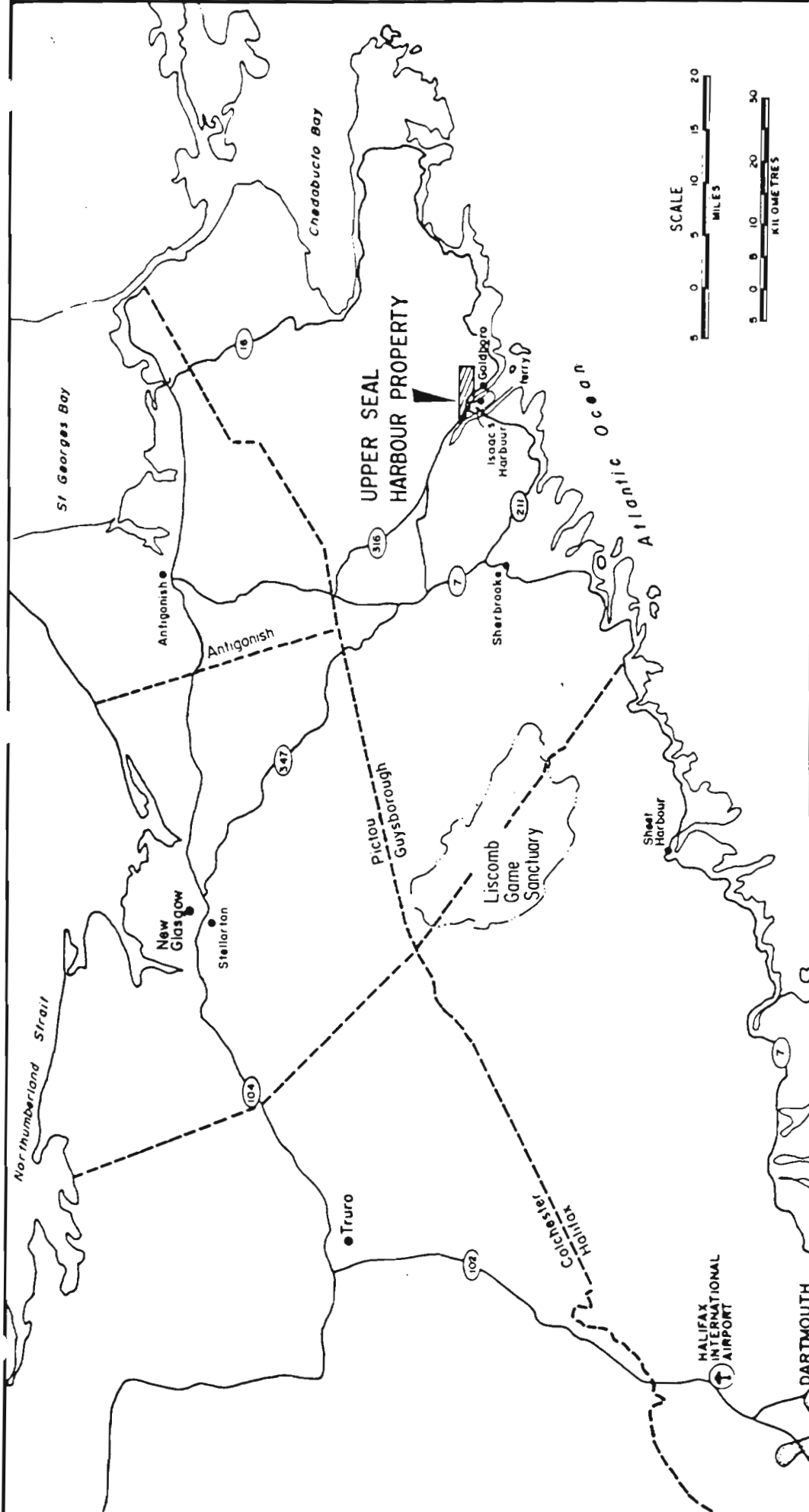
1985: several short holes in the immediate vicinity of the old West Goldbrook mine totalling 1279 ft.

1987: from January to March 5: five holes totalling 6,314 ft. funded and managed by Petromet Resources Limited and Greenstrike Gold Corporation down-dip from the Boston-Richardson mine.

Since May 11, 1987: 23 holes totalling 28,480 ft. also in the vicinity of the Boston-Richardson mine.

PROPERTY:

The property is located approximately one mile north of the village of Goldboro, Nova Scotia (Fig.1). It is shown on the Nova Scotia Department of Mines Sheet No. 11F4D, known as Country Harbour. The property consists of two claim groups, the first of 37 contiguous claims, approximately 40 acres in size (1320 x 1320 feet), for a total of 1,480 acres (Fig.2). The second is a 16 claim group of 640 acres, located one mile east of the 37 claims. The first claim block extends from the head of Isaac's Harbour, eastward for 2.5 miles, and encompasses several old gold mines (Dolliver Mountain, West



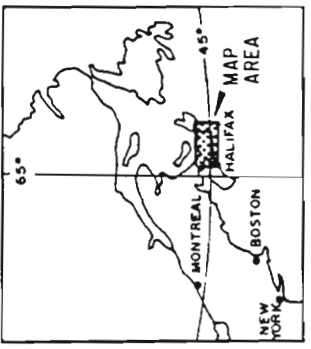
ONITAP RESOURCES INC.

UPPER SEAL HARBOUR DISTRICT
BOSTON - RICHARDSON MINE

LOCATION MAP

Scale as indicated
Drawing No. Figure 1
Date February 7, 1987

MAREX Ore Search Consultants Inc.

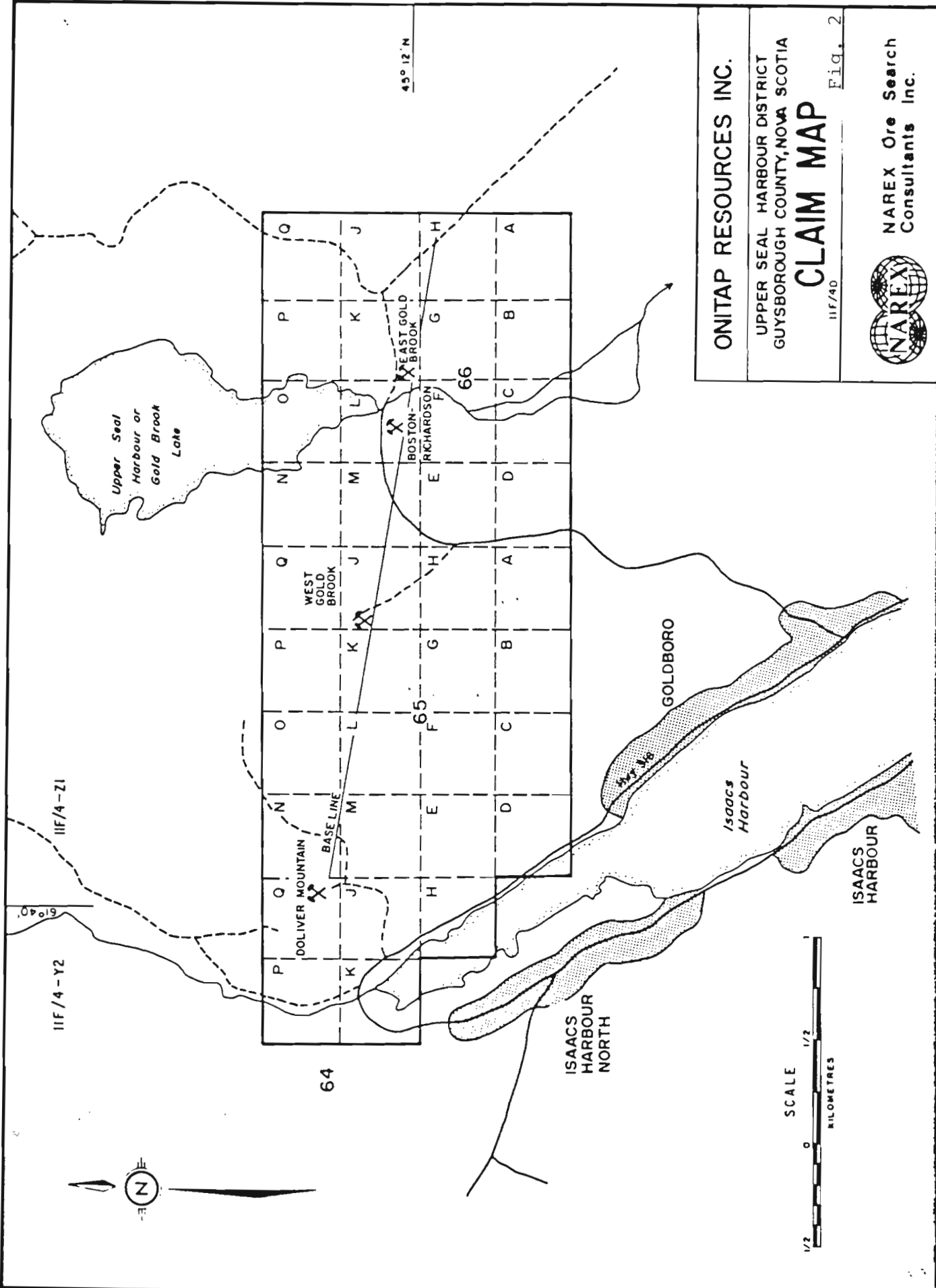


— (147) — Roads
- - - - - County Boundaries

HALIFAX INTERNATIONAL AIRPORT

DARTMOUTH

HALIFAX



ONITAP RESOURCES INC.

UPPER SEAL HARBOUR DISTRICT
GUYSBOROUGH COUNTY, NOVA SCOTIA

CLAIM MAP

III/40 Fig. 2

NAREX

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Consultants Inc.

Goldbrook, Boston Richardson and East Goldbrook). Immediately to the east the next 16 claim block is held by Seabright Resources, Onitap's second block of 16 claims follows immediately to the east.

The claim numbers are :

Tract 64- Claims H, J, K, P, Q.

Tract 65- Claims A, B, C, D, E, F, G, H, J, K, L, M, N, O, P, Q.

Tract 66- Claims A, B, C, D, E, F, G, H, J, K, L, M, N, O, P, Q.

These claims are covered by development license #10491 dated November 29, 1987 and issued for one year.

Tract 68- Claims A, B, C, D, E, F, G, H, J, K, L, M, N, O, P, Q are covered by exploration license 11584 dated March 17, 1986 and issued for a 2nd year commencing March 17, 1987.

Surface Rights:

The surface rights are held by various private landholders and by the Nova Scotia Department of Lands and Forests. The private lands form a series of narrow strips orientated southwest to northeast. The Crown Lands cover the area around the Boston-Richardson mine and the anticlinal axis to the eastern limit of the 37 claim group.

LOCATION AND ACCESS:

The villages of Goldboro and Isaac's Harbour are located on the eastern shore of Nova Scotia, in Guysborough County, approximately 165 km northeast of Halifax. (latitude 45 degrees 11' 30" to 45 degrees 12' 30"; longitude 61 degrees 37' 30" to 61 degrees 40' 40"; NTS 11F/4 -Country Harbour). The fishing village (named after the harbour) lies on the western shore of the harbour, on Highway #316, opposite the village of Goldboro. A gas station, a general store and a post office are the services available in those two communities. All other services are available at the town of Sherbrooke (50 km by road to the west) or from the town of Antigonish 80 km away. The nearest commercial air service is at Halifax.

Access to the claims is excellent. Good gravel roads from Highway #316 pass through the centre of the claim block.

GENERAL DESCRIPTION:

The claims are located between 200 and 250 feet above sea level in an area of gently rolling hills. The shoreline of the harbour rises slowly to about 250 feet over one quarter of a mile. The area is covered with boulder-filled gravels, sandy clay, tills and muskeg. Outcrops of bedrock are rare; probably about one per cent. Approximately one-fifth of the property is covered with swamps. One large lake, Seal Harbour Big Lake (also known as Goldbrook Lake), covers a portion of the claims and drains southward. The area has been cut over and is now covered by secondary growth of tag alders, maple, birch, spruce, balsam and tamarack.

The climate is moderated by the Atlantic Ocean and ranges from an average summer temperature of 70 degrees F to a winter average of 26 degrees F. There is little snow accumulation.

HISTORY:

Gold was first discovered on the Isaac's Harbour Anticline, in quartz veins, in 1861. In 1892, tracing by the Geological Survey of the Upper Seal Harbour Anticline, revealed a band of quartz veins known as the Richardson Belt (later the Boston-Richardson Mine). The Richardson Mine operated until 1912 from two vertical shafts (depths of 170 and 440 feet) and one inclined shaft with much lateral drifting. From a total of 375,000 tons of ore mined, 50,000 ounces of gold were recovered. Grade control was poor and little exploration work was done. In 1926, the property was acquired by the Metals Mining and Smelting Corporation of Canada Ltd. They attempted to recover the auriferous arsenopyrite from the tailings during 1926-1927. Since then the property has been dormant.

Other discoveries of gold on the Upper Seal Harbour Anticline, led to the development of the Dolliver Mountain, East Goldbrook, and West Goldbrook Mines.

The Dolliver Mountain Mine was discovered in the early 1890's and development proceeded until a shaft of 488 feet cut several orebodies. In 1905, a drillhole 500 feet below the shaft, gave unsatisfactory results and the mine was allowed to flood. It has since remained idle. Figures of 205 ounces of gold from 8,059 tons were reported for this mine.

The East Goldbrook Mine was discovered in 1906 and a shaft

was sunk to 175 feet with some cross-cuts. Between 1931 and 1934, Renada Mines Ltd. dewatered and sampled the shaft. Assays from their chip sampling and six, one ton samples, gave values of 0.052 to 0.137 oz. Au per ton.

In 1909, the New England Mining Company cleaned an old 85 foot shaft and did some lateral work on what is known as the West Goldbrook Mine.

In 1929, Locarno Copper Mines Ltd. sank a shaft to 100 feet on the Nugget Lead, west of the New England shaft. A metallurgical test in 1931 recovered 1.61 oz. of Au from 1.1 tons of ore. In 1956, the Canso Mining Corporation dewatered the shaft and did some cross-cutting to locate a previously intersected ore shoot (58 feet assaying approximately 0.51 oz. Au/ton). Work was stopped because of the company's financial difficulties.

In addition to the old mine sites located on this claim block and their associated development work described above, the only other work recorded was done by Patino Mines (Quebec) Ltd. in the summer of 1981. The claims in Tracts 65 and 66 were covered by EM-16 and magnetometer surveys over a grid with lines spaced at 75 m, and station intervals of 25 m. The results of the magnetometer survey indicated a generally low magnetic gradient for the area. This would suggest that the underlying sedimentary sequence is of a relatively uniform nature. The EM-16, VLF survey outlined a conductive trend associated with the anticlinal structure, which passes through the old mine sites.

In 1984, a deep drill hole (1984-01) of 1737 feet was drilled on claim K- tract 66, down-dip from the Boston-Richardson mine and in 1985 a small drilling program of 1279 ft. was performed on the West Goldbrook mine.

In 1987, from January to March 5, 1987, a program funded and managed by Petromet and Greenstrike was executed. Five holes were drilled, using two machines, for a total of 6,314 ft.

Since May 1987, Onitap has completed an additional 23 holes, (holes 87-06 to 87-28 inclusive), for a total of 28,480 ft.

In 1987 the property was surveyed with various geophysical instruments on the old Patino grid lines. Helicopter borne magnetic and EM 16 surveys were also performed by Aerodat Limited.

GENERAL GEOLOGY:

The property is underlain by rocks of the Cambro-Ordovician Meguma Group (Fig. 3) subdivided into the Goldenville Formation overlain by the Halifax Formation.

The Goldenville Formation is mainly made of sandstones interbedded with thin slate horizons, which are inferred to have been deposited by turbidity currents and reworked by bottom currents (Schenk, 1970; Harris, 1971; Waldron, 1983). The Goldenville Formation is at least 2 km thick in the Isaac's Harbour area, however it reaches at least 8 km thick elsewhere in the Meguma Terrane.

The Halifax Formation is composed predominantly of slates with subordinate sandstones and is poorly exposed in the Isaacs Harbour area outcropping at only three localities on either side of Isaacs Harbour and on Goose Island.

Deposition of the Meguma Group appears to have been accompanied by movements on generally highly inclined east-west faults, which produced monoclinial folds. These faulted monoclines also appear to have formed the locus of fissures which formed the conduits for hot springs producing auriferous veins.

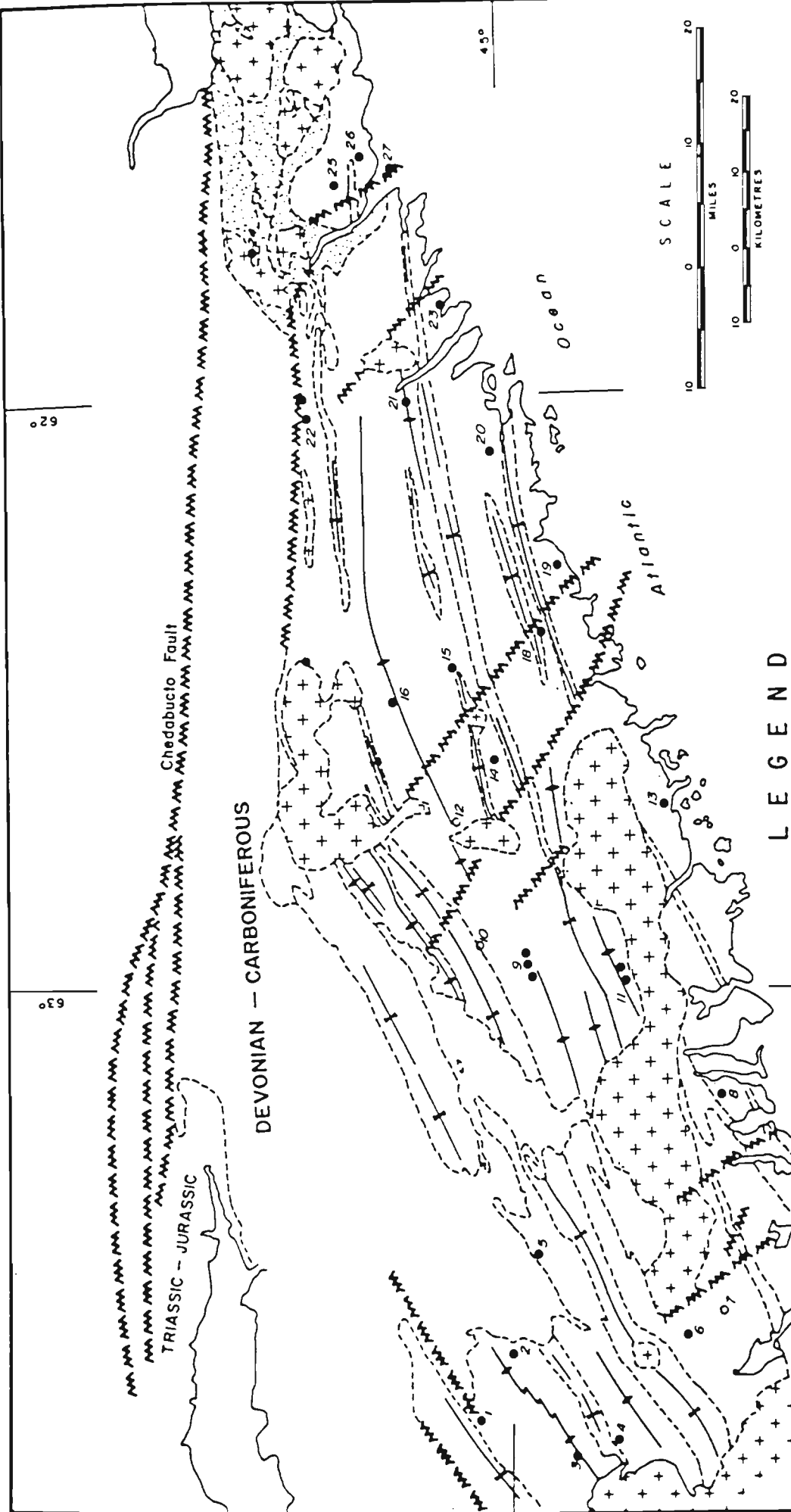
Deposition of the Meguma Group was followed by several phases of deformation accompanied by greenschist facies metamorphism. This was closely followed by amphibolite facies, low pressure regional metamorphism in the northern part of the area.

Further deformation followed correlated with the Hercynian Orogeny. Gold appears to have been remobilized along Hercynian shear zones.

Finally, during the early Mesozoic, the area was cut by a series of northwest-southeast sinistral transcurrent faults associated with kink bands. (Keppie, 1983).

ECONOMIC GEOLOGY:

Gold has been mined in the area sporadically since the late nineteenth century. There are four abandoned mines located on the property. They are in order from west to east, the Dolliver Mountain, the West Goldbrook, the Boston-Richardson and the East Goldbrook. Only the Boston-Richardson can be considered as a producer. It produced 50,000 ounces of gold from a total of 375,000 tons of ore mined over a period of nineteen years at an average grade of 0.13 oz. Au/t. These mines straddle the axis of the Upper Seal Harbour anticlinal structure (Fig. 4) which is oriented in an east-west



029

630

Chedabucto Fault

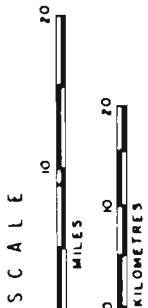
DEVONIAN - CARBONIFEROUS

TRIASSIC - JURASSIC

Ocean

Atlantic

Halifax



45°

LEGEND

- Younger Formations
- Devonian - Carboniferous Granite
- Cambro - Ordovician Halifax Formation
- Goldenville Formation (Metamorphics, schist)
- Major Gold Deposits (See separate list)

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GEOLOGICAL SKETCH MAP OF NOVA SCOTIA WITH MAJOR MEGUMA GOLD DEPOSITS

Fig. 3



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MAJOR GOLD DEPOSITS (Fig. 3)GEOLOGICAL SKETCH MAP OF NOVA SCOTIA WITH MAJOR MEGUMA GOLD
DEPOSITSLIST OF DEPOSITS

<u>Deposit No. of Map</u>	<u>Name</u>
1	East Rawdon
2	Renfrew
3	Mount Uniacke
4	South Uniacke
5	Oldham
6	Waverley
7	Montague
8	Lake Catcha
9	Moose River
10	Caribou
11	Lake Charlotte
12	Beaver Dam
13	Tangier
14	Killag
15	Lachaber
16	15-Mile Stream
17	Mooseland
18	Salmon River
19	Moosehead
20	Miller Lake
21	Goldenville
22	Cochrane Hill
23	Wine Harbour
24	Forest Hill
25	Upper Seal Harbour
26	Seal Harbour
27	Isaacs Harbour

Only those with past production greater than 10,000 ounces or with significant reserves and current exploration are shown (from Graves, M.C., Zentilli, M., A Review of Gold in Nova Scotia; in Geology of Canadian Gold Deposits, C.I.M. Spec. Vol. 24, eds. R.W. Hodder, W. Petruk, P. 233-242).

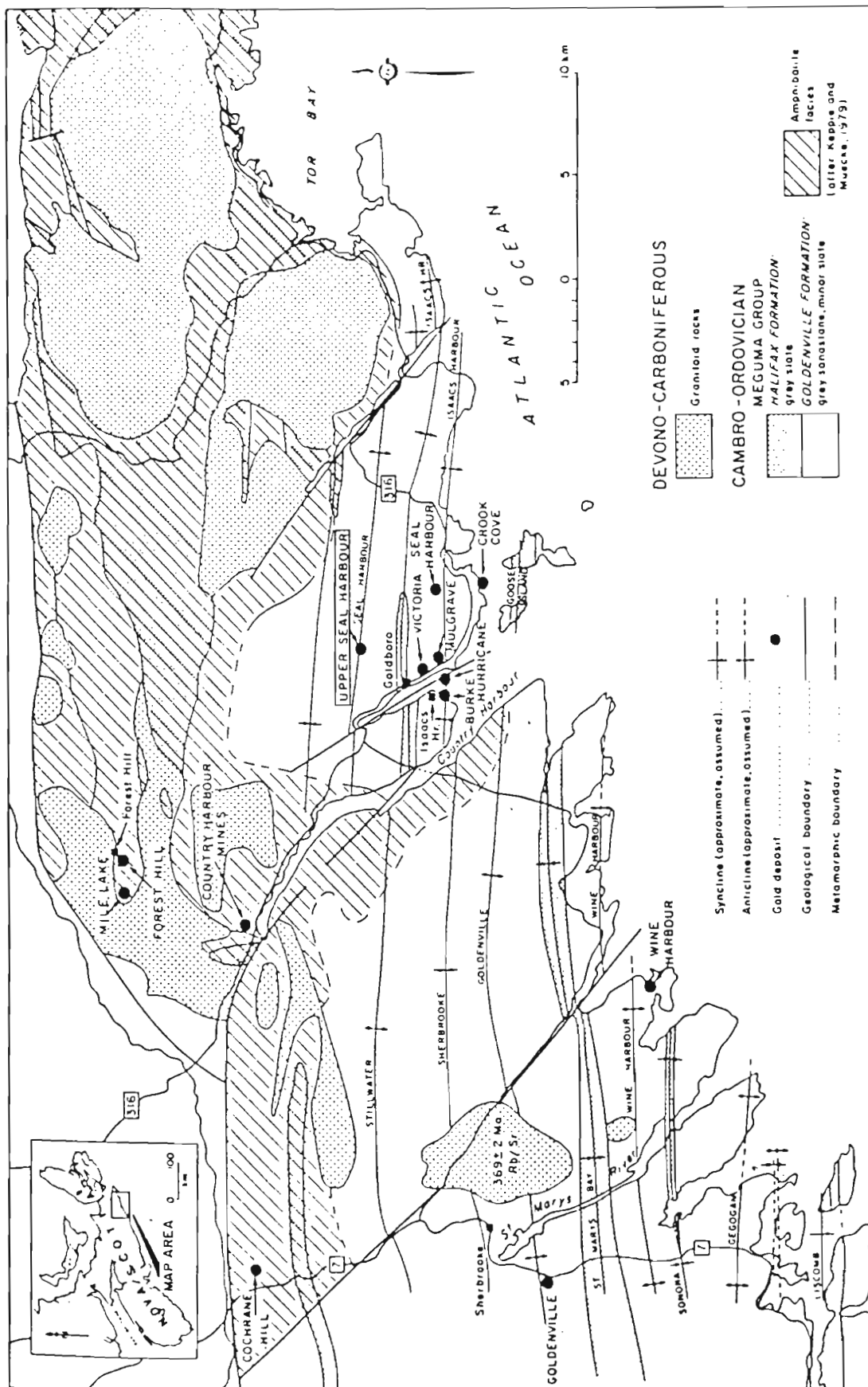


Fig. 4
 Geology of the Area Around Upper Seal Harbour
 (after Haynes, 1983)

direction and plunges gently to the east.

The gold is associated with stratiform, stratabound and side quartz veins and as rare dissemination in the host rock slates interbedded in the sandstones of the Goldenville Formation. The gold districts are preferentially located near the hinge zone of asymmetric Acadian folds. Although true "saddle reefs" are present, as it is the case along the Upper Seal Harbour anticline, many vein systems are located on the limbs of folds adjacent to monoclinial flexures. The mineralogy and form of the veins, and their attendant wall rock alteration effects, suggest that gold was deposited initially from hydrothermal solutions, that passed upward through the fault systems, as they were ejected into seawater as low density plumes from submarine hot springs (Haynes, 1983).

DIAMOND DRILLING PROGRAM:

The lithologies encountered in the drill holes consist mainly of (1) arenites (2) subarenites and (3) mudstones.

(1) Arenites : generally consist of siliceous sediments with a light green to grey colour, massive and well endurated with good sorting present. Also present are bedded arenites and some slightly chloritized arenites. Biotite content ranges from 5-10% throughout the section. Original bedding is difficult to see because a very strong foliation is present.

(2) Subarenites: generally consist of more thinly bedded sequences of argillaceous material which exhibits moderate sorting and have higher lithic component. These rocks are of a medium grey colour.

(3) Mudstones : are aphanatic and deep-black. These rocks are generally fissile and exhibit a well developed "slaty cleavage" . The slates, or shales, generally contain 50% or more biotite with common quartz-carbonate porphyroblasts. In some of the holes, some graphitic slates are also observed. Sulphide mineralization consists mainly of arsenopyrite and lesser pyrite and pyrrhotite are also found locally.

OBJECTIVES

The initial objective was to test by diamond drilling the down plunge extension of the Boston-Richardson Mine in the

vicinity of the deeper hole drilled in 1984.

Geophysical surveys were to be done in order to locate exploration targets with a similar signature to the known deposits.

RESULTS

After the completion of the program funded and managed by Petromet Resources Limited and Greenstrike Gold Corporation, a different interpretation of the drillhole results, combined with the information from the old underground workings, suggested the presence of a new mineralized belt containing visible gold and sulphide mineralization below the Boston Richardson Belt.

This was confirmed by the drilling performed by Onitap since May 1987, specially after taking the decision to drill through the old workings. The New Belt was intersected in most of the holes and traced practically near surface where it lies below an area covered by a small lake and swamps (this explains why it was not discovered at the beginning of the century).

DISCUSSION

New drilling results from the Onitap project to test the extensions of two former producers in Nova Scotia have confirmed the existence of at least three additional mineralized horizons beneath the old mine workings, with impressive gold values and widths in each zone. In the current program, 23 holes have been completed, intersecting the anticlinal fold structures down the easterly plunge from the surface exposure at the Boston Richardson Mine, and beneath the East Goldbrook Mine. The production of 50,000 ounces from the Boston Richardson, prior to 1911, was recovered from a stratabound "belt of quartz and slate lying between well-defined walls of quartzite" (Memoir 385) and mining extended from workings near the apex, or crest of the fold, to both legs of the fold several hundred feet away from the apex (Fig. 5).

The gold bearing structures are described as stratabound belts of the saddle reef type, usually in units of quartz-carbonates, shales, slates and mudstones of Cambro Ordovician age.

Exploration work by Onitap in 1984-1985 and drilling by

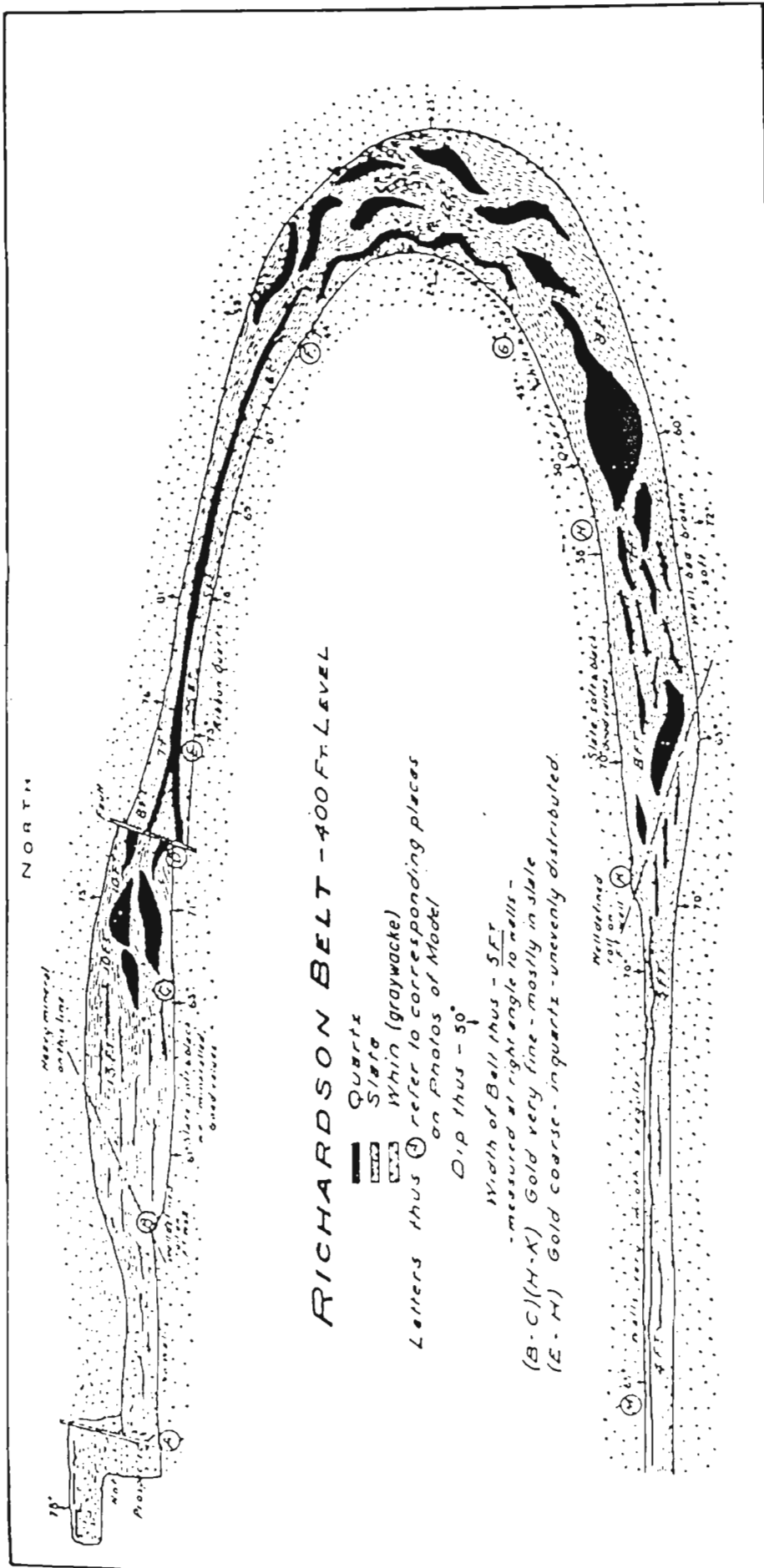


Fig. 5

The Richardson "Belt" on the 400 ft. Level (after Brown, 1909) (no scale)

Greenstrike Gold Corp. and Petromet Resources Ltd. under an option agreement early in 1987 suggested the presence at depth of additional mineralized zones or "belts" below the Boston Richardson Mine. With new flow-through funding Onitap undertook a program of 35,000 feet of diamond drilling to confirm and delineate these horizons with the objective of outlining a minimum potential of 300,000 ounces.

The 1987 program resulted in the discovery of gold mineralization in a zone named the "New Belt", lying approximately 250 feet below the apex of the fold, the site of previous operations. The "Third Belt" was intersected at an additional depth of 150 feet, and several deeper holes have indicated the presence of an additional zone, or "Fourth Belt". Above the Boston Richardson workings, in an upper part of the folded sequence, the East Goldbrook belt has also been intersected, with important gold values.

Tabulation of the most significant drill holes with assay results in the various Belts follows:

Hole No	Section (m)	From Ft.	To Ft.	Interval Ft.	Gold oz./t	# Belt
87-21	585E-25N	181.0	192.0	11.0	0.11	New
87-21		248.0	252.0	4.0	0.11	
87-21		625.0	636.0	11.0	0.22	Fourth
87-19	600E-25N	264.0	275.0	11.0	0.22	New
87-19		297.0	317.0	20.0	0.23	New
87-23	750E-55N	368.5	388.0	19.5	0.23	New
87-23		579.0	603.0	24.0	0.19	Third
87-27	750E-125N	520.0	525.0	5.0	0.10	New
87-27		673.0	680.0	7.0	0.44	(cut) Third
	including	677.0	680.0	3.0	3.64	
87-27		718.8	743.0	24.2	0.21	Third
87-25A	750E-50N	452.0	463.0	11.0	0.12	New
87-25A		899.0	903.0	4.0	0.14	Fourth
87-24	900E-45N	613.0	619.0	6.0	0.16	New
87-24		912.0	914.9	2.9	0.49	Fourth

87-24		942.0	954.0	12.0	0.14	Fourth
87-26	900E-45N	590.0	591.0	1.0	0.22	New
87-26		807.0	818.0	11.0	0.19	Fourth
87-28	975E-45N	819.0	833.0	14.0	0.27	New
87-28		867.0	882.0	15.0	0.19	New
87-28		906.5	912.0	5.5	0.13	Third
87-06	1200E	363.5	365.3	1.8	0.46	EG
87-06		454.3	456.7	2.4	0.18	EG
87-06		952.0	954.9	2.9	0.32	New
87-07	1200E	171.3	181.2	9.9	0.29	EG
87-07		191.8	196.8	5.0	0.24	EG
87-07		214.0	216.6	2.6	0.11	EG
87-07		231.4	234.0	2.6	0.53	EG
87-07		445.0	449.0	4.0	0.23	
87-07		469.5	473.8	4.3	1.55	(unc.)0.42 (c)
87-07		490.0	492.0	2.0	0.51	
87-07		1133.0	1142.0	9.0	0.29	New
87-07		1259.0	1261.0	2.0	0.15	Third

Holes 87-29 (675E-100N) and 87-30 (750E-25S) are in progress, and the remainder of the drilling program will be completed by the end of February, 1988.

Most of the drill cores contain visible gold within the belts. The assay results have been most encouraging and provide confidence that the combined belts have a potential for a 300,000 ounce gold deposit.

Drilling is done on a grid spacing of 75m (246ft.) over a length of 3,000 feet along the anticlinal axis. With the widely spaced drilling to date, only preliminary estimates can be made from significant intersections in each belt. These estimates indicate a range in average grades from 0.10 oz. gold per ton in the unmined portion of the Boston Richardson belt, to 0.18 oz. gold in the deepest, or Fourth belt. Higher grades are evident in the upper part of the deposits, where results obtained in the New and Third Belts suggest a potential for a deposit of at least 1.5 million tons at a grade of 0.22 oz. gold per ton.

POTENTIAL OF THE NEWLY DISCOVERED BELTS:

The New, Third and Fourth belts are of the same type as those described in Memoir 385: "the veins all follow the planes of stratification and some of them attain a great thickness at the apex, in some cases over 20 feet, thinning down on the legs."

The New and Third belts have been intersected over a strike length of 2400 ft. and the thickness of these belts is greater than the Dolliver Mountain and Boston-Richardson belts. To date the Fourth belt is known over approximately a strike length of 1,000 ft.

Giving these belts an average thickness of 14 ft. with a draping of 225 ft. on each flank, the following figures for the New and Third Belts can be derived:

$2 \times 2400 \times 14 \times 450 : 12 = 2,520,000$ tons.

For the Fourth belt over a length of 1,000 ft it is:

$1000 \times 14 \times 450 : 12 = 525,000$ tons.

Cumulative tonnage : 3,045,000 tons.

Quoting from Memoir 385 in reference to the Boston-Richardson belt: "although the greater part of this belt has been milled and furnished a large body of low-grade ore, careful sampling and assaying on the 400-foot level showed that the gold is not evenly distributed but is concentrated in zones.."

Because of the irregular distribution one could consider that only half of the tonnage will grade 0.22 oz. Au/t. As only part of the gold is "free gold" and the remainder is associated with sulphides, mostly arsenopyrite, a metallurgical recovery of 90% is estimated.

The potential gold content in the cumulative tonnage can therefore be calculated as:

$50\% \text{ of } 3,045,000 \times 0.22 \times 90\% = 301,455$ ounces of gold.

RECOMMENDATIONS:

Two options exist to obtain a reserve figure in the proven or drill indicated categories.

Option #1 is the minimum necessary program needed to obtain these reserves.

It considers a surface drilling program done on sections located at 25 meter intervals. On each of these sections 3 holes would be drilled, one on the apex, the other two located on each of the flanks.

Drilling would be done on the following sections : 575E, 625E, 650E, 700E, 725E, 775E, 800E, 850E, 875E, 925E, 950E, 1150E, 1175E for a total footage of 36,000 ft.

Budget:

36,000 ft. @ \$33/ft. all inclusive:	\$ 1,188,000
Metallurgical testing	100,000
Reserve calculations	100,000
Contingencies	162,000

	\$1,550,000

Option #2 would consist of an underground program that would include a ramp from surface, drifting on several levels, with detailed drilling and bulk sampling. Another eventuality would be to rehabilitate and deepen the old vertical shaft (3 compartment 19 ft. by 6 ft.)

The budget for such a program is estimated to be between \$5 and \$6 million.

CONCLUSIONS


Exploration work by Onitap on its Goldboro property has resulted in the discovery of gold mineralization in several belts namely the New, Third and Fourth belts. In addition, above the Boston Richardson belt, in an upper part of the folded sequence, the East Goldbrook belt has also been intersected, with important gold values.

The potential of this new discovery is in excess of 300,000 ounces of gold and at Can\$625.00 an ounce it represents a value of \$187,500,000.

To arrive at "drill indicated and proven" reserves two work options are open:

The first option would consist of a detailed drilling program on sections at 25 m interval for an estimated budget of \$1,550,000.

The second option would be to realise immediately an underground exploration program complete with detailed drilling and bulk sampling up to the feasibility decision. The cost of such a program is estimated to be between \$5 and \$6 million.


Karl A. Naert, Ph.D., P.Eng.

RJD/KAN/



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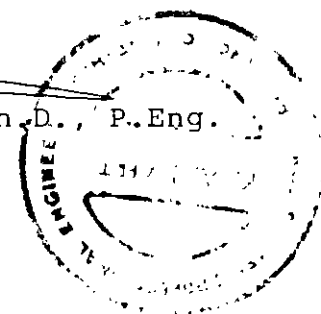
CERTIFICATE OF QUALIFICATION

I, Karl A. Naert, hereby certify:

- 1) that I am a consulting geologist employed by Narex Ore Search Consultants Inc., 48-151 Nashdene Road, Scarborough, Ontario;
- 2) that I am a graduate of the University of Leuven (Belgium) with a Licence in Geology and Mineralogy (B. Sc. Honours equivalent) 1963, and of The Pennsylvania State University with an M. Sc. and Ph. D. in 1973;
- 3) that I have been practising my profession as a geologist since 1963;
- 4) that I am a registered Professional Engineer in the Province of Ontario, a Fellow of the Geological Association of Canada, a member of the Geological Society of America, a member of the American Institute of Mining and Metallurgical Engineers and a member of the Canadian Institute of Mining and Metallurgy;
- 5) that I am an officer and a minor shareholder of Onitap Resources Inc.


Karl A. Naert, Ph.D., P.Eng.

Scarborough, Ontario
December 21, 1987





MINES REPORT

1899. *Richardson Mine.* The main or east shaft was 400 ft. deep, and dipped at an angle of about 35°. The lead was from 6 to 20 ft. thick, and was composed of 60% quartz, and the remainder slate, all of it was put through the mill. The milling process was improved by introducing two Wilfley concentrators one of which was in use since August 1898. On it they passed the pulps from 20 stamps and have saved upwards of 150 tons of concentrates worth about 45 dollars per ton. A tunnel was driven of 100 feet under a bridge of solid rock, between the north and east shafts, cutting through the fault that passed through the mine.

1900. *Richardson Mine.* There were two shafts in operation working a block of 100 acres. The east or main shaft is at the apex of the anticlinal, dipping at an angle of 35° and was 530 ft. deep, with workings extended north 750 ft. and south 270 ft. The belt was 15 ft. thick, and until a short time previously everything was put through the mill. "The management, profiting by past experience are now leaving good substantial shaft pillars, alternating on each side. Two of the pillars I examined were 40 ft. x 60 ft. and 50 ft. x 70 ft. There was some time ago a heavy cave-in of rise workings and it must have been at considerable cost; that the shafts now in operation, were saved." The North Shaft was situated on the same belt and on the north arm of the fold; this shaft was 280 ft. deep and at an angle of 70° and connected with the main shaft by a cut through reported in 1899. On account of the change in quality of material mined and sent to the mill it became possible to crush about 2,000 tons per month yielding 45 tons or about 2½% of concentrates, worth \$17 per ton after paying all expenses.

1901. *The Richardson Mine.* The main shaft reached a depth of 620 ft. measured on the incline, which was on an angle of 22° to 25° for 100 ft. and from there at about 35° to the bottom. A drift on the 500 ft. level was run on the south leg for about 700 feet, and thickly covered with timber to within 160 ft. of the head, from which point a solid rock cover is left between it and the old crushed upper workings. The pillar measured about 70 ft. in height. At 530 ft. from the main shaft in this level a mill hole was down to the face of the underhand stopes, being carried from the shaft bottom up to the level, and in this working two pillars, some 40 ft. long by 30 ft. high, had been left. The north shaft reached a depth on the incline of 240 feet, but on account of the steepness of its dip, which decreased from 80° to 65°, (*) bottom was only some 50 ft. above the level of the main east shaft, and about

(*) See footnote, Dept. Mines, Rep. N. S., 1902, p. 47.

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350 ft. from it, measured round the bend, which here appeared to be more gradual than the fold formed by the south leg. The level driven from the bottom of the north shaft northwesterly reached a distance of 220 ft., and from its head a vertical bluff to the surface marked the limit of the work in this direction.

Dolliver Mountain Mine. This company's work was chiefly confined to prospecting and development on the surface at a point some $1\frac{1}{2}$ miles from the Richardson Coy's workings. A vertical prospecting shaft 12 ft. x 6 ft. was sunk here to a depth of 60 ft. Two veins, measuring 5 ft. to 8 ft. in thickness, were proved on the surface, one 500 ft. west and another about the same distance east of the shaft just mentioned.

1902.

Richardson Mine. During the past year 29,000 tons of ore were extracted and crushed at this mine, and the underground workings were extended as follows: The main east incline has now reached a distance of 760 ft. At 707 ft. a level was driven on the belt 90 ft. each way, and underhand stoping has been carried up from the faces to a level driven at a depth of about 670 ft.; this level was in 220 ft. on the south leg, and 323 ft. northwesterly. Above the end of this level on the south side a pillar was left, 30 ft. long by 30 ft. high, and at the shaft under the level there was a small rock support. On the north side two pillars were left 30 ft. x 30 ft. to support the walls and between these at close intervals heavy stulls were hitched. At the face of this level a block of ground was left in position about 40 ft. to 50 ft. in height, and about 140 ft. on the level. West of this block and on the same level the ore was all taken out to the north shaft, a distance of 110 ft., and on the west side of the shaft the level was continued for 120 feet. This north shaft only measured from the deck 285 feet to the level just mentioned; but the difference in measurement and the distance from deck to the corresponding level in the main shaft was accounted for by the difference in dip, which in the last 150 ft. of the main shaft only averaged 19°, whereas the north shaft the bottom dipped at 74°, 30'. The ore was extracted from above the bottom level for a distance of 85 feet west of the shaft, and the ground above the 250 ft. level was worked out for some 200 ft. or more in the same direction, westerly. A vertical shaft was sunk to the eastward, and tapped an overlying vein on the south dip at a depth of between 150 and 200 ft., from which point a cross-cut was driven to the north dip. The information about these workings was given by Mr. Cox, the then manager.

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Dolliver Mountain Mine. The shaft, which was vertical, measured 17 ft. 6 ins. x 4 ft. 6 ins. inside timbers. At depth of 55 ft., 92 ft. and 102 ft. small veins were cut which though not apparently of workable size, showed the dip of the measures which lie at 19° to the south and from 24 to 45° to the north. At 130 ft. a belt of ore was intersected which measured 32 ft. in the shaft, which, judging by samples, resembled the Richardson belt in composition. The total depth of the shaft was 190 ft. The pitch of these veins to the eastward varied from 10° to 16°.

1903.

The *Boston Richardson Mining Company* took over the property of the Richardson Mining Company. In March the workings were completely lost by an extensive crush which demolished the main shaft. This was caused by the tremendous swinging weight of the practically unsupported roof closing in on the footwall. The Inspector of Mines reports: "There can be no doubt that the cave-in and subsequent loss of money and employment to a large number of families was directly due to negligence for a period covering a number of years."

Dolliver Mountain Mine. The vertical shaft measuring 17 ft. 6 ins. x about 5 ft. inside timbers, reached a depth of 265 ft. A station was cut on the "Partington" belt and rails laid at 159 ft. from the deck; levels from this station were carried back on the legs of the belt, 200 ft. on the south leg, and 150 ft. on the north. An air shaft has been sunk 60 ft. on the south leg and is situated 450 feet west of the main shaft. The belt contained between 5 and 6 ft. of milling stuff at the faces; the main shaft was sunk through the 22 ft. belt and tapped the "Forge" belt.

1904.

Dolliver Mountain Mining Coy. was the first company to take advantage of the Act by which the Government paid part of the cost of sinking a deep shaft. The shaft on May, 1904, was 330 ft. deep and about 21 ft. x 10 ft. in rock. On June 26th, 60 ft. had been gained. All other mining work was stopped while the sinking was in progress. Since the previous year the underground development has proceeded steadily and the levels, etc., were extended as follows: the shaft was 488 ft. deep. On the Partington belt the No. 1 South level has been extended from 164 ft. from the shaft station to a total distance of 645 ft. At a distance of 583 ft.

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from the station an upraise was made on the belt, and connected with the air shaft sunk from the surface on the belt. The dip of this shaft at 6 ft. from the surface was 53'. 30' and it measured from the deck level 158 ft. The north leg was extended from 150 to 204 feet from the station. The ore was stoped up from the levels on each side for distances of about 350 ft. from the station on the south level and 175 ft. on the north level. The belt matter over the crown or saddle of the fold was, however to a great extent left in place. At 110 ft. in the north level a raise was put up, and connected over the apex with a raise from the south level driven at a distance of 151 ft. from the station. At 308 ft. in the shaft a similar station to No. 1 was cut on the "Forge" belt, and this belt was drilled on for 180 feet south and 194 feet north. Very little stoping was done on these levels. Near the face of the south levels a fault was encountered throwing the belt 18 ft. to the south. A crosscut was driven from the station 80 feet north, and 125 feet south, and connected with the Partington Belt. On the south side of the belt there was a drift 62 ft. west, and 74 ft. east, and from the crosscut and on the north leg the drifts reached 50 ft. west and 80 ft. east.

Boston Richardson Mine. Attention was solely directed to the enlarging and sinking of the vertical shaft commenced and sunk to a depth of 180 feet by the former company. The new shaft measured 19 ft. x 6 ft. inside timbers, and was divided into three compartments. The bed rock was not encountered until 30 feet below the surface. At 96 ft. a drift was put in 45 feet east of the shaft and disclosed a large belt dipping south. A crosscut was driven north from this drift and a small drift was put in east on a belt dipping nearly vertically, but with a slight northerly inclination. Between this depth (96 ft.) and 386 feet from the surface the shaft intersected 8 veins, ranging from 4 to 7 1/4 inches thick. At 386 feet a gouge seam occurred apparently dipping northeast, and below this considerable quartz was mixed through the rock. This ore is doubtless an extension of the Richardson belt, for a crosscut was made to both legs on which levels were driven and connection made with the old workings which were pumped out.

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1905.

Boston Richardson Mine. The vertical shaft was continued through the Richardson ore-body, and a station made at 400 feet; crosscuts were driven on each leg. A large pillar was left behind the shaft; and, during the winter, connection was made from the stopes above the south level to the old workings. The south leg dipped 65°, and the level was 320 feet from the shaft; while the north side varied from 69° to 75°. A large amount of ore was stoped out over the crown, and stoping was carried back to the faces of the levels. Contrary to the practice in the old workings, the ore was worked entirely by the overhand method. A thorough system of sampling and mill testing was instituted, and proved of immense benefit in bringing to light the fact here, as was probably the case elsewhere in the province, a very large percentage of rock (so-called ore) was mined and milled, which should have been left in the mine. To aid the work a very useful and ingenious model of the mine was prepared; it was of plaster, and accurately depicted the workings to scale.

DeWier Mountain Mine. Sinking was continued under the Deep Mining Act until October. A depth of 488 feet was gained, and several ore-bodies were cut in the sinking. In November a contract was made with the Sullivan Machinery Company to drill from the bottom of the shaft in prolongation of the axis (about 4° 30' south of vertical). This was put down for 500 feet, and though several bodies of quartz and slate were encountered, the results were unsatisfactory. Shortly after this the mine was allowed to fill with water and has since remained idle.

1906.

Boston Richardson Mine.—On the 400 ft. level, south leg, the face was 1,220 feet, 900 feet having been driven during the year; the dip of the lead at this face was 70°. On the north leg 650 feet were driven, the face being 1,010 feet, and the dip here was 75°. Stoping was carried on in both legs; in the south leg the bottom of the stope was 700 feet from the shaft, and in the north 800 feet. Of the ore mined only the over run or about half was taken out. Ninety feet from the shaft on the south leg in the 400 ft. level a crosscut was driven west about 500 feet, cutting five belts, varying in width from 1 to 26 feet, from only two of which mill tests were taken. For a distance of 700 feet from the shaft on the north leg the ore-body continued in size the same as in the old workings above; from here on it rapidly widened, until at 900 feet from the shaft it attained a width from 14 to 15 feet, and from there to the face it appeared to maintain its size and was heavily mineralized. In the south leg the ore-body showed similar characteristics to the old workings above.

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1907.

Boston Richardson Mine. A production of 6,504 oz. of gold was obtained from 43,458 tons of quartz crushed. On the 400 ft. level no drifting was done, work being wholly confined to the stopes and very little unbroken ore was left in place above this level. The stoping at the west end of the old workings on the north side was carried to within 100 feet of the surface; no difficulty was encountered in doing this work by the overhand method. Work was commenced on the sinking of an incline shaft on the apex of the fold of the belt at the 400 ft. station. This shaft measured 23 x 10 ft. and reached 475 feet on the incline (incline measurement, slope 25°). Sinking was temporarily discontinued while levels were driven in north and south from what was called the 550 ft. station (360 ft. from the 400 ft. station, measured on the incline, and 150 ft. vertical). These levels on September 16th were in 265 feet north and 235 feet south. The ore encountered was practically identical with that mined in the corresponding workings above.

1908.

Boston Richardson Mine. During the year ended Sept. 30th, 38,000 tons of ore were crushed, yielding 4,092 oz. of gold. Work was resumed on the incline shaft, which was 700 ft. deep, measured on the slope from the 400 ft. station; the 550 ft. level, south, was driven 495 feet, making a total of 730 feet, and north 820 feet, making 1,085 feet; the 700 ft. level was started south and driven 181 feet, the north level from the 700 ft. station had not yet been started. Stoping was done on the 550 ft. level, in both legs, principally on the south side; on the north side the stopes have just entered what was termed the main shoot on this leg. On the north side 170 ft. from the station a raise was driven on the vein to the incline shaft and 1,200 feet from the station a raise was driven to the 400 ft. level; on the south side 275 feet from the station, a raise was driven to connect with the incline. The level south from the 700 ft. station was 181 feet, and was being continued.

Arsenic. During the year 1907, 323 tons of arsenical concentrates were shipped to Belgium, containing an average product of 40% metallic arsenic, and during the year 1908, 595 tons were shipped. Nearly all of this concentrate has been taken from the old accumulation. The prices received were dependent upon the market price of pure white arsenic, and were during the year 1908 in the vicinity of 55 cents a unit. These concentrates also carried from \$5.00 to \$9.00 in gold values, which were not at that time paid for by the buyers.

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1909.

The New England Mining Coy. (Formerly the Boston Richardson Mining Company). During the year ended September 30th, 41,425 tons of ore crushed yielded 5,024 oz. of gold valued at \$95,456.00—this recovery being 86.6% by stamp amalgamation, and 17.4% by bromo-cyanide extraction, from 1,171.5 tons of concentrate, and being at total yield of \$2.30 from each ton of ore crushed. Compared with the previous year, the production showed an increase of 3,425 tons crushed; 938 ounces of gold recovered, and 24 cts. a ton yield. Operations were almost wholly confined to the 550 ft. level, north and south; on the south side practically all the ore was broken. The 700 ft. level south was advanced 629 feet, making a total from shaft to face of 806 feet. A raise from this level to the 550 ft. level was driven 50 feet east of the face on the 700 ft. level; no stoping was done. The level on the north side was driven a distance of 20 feet from the station, but it was not continued.

West Block. An old shaft at the western end of the company's property was cleaned out. The shaft was 85 feet deep; and at a depth of 73 feet, a drift was driven east 56 feet; also 6 ft. east of the shaft a crosscut was driven north 72 feet 6 inches, cutting two belts; the first at a distance of 66 feet; the second at a distance of 72 feet, making a total of three belts exploited from this shaft. On the first belt met in the crosscut, a drift was put in east 66 feet. Number 1 or the shaft belt, was 6 ft. between walls, and was composed of quartz and slate containing probably an average of 18 inches of quartz. No. 2 belt, the first in the crosscut, north, was about 5 ft. between walls, and is composed of quartz and slate. No. 3 belt was about 18 inches, made up of quartz and slate. These belts were parallel, their course being roughly north 20° W., and they dipped west at an angle of 60°.

1910.

New England Mining Company. From 36,940 tons of ore crushed, 4,063 ounces of gold were recovered, valued at \$77,297—being an average recovery of \$2.09 from each ton of ore mined and crushed. Compared with the previous year, the production shows a decrease of 4,485 tons crushed, 961 ounces of gold recovered and \$0.21 in the yield per ton. Of the above production, 715 oz. of gold were recovered from 956 tons of concentrates made and treated by bromo-cyanide process. 529 tons of arsenical concentrates were made and shipped to Swansea, Wales. During the year operations at the Richardson Mine property were confined to the stoping and drawing of the developed and broken ore, from the bodies on the 550 ft. and 700 ft. levels. No development or prospect-

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ing work was carried on other than the driving of a crosscut south from the vertical shaft at a depth of 170 feet, which crosscut had been driven at the end of the year a distance of 88 feet, and had encountered two belts, one immediately adjoining the shaft, and a second at a distance of 86 feet from the shaft. These belts closely resembled the Richardson belt in general characteristics, and, so far as opened, measured: No. 1 belt, 6 feet; and No. 2 belt 7 feet in width. A serious, though not unexpected, "cave" took place in the upper portion of the old working on the north side of the fold, the caving ground extended from what was known as the old incline around the north leg of the fold for a distance of about 300 feet, and being very similar in extent and character to the "cave" which took place several years ago. The cause of this "cave" as well as that on the south side was insufficient pillars. Its effect upon the late workings of the mine was the opening up an underground water course, letting in roughly 300 additional gallons of water a minute, the workings formerly making in the vicinity of 100 gallons of water a minute. The ore has been low grade. The greatest yield a ton (1893) \$7.22, and the smallest (1905) \$1.55, the average being \$2.51.

West Block. On account of unsatisfactory values in the ore, work was here abandoned. The extent of the work was as follows: From the shaft (85 ft. deep) at a depth of 75 ft. levels were driven east 56 ft. and west 85 ft., on what is known as the shaft belt; from the drift east, 6 ft. away from the shaft, a crosscut has been driven north 178 ft., cutting No. 1 belt at a distance in of 35 ft.; No. 2 belt 85 ft.; No. 3 belt 112 ft. and No. 4 belt at 160 ft. Mill tests of from 10 to 60 tons from these workings gave from shaft belt, \$1.11 to \$2.90 a ton; from No. 1 belt, north, \$0.17 to \$3.40 a ton, and from No. 4 belt \$1.00 to \$1.25 per ton; and in addition to this a large test of 96 tons taken from the roof of the level on No. 1 belt gave 9.39 oz. of gold or \$1.79 a ton.

East Block. A vertical shaft was sunk 202 feet east of the old East Block shaft to cut what was designated No. 3 belt in the former workings; this belt was cut at a depth of 100 ft., and from this depth the shaft was continued 40 ft. on the belt. Stopping was carried on at the end of the year, but no clean up was made. In the former work on this belt carried on from the old East Block workings, some very good ore was recovered.

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1911.

New England Mining Coy. The only mining engaged in during the year by this company was a small amount of stoping at the East Block property, 70 tons of ore being taken from what is known as No. 3 belt. Subsequently to the closing of the mine a final clean-up was made of the millplates and cyanide plant, resulting in the recovery of 1,502 oz. of gold, which makes the total recovery of gold from the Richardson mine to date, 53,835 ounces from 395,731 tons of ore mined and milled. The bullion was valued (at \$19.00 an ounce) \$1,022,965, being an average yield of \$2.58 a ton.

1912.

New England Mining Coy. (Richardson). Surface prospecting was carried on. 75 tons of material recovered from several veins prospected were crushed, yielding 14 oz. or 7 dwts. of gold.



APPENDIX II

ASSAY RESULTS

Holes BR 87-06 to 87-28, inclusive

Description of Assay Methods





ASSAYERS (ONTARIO) LIMITED

33 CHAUNCEY AVENUE TORONTO, ONTARIO M8Z 2Z2 TELEPHONE (416) 239-3527

METHOD OF FIRE ASSAY

15 grams of pulverized sample are mixed with appropriate fluxes (PbO , Na_2CO_3 , $\text{Na}_2\text{B}_4\text{O}_7$, Flour) with Ag added and fused in ceramic pots at 1000°C for at least 1 hour or until melt is ready.

The Pb button (which contains the precious metals) is cupelled in bone ash cupels. The Ag bead obtained is parted in dilute HNO_3 . The Au is dissolved in Aqua Regia (mixture of HNO_3 and HCL). This solution is made up to volume and then compared against appropriate Au standards with an Atomic Absorption instrument at wave length 2428 \AA . The results are then reported in oz/ton.

METHOD OF CALCULATION:

$$\begin{aligned} 1 \text{ oz/ton} &= 1 \text{ mg of Au in } 29.166 \text{ g of sample} \\ &= 1000/29.166 = 34.29 \mu/\text{g} = 34.29 \text{ ppm} \end{aligned}$$

$$1 \text{ ppm} = 1000 \text{ ppb}$$



ASSAYERS (ONTARIO) LIMITED

33 CHAUNCEY AVENUE TORONTO, ONTARIO M8Z 2Z2 TELEPHONE (416) .

METHOD FOR FREE GOLD DETERMINATION

Sample as received is weighed, crushed, pulverized and screened over 50 mesh screen. If +50 mesh fraction is more than 15 g, it is pulverized by hand and weighed. This entire portion is then used in the Fire Assay.

The -50 mesh portion is mixed and 2X15 g portions Fire Assay.

These three assays are then proportioned to the sample as received.

The table below lists the assay results of Hole #BR 87-06:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t *Free Gold Method
01	27.0	28.25	1.25	1038	0.037
02	36.5	38.5	2.0	101	
03	66.8	68.0	1.2	5	
04	99.0	100.5	1.5	144	
05	100.5	102.0	1.5	5	
06	102.0	103.75	1.75	604	
07	103.75	105.5	1.75	270	
08	140.0	142.0	2.0	324	
09	142.0	143.8	1.8	189	
10	143.8	144.8	1.0	75	
11	144.8	145.8	1.0	33	
12	150.5	153.0	2.5	80	
13	153.0	153.7	0.7	40	
14	153.7	156.2	2.5	286	
15	156.2	158.3	2.1	412	
16	158.3	160.0	1.7	568	
17	160.0	162.0	2.0	3515	0.094
18	162.0	163.75	1.75	796	0.029
19	171.0	172.4	1.4	725	
20	172.4	174.4	2.0	715	
21	186.25	187.5	1.25	331	
22	201.75	203.0	1.25	464	
23	203.0	205.0	2.0	3805	0.12
24	205.0	206.5	1.5	457	
25	211.2	212.8	1.6	253	
26	218.7	219.6	0.9	1433	0.044
27	219.6	221.0	1.4	459	
28	221.0	222.3	1.3	528	
29	222.3	223.0	0.7	1227	0.035
30	224.3	225.3	1.0	3247	0.13
183	235.5	238.0	2.5	218	

31	259.5	261.9	1.4	180		
32	290.8	291.5	0.7	4033		0.10
33	314.1	315.9	1.8	582		
34	316.8	317.2	0.4	485		
35	317.6	319.6	2.0	125		
36	319.6	321.4	1.8	1213		0.046
37	322.5	323.1	0.6	168		
38	347.8	349.4	1.4	606		
39	349.4	350.5	1.1	3630		0.11
141	362.0	363.5	1.5			0.006
40	363.5	365.3	1.8	6878	0.21	0.46*
142	365.3	367.5	2.2			0.010
143	367.5	369.0	1.5			0.001
41	389.3	389.9	0.6	5		
42	394.2	394.9	0.7	126		
43	395.8	397.2	1.4	106		
44	397.2	399.2	2.0	45		
45	399.2	401.2	2.0	556		
46	401.2	402.5	1.3	6050		0.20
47	402.5	403.8	1.3	177		
48	403.8	404.8	1.0	111		
49	404.8	406.2	1.4	1225		0.042
50	417.7	418.3	0.6	4789		0.075
51	421.5	422.0	0.5	5581		0.15
144	422.0	424.0	2.0			0.017
52	424.0	425.5	1.5	675		
145	431.3	433.7	2.4			0.002
53	433.7	435.0	1.3	1976		0.072
146	435.0	437.0	2.0			0.032
147	438.1	438.9	0.8			0.049
54	438.9	439.9	1.0	928		0.04
148	439.9	440.7	0.8			0.058

55	440.7	441.6	0.9	161		
56	441.6	443.4	1.8	5		
57	443.4	445.5	2.1	78		
58	445.5	447.1	1.6	52		
152	447.1	449.0	1.9			
149	450.3	452.3	2.0	342		
150	452.3	454.3	2.0	265		
59	454.3	455.5	1.2	6803	0.19	
60	455.5	456.7	1.2	1456	0.026	0.16*
151	456.7	458.0	1.3	171		
154	459.9	462.2	2.3	513		
61	462.2	462.8	0.6	10000		0.92 (1.04)
155	462.8	464.75	1.95	169		
62	470.1	471.1	1.0	609		
156	472.5	474.2	1.5	183		
63	474.2	475.5	1.3	1561	0.028	
157	475.5	477.5	2.0	147		
158	477.5	479.7	2.2	228		
64	479.7	480.5	0.8	3829	0.12	
159	480.5	482.5	2.0	188		
65	485.1	485.8	0.7	265		
66	487.8	488.0	0.2	106		
67	497.1	498.3	1.2	101		
68	507.0	507.7	0.7	82		
69	507.7	508.3	0.6	1232	0.037	
70	511.7	512.9	1.2	97		
71	534.5	535.3	0.8	163		
72	537.0	538.0	1.0	85		
73	538.9	540.7	1.8	1715	0.052	
73	538.9	540.7	1.8	1715	0.052	
181	540.7	542.7	2.0	70		
182	542.7	546.0	3.3	94		
74	556.7	558.0	0.3	146		

75	598.8	599.8	1.0	82	
76	599.8	601.4	1.4	94	
77	603.0	603.8	0.8	180	
78	608.9	609.4	0.5	82	
177	610.8	612.1	1.3	5	
178	612.1	614.2	2.1	5	
179	614.2	615.3	1.1	5	
79	615.3	616.7	1.4	106	
180	616.7	620.8	4.1	37	
80	630.5	631.2	0.7	49	
81	664.5	665.5	1.0	3045	0.071
82	686.5	687.4	0.9	94	
83	687.4	688.3	0.9	92	
84	697.0	697.2	0.2	324	
85	701.7	702.2	0.5		0.006
86	716.0	718.4	2.4		0.046
87	718.4	720.9	2.5		0.001
88	720.9	721.2	0.3		0.005
89	721.2	723.7	2.5		0.008
90	723.7	725.4	1.7		0.001
91	884.5	885.3	0.8		0.003
92	898.5	900.2	1.7		0.009
93	941.0	942.3	1.3		0.001
94	947.0	949.0	2.0		0.001
95	949.0	950.9	1.9		0.001
96	950.9	952.0	1.1		0.011
97	952.0	953.3	1.3		0.18
98	953.3	954.9	1.6		0.44
99	954.9	956.1	1.2		0.002
100	956.1	958.1	2.0		0.012
101	958.1	960.2	2.1		0.013
102	960.2	962.2	2.0		0.001
103	962.2	964.4	2.2		0.001
104	964.4	966.6	2.2		0.07
105	966.6	968.6	2.0		0.018
106	968.6	971.1	2.5		0.026

107	971.1	973.1	2.0		0.016
108	973.1	975.1	2.0		0.005
109	975.1	977.6	2.5		0.002
110	977.6	979.6	2.0		0.02
111	979.6	981.7	2.1		0.008
112	981.7	984.0	2.3		0.004
113	989.3	990.3	1.0		0.011
114	994.5	996.9	2.4		0.011
115	1042.0	1044.5	2.5		0.001
116	1044.5	1047.0	2.5		0.012
117	1053.8	1055.2	1.4		0.003
118	1057.0	1058.8	1.8		0.002
119	1058.8	1060.5	1.7		0.008
120	1063.3	1064.4	1.1		0.004
176	1064.4	1065.3	0.9	5	
121	1075.0	1075.8	0.8		0.012
122	1084.5	1085.5	1.0		0.002
123	1086.8	1087.5	0.7		0.001
124	1162.4	1164.3	1.9		0.002
125	1165.6	1166.3	0.7		0.001
126	1171.0	1171.3	0.3		0.006
127	1189.4	1190.6	1.2		0.018
128	1199.4	1200.9	1.5		0.006
129	1202.2	1202.8	0.6		0.001
174	1232.5	1235.5	3.0	5	
175	1235.5	1238.5	3.0	5	
130	1337.5	1339.1	1.6		0.001
131	1340.0	1341.0	1.0		0.001
132	1341.8	1342.2	0.4		0.001

133	1342.2	1344.8	2.6		0.002
134	1347.0	1348.5	1.5		0.022
135	1348.5	1350.0	1.5		0.001
136	1355.3	1356.5	1.2		0.001
137	1447.8	1449.8	2.0		0.001
138	1449.8	1451.8	2.0		0.001
139	1456.0	1458.2	2.2		0.001
140	1458.2	1460.5	2.3		0.028
160	1552.0	1553.3	1.3	27	
161	1739.2	1740.3	1.1	5	
162	1741.5	1744.0	2.5	11	
163	1778.8	1781.0	2.2	11	
164	1781.0	1783.2	2.2	76	
165	1870.5	1872.8	2.3	62	
166	1872.8	1875.0	2.2	188	
167	1875.0	1877.2	2.2	37	
173	2002.0	2003.0	1.0	5	
168	2170.0	2171.2	1.2	15	
169	2173.3	2174.3	1.0	13	
170	2175.7	2177.0	1.3	5	
171	2177.0	2178.0	1.0	5	

The table below lists the assay results of Hole #BR 87-07:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
201	12.0	12.7	0.7	1608	0.056
202	12.7	14.9	2.2	329	
203	14.9	17.0	2.1	1236	0.047
204	17.0	18.7	1.7	525	
205	19.9	22.5	2.6	321	
206	22.5	24.0	1.5	396	
207	24.0	25.5	1.5	98	
208	25.5	26.5	1.0	942	0.033
209	26.5	28.2	1.7	713	
210	28.2	30.0	1.8	210	
211	30.0	32.0	2.0	356	
212	35.2	37.1	1.9	52	
213	37.1	39.0	1.9	490	
214	41.3	42.3	1.0	606	
215	42.3	43.2	0.9	903	0.058
216	43.2	44.0	0.8	279	
217	74.4	75.4	1.0	20	
218	106.1	108.7	2.6	177	
219	113.5	115.2	1.7	542	
220	115.2	116.0	0.8	1720	0.057
221	116.0	116.5	0.5	5	
222	158.3	160.8	2.5	81	
223	160.8	162.6	1.8	66	
224	162.6	163.8	1.2	77	
225	163.8	165.5	1.7	68	
226	168.9	171.3	2.4	156	
227	171.3	174.1	2.8	10000	0.96)
228	174.1	176.8	2.7	1324	0.02) 9.9
229	176.8	178.7	1.9	285) @
230	178.7	181.2	2.5	1084	0.035) 0.29
231	181.2	183.2	2.0	300	
232	183.2	185.2	2.0	460	
233	185.2	187.0	1.8	248	
234	187.0	189.5	2.5	108	
235	189.5	191.8	2.3	189	

236	191.8	194.0	2.2	10000	0.47)5.0
237	194.0	195.7	1.7	1460	0.055) @
238	195.7	196.8	1.1	1268	0.045)0.24
239	196.8	199.0	2.2	273	
240	199.0	201.0	2.0	1153	0.040
241	206.0	207.4	1.4	5	
242	212.5	214.0	1.5	600	
243	214.0	216.6	2.6	3769	0.11
244	227.8	228.8	1.0	99	
245	230.2	231.4	1.2	8	
246	231.4	232.7	1.3	10000	0.37)2.6
247	232.7	234.0	1.3	10000	0.69) @
248	234.0	235.2	1.2	260	0.53
249	235.2	236.8	1.6	625	
250	254.0	256.0	2.0	106	
251	263.25	265.75	2.5	216	
252	265.75	268.25	2.5	219	
253	268.25	270.0	1.75	821	0.025
254	363.2	366.0	2.8	1108	0.035
255	366.0	369.3	3.3	249	
256	369.3	371.3	2.0	279	
257	397.9	401.8	3.9	102	
258	401.8	404.5	2.7	5	
259	404.5	408.0	3.5	13	
260	420.0	423.0	3.0	55	
261	423.0	425.5	2.5	246	
262	445.0	449.0	4.0	6765	0.23
263	469.5	471.8	2.3	10000	2.55)uncut
264	471.8	473.8	2.0	10000	0.40)1.55 cut 0.72
265	490.0	492.0	2.0	10000	0.51
266	492.0	494.0	2.0	304	
267	509.3	512.5	3.2	254	
268	512.5	514.5	2.0	127	
269	521.0	522.5	1.5	298	

270	522.5	524.5	2.0	202	
271	524.5	526.0	1.5	105	
272	531.0	534.0	3.0	146	
273	811.5	814.0	2.5	106	
274	814.0	817.0	3.0	5	
275	817.0	820.0	3.0	5	
276	820.0	821.5	1.5	5	
277	821.5	823.0	1.5	8	
278	946.0	948.2	2.2	290	
279	954.0	955.5	1.5	19	
280	1121.0	1124.0	3.0	321	
281	1124	1127	3.0	16	
282	1127	1130	3.0	13	
283	1130	1133.0	3.0	13	
284	1133.0	1136.0	3.0	2815	0.091)9ft.
285	1136.0	1139.0	3.0	10000	0.65)@
286	1139.0	1142.0	3.0	3836	0.13)0.29
287	1142.0	1145.0	3.0	5	
288	1145.0	1149.75	4.75	83	
289	1220.0	1224.5	4.5	448	
290	1224.5	1227.0	2.5	24	
291	1227.0	1230.0	3.0	49	
292	1230.0	1232.5	2.5	262	
293	1232.5	1235.0	2.5	1975	0.065
294	1235.0	1238.0	3.0	537	
295	1238.0	1242.2	4.2	11	
296	1242.2	1246.0	3.8	387	
297	1256.0	1259.0	3.0	47	
298	1259.0	1261.0	2.0	5348	0.15

The table below lists the assay results of Hole #BR 87-08:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
301	41.0	42.5	1.5	5	
302	51.5	54.0	3.5	346	
303	54.0	57.0	3.0	5	
304	69.0	71.5	2.5	5	
305	71.5	74.0	2.5	83	
306	74.0	76.0	2.0	20	
307	76.0	78.2	2.2	5	
308	90.0	92.5	2.5	5	
309	107.0	109.0	2.0	56	
310	139.7	141.3	1.6	95	
311	141.3	144.0	2.7	1987	0.058
312	144.0	146.5	2.5	265	
313	146.5	148.5	2.0	47	
314	148.5	151.5	3.0	56	
315	151.5	153.5	2.0	26	
316	153.5	155.2	1.7	5	
317	171.5	174.5	3.0	5	
318	174.5	177.6	3.1	5	
319	201.4	203.0	1.6	5	
320	203.0	206.0	3.0	5	
321	258.5	261.5	3.0	402	
322	270.0	272.7	2.7	283	
323	377.5	378.5	1.0	109	
324	491.0	495.0	4.0	144	
325	577.0	581.5	4.5	75	
326	641.0	643.6	2.6	515	
327	679.5	681.8	2.3	5	
328	681.8	684.8	3.0	5	
329	684.8	686.8	2.0	5	
330	686.8	688.8	2.0	5	

331	707.5	710.5	5.0	5	
332	710.5	714.0	3.5	5	
333	732.0	733.0	1.0	23	
334	733.0	737.5	4.0	112	
335	737.5	738.5	1.0	413	
336	753.5	754.5	1.0	92	
337	762.8	764.5	1.7	1779	0.069
338	770.0	773.5	3.5	5	
339	786.4	788.7	2.3	49	
340	788.7	791.4	1.7	5	
341	791.4	794.4	3.0	5	
342	794.4	797.4	3.0	5	
343	797.4	800.4	3.0	5	
344	800.4	803.4	3.0	5	
345	803.4	805.8	2.4	5	
346	805.8	808.1	2.3	5	
347	808.1	811.0	2.9	5	
348	811.0	814.5	3.5	5	
349	832.0	834.7	2.7	5	
350	848.0	849.0	1.0	5	
351	886.0	887.5	1.5	283	
352	891.0	892.6	1.6	162	
353	960.5	963.5	3.0	27	
354	963.5	965.8	2.3	13	
355	965.8	967.75	1.95	5	
356	970.0	974.8	4.8	67	
357	1066.7	1069.8	3.1	24	
358	1069.8	1072.5	2.7	37	
359	1072.5	1075.7	3.2	21	
360	1081.5	1082.7	1.2	27	
361	1084.0	1088.0	4.0	37	
362	1088.0	1092.0	4.0	56	

			3		
363	1097.5	1099.9	2.4	5	
364	1502.9	1504.5	1.6	868	0.027
365	1511.0	1511.5	0.5	89	
366	1520.0	1522.0	2.0	5	

The table below lists the assay results of Hole #BR 87-09:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
367	46.5	48.3	1.8	5	
368	48.3	50.0	1.7	5	
369	59.5	60.5	1.0	21	
370	60.5	62.2	1.7	86	
371	62.2	65.2	3.0	5	
372	70.0	72.0	2.0	5	
373	72.0	74.0	2.0	5	
374	80.5	81.5	1.0	5	
375	83.0	86.0	3.0	5	
376	88.0	89.2	1.2	5	
377	91.0	92.2	1.2	5	
378	103.7	106.0	2.3	5	
379	106.0	108.0	2.0	5	
380	108.0	110.0	2.0	5	
381	110.0	111.0	1.0	5	
382	156.0	157.8	1.8	5	
383	157.8	160.0	2.2	5	
384	160.0	162.3	2.3	5	
385	162.3	164.3	2.0	5	
386	164.3	167.0	2.7	5	
387	167.0	169.5	2.5	265	
388	169.5	171.0	1.5	5	
389	171.0	173.5	2.5	5	
390	216.0	218.2	2.2	163	
391	218.2	221.0	2.8	6690	0.16
392	221.0	224.0	3.0	217	
393	236.8	238.2	1.4	5	
394	246.0	248.5	2.5	5	
395	248.5	251.0	2.5	5	
396	397.0	400.5	3.5	5	

397	452.0	454.8	2.8	169	
398	464.3	466.0	1.7	5	
399	471.0	476.0	5.0	5	
400	480.0	484.0	4.0	5	
401	555.9	560.0	4.1	5	
402	560.0	564.5	4.5	5	
403	685.5	688.0	2.5	5	
404	705.8	710.0	4.2	5	
405	710.0	713.0	3.0	5	
406	713.0	716.5	3.5	5	
407	832.5	837.0	4.5	5	
408	837.0	842.0	5.0	505	
409	863.0	867.0	4.0	5	
410	867.0	870.0	3.0	5	
411	870.0	872.2	2.2	5	
412	889.0	892.0	3.0	147	
413	909.9	911.0	1.1	188	
414	912.0	913.5	1.5	5	
415	976.9	979.5	2.6	5	
416	992.7	993.5	0.8	5	
417	1034.4	1034.7	0.3	5	
418	1044.0	1047.5	3.5	96	
419	1063.0	1065.5	3.5	5	
420	1123.9	1127.2	3.3	5	
421	1127.2	1130.2	3.0	5	
422	1130.2	1133.5	3.3	7504	0.25
423	1137.6	1139.0	1.4	2982	0.097
424	1139.0	1141.5	2.5	403	
425	1141.5	1142.5	1.0	32	

426	1175.8	1176.7	0.9	41
427	1294.0	1297.0	3.0	5
428	1297.0	1300.2	3.2	102
429	1300.2	1303.0	2.8	64
430	1303.0	1307.0	4.0	64
431	1307.0	1308.5	1.5	51
432	1312.0	1315.0	3.0	48
433	1568.5	1573.0	4.5	118
434	1848	1850.5	2.5	5

The table below lists the assay results of Hole #BR 87-10:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
435	31.5	35.2	3.7	180	
436	71.6	75.1	3.5	5	
437	96.8	98.0	1.2	5	
438	224.9	228.0	3.1	5	
439	228.0	233.0	5.0	5	
440	239.5	242.0	2.5	5	
441	242.0	245.0	3.0	211	
442	299.0	302.5	3.5	5	
443	322.8	324.9	2.1	5	
444	332.0	332.9	0.9	15	
445	332.9	336.0	3.1	48	
446	336.0	340.0	4.0	72	
447	382.0	384.0	2.0	40	
448	384.0	385.0	1.0	29	

The table below lists the assay results of Hole #BR 87-11:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
449	44.0	44.7	0.7		0.29
452	44.7	47.7	3.0	170	
453	47.7	50.7	3.0	181	
454	50.7	53.0	2.3	136	
455	53.0	55.2	2.2	121	
456	58.9	60.9	2.0	272	
457	74.5	76.0	1.5	100	
458	91.0	94.1	3.1	205	
459	96.1	99.1	3.0	195	
491	99.1	101.0	1.9	5	
460	159.0	161.5	2.5	87	
461	164.5	166.5	2.0	71	
462	172.5	176.0	3.5	86	
463	176.0	179.0	3.0	47	
464	179.0	181.0	2.0	90	
465	238.0	241.0	3.0	119	
466	241.0	245.0	4.0	93	
467	245.0	247.3	2.3	75	
468	247.3	251.5	4.2	312	
469	298.0	301.0	3.0	75	
470	301.0	304.0	3.0	5	
471	304.0	309.0	5.0	35	
472	309.0	312.2	3.2	121	
473	312.2	316.8	4.6	19	
474	402.0	405.2	3.2	271	
475	492.1	495.1	3.0	321	
476	495.1	500.0	4.9	77	
477	500.0	502.0	2.0	56	
478	519.7	523.0	3.3	5	
479	523.0	524.4	1.4	19	
480	524.4	529.0	4.6	16	
481	582.4	587.2	4.8	5	

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482	600.0	604.0	4.0	5	
483	617.0	619.0	2.0	2258	0.068
484	637.0	639.0	2.0	5	
485	653.5	655.5	2.0	5	
486	676.0	678.0	2.0	321	
487	699.0	703.0	4.0	152	
488	703.0	707.0	4.0	5	
489	707.0	711.0	4.0	5	
490	724.8	728.6	3.8	230	

The table below lists the assay results of Hole #BR 87-12:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
492	32.0	35.0	3.0	3648	0.11
493	56.8	61.0	4.2	1699	0.043
494	61.0	64.0	3.0	402	
495	64.0	67.0	3.0	338	
496	67.0	70.0	3.0	109	
497	70.0	72.0	2.0	223	
498	72.0	74.0	2.0	342	
499	74.0	77.0	3.0	68	
500	77.0	79.4	2.4	283	
501	79.4	81.4	2.0	201	
502	81.4	84.0	2.6	132	
503	84.0	87.0	3.0	191	
504	102.0	105.8	3.8	1200	0.034
505	120.5	121.5	1.0	1944	0.052
506	121.5	124.0	2.5	123	
507	124.0	125.2	1.2	1200	0.044
508	125.2	126.5	1.3	57	
509	126.5	129.0	2.5	50	
510	129.0	130.5	1.5	82	
511	130.5	133.5	3.0	520	
512	133.5	134.5	1.0	839	
513	134.5	136.1	1.6	63	
514	136.1	138.5	2.4	675	
515	138.5	139.5	1.0	68	
516	139.5	142.0	2.5	73	
517	142.0	144.5	2.5	182	
518	144.5	147.0	2.5	292	
519	147.0	149.5	2.5	2107	0.060
520	149.5	151.5	2.0	903	
521	151.5	153.5	2.0	168	
522	153.5	154.2	0.7	77	
523	154.2	157.0	2.8	95	
524	224.5	227.0	2.5	118	
525	227.0	229.2	2.2	36	
526	229.2	230.7	1.5	59	
527	273.5	275.0	1.5	369	

528	283.5	285.0	1.5	529	
529	285.0	287.0	2.0	173	
530	287.0	289.5	2.5	456	
531	289.5	292.0	2.5	164	
532	292.0	294.8	2.8	177	
533	294.8	297.0	2.2	136	
534	297.0	297.8	0.8	150	
567	340.0	341.5	1.5	685	
568	341.5	342.5	1.0		0.28
569	342.5	344.7	2.2		0.54
570	344.7	346.5	1.8	692	
571	346.5	350.0	3.5	219	
572	350.0	351.8	1.8	303	
535	366.0	367.0	1.0	182	
536	367.0	369.0	2.0	4362	0.12
537	369.0	370.1	1.1	180	
538	370.1	373.0	2.9	474	
539	381.8	384.0	2.2	10000	0.81
540	384.0	386.5	2.5	215	
541	386.5	388.7	2.2	3691	0.13
542	397.5	401.0	3.5	3302	0.11
543	440.0	443.0	3.0	110	
544	498.8	501.8	3.0	100	
545	501.8	504.2	2.4	96	
546	504.2	506.0	1.8	80	
547	506.0	508.0	2.0	98	
548	596.6	599.6	3.0	306	
549	599.6	602.0	2.4	383	
550	619.0	622.0	3.0	305	
551	622.0	626.0	4.0	470	
552	626.0	629.0	3.0	406	
553	629.0	632.0	3.0	251	
573	699.0	700.8	1.8	515	
574	700.8	703.5	2.7	38	
554	770.0	773.0	3.0	250	
555	773.0	775.2	2.2	356	
556	775.2	778.0	2.8	324	

557	789.0	791.0	2.0	475
558	791.0	794.0	3.0	301
559	794.0	796.0	2.0	338
591	821.0	824.0	3.0	19
575	877.5	880.0	2.5	46
576	880.0	883.0	3.0	7
560	982.0	984.0	2.0	278
561	996.3	999.3	3.0	228
562	999.3	1002.0	2.7	246
563	1002.0	1003.0	1.0	397
564	1003.0	1005.5	2.5	274
565	1005.5	1007.0	1.5	361
566	1007.0	1011.0	4.0	342
585	1390.0	1391.0	1.0	42
577	1402.0	1404.2	2.2	8
578	1404.2	1408.0	3.8	5
579	1408.0	1409.7	1.7	80
580	1409.7	1411.2	2.5	65
581	1411.2	1413.0	1.8	7
582	1413.0	1415.0	2.0	76
583	1415.0	1416.8	1.8	34
584	1416.8	1420.8	4.0	38
586	1467.0	1470.0	3.0	10
587	1678.5	1679.5	1.0	199
588	1683.0	1684.0	1.0	103
589	1722.0	1723.5	1.5	42
590	1728.0	1730.0	2.0	69

The table below lists the assay results of Hole #BR 87-13:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
592	205.5	206.5	1.0	10000	1.42
593	206.5	210.0	3.5	976	0.02
594	210.0	213.0	3.0	2884	0.072
595	213.0	217.0	4.0	153	
596	217.0	220.0	3.0	7	
597	220.0	223.0	3.0	31	
598	241.5	243.0	1.5	1048	0.031
599	245.0	246.5	1.5	186	
600	263.0	268.0	5.0	10000	0.36
601	268.0	270.2	2.2	10000	0.38
602	274.8	276.1	1.3	580	0.013
603	277.5	282.0	4.5	344	
604	282.0	286.5	4.5	306	
605	286.5	290.7	4.2	268	
606	290.7	293.0	2.3	256	
607	293.0	297.0	4.0	232	
608	310.5	312.0	1.5	214	
609	359.7	362.0	2.3	285	
610	362.0	366.0	4.0	246	
611	421.5	423.0	1.5	247	
612	424.5	428.0	3.5	234	
613	456.0	457.5	1.5	652	0.018
614	489.0	492.0	3.0	290	
615	492.0	494.5	2.5	392	
616	563.5	564.5	1.0	127	
617	615.3	618.0	2.7 VG	10000	0.35
618	632.0	633.5	1.5	134	
619	668.0	671.0	3.0	108	

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620	783.0	785.5	2.5	1060	0.029
621	794.0	795.5	1.5	492	0.020
622	859.0	864.0	5.0	558	0.017

The table below lists the assay results of Hole #BR 87-14:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
623	240.0	242.0	2.0	127	
624	445.8	446.6	0.8	3180	0.090
625	492.0	494.3	2.3	10000	0.36
626	503.0	506.0	3.0	9254	0.34
627	517.0	519.5	2.5	462	0.016
628	525.8	528.0	2.2	1100	0.041
629	528.0	531.0	3.0	397	
630	545.3	547.0	1.7	244	
631	547.0	552.0	5.0	290	
632	552.0	554.5	2.5	356	
633	564.0	565.8	1.8	1395	0.043
634	565.8	570.0	4.2	278	
635	629.5	630.0	0.5	924	0.033
636	644.5	647.0	2.5	276	
637	647.0	650.5	3.5	662	0.014
638	690.5	692.0	1.5	10000	0.30
639	724.5	727.0	2.5	690	0.011
640	727.0	729.8	2.8	448	0.025
641	735.8	736.2	0.4	214	
642	747.2	748.0	0.8	276	

The table below lists the assay results of Hole # 87-15:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
643	59.5	61.5	2.0	1488	0.052
644	70.0	73.4	3.4	866	0.038
645	142.0	144.0	2.0	100	
646	242.0	245.5	3.5	599	0.015
647	289.0	290.0	1.0	380	
648	310.0	313.0	3.0	4470	0.17
649	313.0	316.0	3.0	276	
650	352.0	354.0	2.0	7218	0.26
651	387.5	389.5	2.0	274	
652	289.5	393.0	3.5	946	0.033
653	461.0	463.5	2.5	985	0.041
654	476.5	479.5	3.0	600	0.019
655	479.5	482.5	3.0	199	
656	482.5	485.0	2.5	282	
657	504.0	508.5	4.5	326	
658	508.5	512.5	4.0	52	
659	512.5	515.5	3.0	40	
660	532.5	538.0	5.5	25	
661	538.0	542.0	4.0	97	
662	542.0	547.0	5.0	123	
663	547.0	552.0	5.0	60	
664	552.0	554.5	2.5	51	
665	569.0	571.0	2.0	62	
666	580.0	585.0	5.0	73	
667	597.0	600.5	3.5	221	
668	612.0	614.0	2.0	1718	0.060
669	641.5	643.0	1.5	1466	0.043

670	655.0	656.0	1.0	49	
671	667.7	671.2	3.5	167	
672	684.5	688.0	3.5	155	
673	701.0	705.0	4.0	3668	0.13
674	705.0	710.0	5.0	2095	0.052
675	710.0	713.7	3.7	2658	0.081
676	726.5	732.0	5.5	763	0.023
677	783.0	788.0	5.0	152	
678	862.0	864.0	2.0	150	
679	873.5	876.0	2.5	91	
680	876.0	880.0	4.0	173	
681	1065.0	1070.0	5.0	110	
682	1115.0	1118.5	3.5	141	
683	1170.7	1174.0	3.3	295	
684	1188.5	1192.5	4.0	2018	0.058
685	1192.5	1196.0	3.5	873	0.030
686	1196.0	1201.0	5.0	572	0.015
687	1232	1235.0	3.0	961	0.026
688	1277.5	1280.0	2.5	239	
689	1280.0	1284.0	4.0	554	0.015
690	1284.0	1288.0	4.0	194	
691	1288.0	1291.0	3.0	191	
692	1291.0	1295.0	4.0	238	
693	1334.2	1337.0	2.8	163	
694	1337.0	1342.0	5.0	28	
695	1347.0	1348.2	1.2	61	
696	1433.3	1436.5	3.2	19	
697	1436.5	1441.7	5.2	1351	0.047*0.039
698	1441.7	1446.0	4.3	3302	0.096*0.092
699	1446.0	1450.0	4.0	889	0.036*0.030
700	1450.0	1452.5	2.5	3402	0.10 *0.083

701	1475.0	1480.0	5.0	913	0.034
702	1480.0	1484.0	4.0	1281	0.041
703	1484.0	1488.0	4.0	837	0.027
704	1488.0	1491.0	3.0	179	
705	1491.0	1494.0	3.0	341	
706	1581.5	1587.5	6.0	867	0.028
707	1651.0	1654.0	3.0	228	
708	1661.0	1666.0	5.0	87	
709	1666.0	1669.5	3.5	537	
710	1669.5	1671.5	2.0	50	
711	1705.5	1710.0	4.5	2195	0.062
712	1741.0	1745.0	4.0	741	0.026
713	1745.0	1748.0	3.0	96	

* Free Gold Method

The table below lists the assay results of Hole #BR 87-16:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
714	128.0	131.5	3.5	63	
715	328.0	330.0	2.0	72	
716	330.0	332.0	2.0	19	
720	501.0	502.5	1.5	59	
721	509.5	512.0	2.5	35	
722	559.0	562.5	3.5	77	
723	622.0	624.2	2.2	1804	0.081
724	709.5	712.0	2.5	148	
725	723.5	725.5	2.0	69	
726	735.5	740.0	4.5	5	
727	774.3	777.0	2.7	1700	0.047
728	777.0	780.5	3.5	99	
729	780.5	783.8	3.3	4456	0.11
730	788.5	792.5	4.0	239	
731	792.5	797.0	4.5	243	
732	797.0	800.0	3.0	401	0.012
733	819	823.0	4.0	89	
734	823.0	825.5	2.5	134	
735	825.5	827.1	1.6	141	
736	827.1	832.0	4.9	2103	0.073
737	838.5	841.5	3.0	9481	0.31* 0.26
738	841.5	844.5	3.0	1677	0.049 0.053
739	846.0	851.0	5.0	1928	0.066
740	851.0	856.5	5.5	521	0.017
741	899.2	902.0	2.8	1374	0.037
742	907.0	912.0	5.0	560	0.014
743	912.0	913.5	1.5	631	0.021

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744	924.0	928.5	4.5	VG	2534	0.11*	0.070
745	931.0	934.5	3.5		379		
717	971.5	975.0	3.5	VG	2632	0.095*	0.078
718	975.0	976.8	1.8		667		
719	976.8	979.1	2.3	VG	2191	0.068*	0.051
746	1006.0	1008.0	2.0		526		0.041
747	1116.2	1119.0	2.8		60		
748	1203.0	1206.5	3.5		110		

*Free Gold Method

The table below lists the assay results of Hole #BR87-17:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
10512	637.0	638.5	1.5VG		0.01
10513	991.0	993.0	2.0	229	
10516	1368.5	1373.0	4.5	199	
10517	1582.0	1585.0	3.0	377	
10518	1585.0	1590.0	5.0	338	
10519	1590.0	1595.0	5.0	959	0.023
10520	1595.0	1598.0	3.0	141	
10521	1598.0	1601.5	3.5	53	
10522	1635.0	1639.0	4.0	815	0.027
10523	1639.0	1643.0	4.0	167	
10524	1643.0	1648.0	5.0	298	
10525	1716.5	1719.5	3.0	439	0.013
10526	1830.0	1832.0	2.0	587	0.015
10527	1888.0	1893.0	5.0	315	
10528	1912.0	1917.0	5.0	303	
10529	1917.0	1922.0	5.0	79	
10530	1922.0	1927.0	5.0	758	0.023
10531	1927.0	1931.0	4.0	121	
10532	1931.0	1932.5	1.5	343	
10533	1932.5	1937.0	4.5	107	
10534	1937.0	1942.0	5.0	115	
10535	1942.0	1946.0	4.0	119	
10536	1946.0	1949.0	3.0	163	

The table below lists the assay results of Hole #BR87-18:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
790	252.0	255.0	3.0	24	
791	255.0	257.5	2.5	79	
792	312.0	314.5	2.5	328	
793	362.5	365.0	2.5	68	
794	398.0	402.5	4.5	119	
795	467.0	470.0	3.0	136	
796	488.0	489.0	1.0	507	0.013
797	541.0	544.0	3.0	83	
798	566.8	572.0	5.2	70	
799	572.0	575.0	3.0	93	
800	582.0	585.0	3.0	52	
801	585.0	588.5	3.5	70	
802	609.0	610.5	1.5	11	
803	811.5	814.7	3.2	76	
804	830.0	834.0	4.0	82	
805	834.0	838.0	4.0	48	
806	838.0	842.0	4.0	105	
807	842.0	846.0	4.0	31	
808	846.0	850.0	4.0	58	
809	850.0	855.5	5.5	162	
810	888.3	889.9	1.6	10000	0.43
811	896.8	902.1	5.3	995	0.029
812	902.1	906.8	4.7	988	0.028
813	906.8	910.0	3.2	1450	0.039
814	910.0	914.0	4.0	10000*	0.14
815	914.0	918.0	4.0	1600*	/8'
816	918.0	923.0	5.0	330	0.053
817	923.0	927.0	4.0	828	0.023
819	933.0	937.0	4.0	424	0.011
820	937.0	942.0	5.0	1472	0.035
821	942.0	947.0	5.0	1598	0.047

822	947.0	950.0	3.0	1350	0.039
818	975.7	977.2	1.5 VG		0.37
823	1004.5	1009.0	4.5	52	
824	1009.0	1014.0	5.0	31	
825	1014.0	1019.0	5.0	43	
826	1019.0	1021.3	2.3	61	
827	1034.5	1037.0	2.5	67	
828	1037.0	1040.2	3.2	50	
829	1075.0	1078.0	3.0	98	
830	1097.0	1102.0	5.0	93	
831	1109.8	1115.0	5.2	85	
832	1115.0	1119.0	4.0	171	
833	1119.0	1122.0	3.0	77	
834	1122.0	1127.0	5.0	48	
835	1127.0	1132.0	5.0	35	
836	1132.0	1137.0	5.0	112	
837	1137.0	1142.0	5.0	128	
838	1142.0	1147.0	5.0	67	
839	1147.0	1153.0	6.0	50	

The table below lists the assay results of Hole #BR87-19:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
749	120.0	122.0	2.0	149	
750	122.0	124.5	2.5	110	
751	264.0	267.0	3.0	1489*	0.060
752	267.0	270.0	3.0	2295*	0.22 0.080
753	270.0	271.5	1.5	3991*	/11' 0.14
754	271.5	273.5	2.0	10000*	0.72
755	273.5	275.0	1.5	6450*	0.20
756	283	284.0	1.0	3600	0.11
757	284.0	286.0	2.0	351	
758	286.0	288.0	2.0	145	
759	288.0	291.0	3.0	594	0.014
760	291.0	293.2	2.2	430	
761	293.2	297.0	3.8	1129	0.029
762	297.0	301.0	4.0	10000*	0.87
763	301.0	305.0	4.0	3668*	0.23 0.13
764	305.0	309.0	4.0	1996*	/20' 0.059
765	309.0	313.0	4.0	2050*	0.058
766	313.0	317.0	4.0	1532*	0.040
767	317.0	319.0	2.0	772	0.019
768	319.0	323.0	4.0	306	
769	323.0	328.0	5.0	895	0.029
770	328.0	332.0	4.0	453	0.013
771	332.0	334.0	2.0	2500	0.075
772	334.0	338.5	4.5	1200	0.037
773	348.0	351.0	3.0	2150	0.065
774	402.0	404.0	2.0	110	
775	404.0	408.5	4.5	166	
776	408.5	413.0	4.5	499	0.016
777	413.0	416.0	3.0	343	
778	416.0	418.5	2.5	970	0.024
779	418.5	422.0	3.5	175	
780	428.0	432.0	4.0	1738	0.050
781	432.0	436.0	4.0	3748	0.11
782	436.0	440.0	4.0	828	0.029
783	440.0	443.0	3.0	145	
784	502.0	504.0	2.0	3120	0.089
785	506.0	510.0	4.0	628	0.020

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786	510.0	514.0	4.0	590	0.017
787	514.0	519.0	5.0	333	
788	519.0	524.0	5.0	430	0.011
789	524.0	529.0	5.0	48	

The table below lists the assay results of Hole #BR87-20:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
840	101.0	103.0	2.0	41	
841	103.0	106.0	3.0	79	
842	185.5	186.5	1.0	1976	0.066
843	206.0	207.7	1.7	4600	0.11
844	298.5	301.0	2.5	1400	0.057
845	301.0	305.0	4.0	355	
846	305.0	309.0	4.0	288	
847	320.0	322.3	2.3	1495	0.049
848	337.0	342.0	5.0	263	
849	342.0	347.0	5.0	305	
850	484.0	487.0	3.0	379	
851	487.0	491.0	4.0	111	
852	491.0	495.5	4.5	65	
853	574.0	577.0	3.0	80	
854	577.0	580.0	3.0	56	
855	580.0	583.5	3.5	351	
856	695.0	699.0	4.0	315	
857	699.0	703.0	4.0	127	
858	703.0	705.0	2.0	161	
859	705.0	708.0	3.0	92	
860	1033.0	1037.0	4.0	954	0.031
861	1037.0	1040.0	3.0	115	
862	1040.0	1042.0	2.0	87	
863	1042.0	1045.0	3.0	834	0.023
864	1045.0	1047.0	2.0	141	
865	1105.0	1108.0	3.0	119	
866	1108.0	1109.5	1.5		0.01
867	1109.5	1112.0	2.5	290	

The table below lists the assay results of Hole #BR87-21A:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
868	178.0	181.0	3.0	1842	0.050
869	181.0	184.0	3.0	2461	0.072
870	184.0	186.8	2.8	7258	0.19
871	186.8	189.2	2.4	1950	0.050
872	189.2	192.0	2.8	4280	0.11
873	192.0	196.0	4.0	2316	0.059
874	196.0	198.5	2.5	1950	0.056
875	212.5	216.5	4.0	2304	0.071
876	224.0	227.0	3.0	2320	0.066
877	227.0	230.0	3.0	1858	0.055
878	240.0	244.0	4.0	630	0.020
879	244.0	248.0	4.0	1121	0.033
880	248.0	252.0	4.0	4064	0.11
881	252.0	256.0	4.0	906	0.029
882	256.0	259.1	3.1	369	0.018
883	272.0	276.0	4.0	1303	0.042
884	276.0	280.5	4.5	414	0.025
885	280.5	286.0	5.5	383	
886	286.0	289.5	3.5	131	
887	289.5	293.0	3.5	516	0.016
888	293.0	297.0	4.0	1985	0.060
889	297.0	301.0	4.0	271	
890	301.0	306.5	5.5	61	
891	306.5	308.5	2.0	347	
892	315.5	318.6	3.1	59	
893	337.5	341.0	3.5	87	
894	341.0	343.0	2.0	35	
895	343.0	345.5	2.5	400	0.011
896	352.0	357.0	5.0	221	
897	357.0	362.0	5.0	67	
10901	390.0	395.0	5.0	147	
10902	410.5	413.0	2.5	1580	0.047
10903	413.0	418.5	5.5	791	0.023
10904	418.5	420.5	2.0	202	
10905	420.5	423.0	2.5	599	0.014

10906	423.0	427.0	4.0	389		
10907	427.0	430.0	3.0	351		
10908	430.0	434.5	4.5	247		
10909	434.5	438.0	3.5	681		0.014
10910	438.0	442.5	4.5	1018		0.028
10911	442.5	448.0	5.5	312		
10912	485.0	490.0	5.0	105		
10913	490.0	495.0	5.0	1118		0.036
10914	512.0	517.0	5.0	281		
10915	517.0	522.0	5.0	287		
10916	522.0	527.0	5.0	681		0.019
10917	527.0	532.0	5.0	135		
10918	571.0	576.0	5.0	133		
10919	576.0	581.5	5.5	87		
10920	608.0	611.0	3.0	207		
10921	611.0	615.0	4.0	169		
10922	615.0	620.0	5.0	281		
10923	620.0	625.0	5.0	97	
10924	625.0	628.0	3.0	927	0.22	0.030
10925	628.0	631.0	3.0	VG	/11'	0.15
10926	631.0	636.0	5.0	10000	0.37
10927	647.5	651.0	3.5	451		0.011
10928	651.0	655.0	4.0	91		
10929	655.0	659.0	4.0	59		
10930	659.0	662.0	3.0	119		
10931	678.5	683.0	4.5	145		
10932	683.0	687.0	4.0	905		0.023

The table below lists the assay results of Hole #BR87-22:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
10692	93.0	96.0	3.0	115	
10693	96.0	99.0	3.0	118	
10694	187.0	190.0	3.0	2002	0.060
10695	190.0	193.5	3.5	1771	0.056
10696	221.0	223.0	2.0	441	0.016
10697	277.5	280.0	2.5	79	
10698	280.0	282.0	2.0	63	
10699	282.0	285.0	3.0	71	
10700	285.0	288.0	3.0	83	
10701	288.0	291.0	3.0	125	
10702	310.0	312.5	2.5	151	
10703	312.5	315.0	2.5	986	0.036
10704	509.0	512.5	3.5	112	
10705	594.5	597.5	3.0	103	
10706	597.5	601.0	3.5	75	
10707	611.0	614.0	3.0	77	
10708	614.0	616.0	2.0	259	
10709	616.0	619.0	3.0	492	0.015
10710	619.0	621.0	2.0	77	
10711	897.5	902.0	4.5	111	
10712	902.0	907.0	5.0	131	
10713	907.0	912.0	5.0	165	
10714	912.0	917.0	5.0	661	0.015
10715	917.0	922.0	5.0	1337	0.042
10716	922.0	925.5	3.5	1015	0.017
10717	938.0	942.0	4.0	930	0.032
10718	942.0	946.0	4.0	795	0.022
10719	946.0	951.0	5.0	6000	0.18
10720	951.0	954.0	3.0	369	
10721	954.0	957.0	3.0	331	
10722	957.0	961.0	4.0	3311	0.11
10723	961.0	964.5	3.5	1355	0.038

The table below lists the assay results of Hole #BR87-23:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
10933	52.0	54.0	2.0	2022	0.051
10934	54	57.0	3.0	331	
10935	57.0	60.0	3.0	8344	0.25
10936	145.0	148.0	3.0	845	0.024
10937	148.0	151.0	3.0	2241	0.063
10938	151.0	153.0	2.0	1356	0.041
10939	165.0	168.0	3.0	2631	0.091
10940	168.0	171.0	3.0	1363	0.040
10941	171.0	174.0	3.0	6211	0.15
10942	174.0	178.0	4.0	329	
10943	368.5	373.0	4.5	... 991	0.030
10944	373.0	376.0	3.0	VG	0.63
10945	376.0	379.0	3.0	2500	0.063
10946	379.0	381.0	2.0	0.28 10000	0.77
10947	381.0	384.0	3.0	/15' 1032	0.033
10948	384.0	388.0	4.0	... 4754	0.12
10949	388.0	393.5	5.5	781	0.022
10950	393.5	396.5	3.0	322	
10951	396.5	400.0	3.5	553	0.018
10952	400.0	405.0	5.0	331	
10953	405.0	409.5	4.5	461	0.014
10954	432.0	435.5	3.5	612	0.017
10955	496.0	499.0	3.0	1121	0.031
10956	542.0	545.5	3.5	115	
10957	576.0	579.0	3.0	... 279	
10958	579.0	581.5	2.5	VG 10000	0.85
10959	581.5	586.0	4.5	10000	0.27
10960	586.0	591.0	5.0	0.20 1706	0.05
10961	591.0	594.0	3.0	/24' 3900	0.13
10962	594.0	597.0	3.0	3135	0.085
10963	597.0	599.5	2.5	400	0.011
10964	599.5	603.0	3.5	... 3700	0.11
10965	603.0	608.0	5.0	965	0.029
10966	633.0	638.0	5.0	983	0.029

10967	703.0	708.0	5.0		3700	0.11
10968	761.0	763.0	2.0		271	
10969	785.0	790.0	5.0		343	
10970	809.5	812.0	2.5		350	
10971	812.0	816.0	4.0		2389	0.069
10972	816.0	817.0	1.0	VG		0.13
10973	817.0	821.0	4.0		950	0.026
10974	821.0	824.0	3.0		305	
10975	824.0	828.0	4.0		973	0.029
10976	847.0	853.0	6.0		988	0.030
10977	859.0	863.0	4.0		995	0.028
10978	863.0	867.0	4.0		304	
10979	867.0	872.0	5.0		431	0.012
10980	872.0	877.0	5.0		383	
10981	877.0	882.0	5.0		378	
10982	882.0	887.0	5.0		201	

The table below lists the assay results of Hole #BR87-24:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
10990	76.0	79.0	3.0	81	
10991	79.0	82.0	3.0	92	
10992	82.0	85.5	3.5	418	0.011
10993	191.0	192.0	1.0 VG		0.52
10994	375.0	378.0	3.0	1435	0.082
10995	378.0	381.0	3.0	1315	0.032
10996	381.0	384.0	3.0	4021	0.11
10997	384.0	387.5	3.5	401	0.011
10998	579.5	584.0	4.5	845	0.029
10999	584.0	588.0	4.0	1248	0.031
11000	588.0	594.0	6.0	191	
10501	594.0	597.0	3.0	528	0.015
10502	597.0	600.0	3.0	821	0.024
10503	608.0	613.0	5.0	489	0.013
10504	613.0	616.0	3.0	10000	0.29
10505	616.0	619.0	3.0	1251	0.033
10506	619.0	621.0	2.0	257	
10507	621.0	625.0	4.0	800	0.026
10508	625.0	629.0	4.0	171	
10509	629.0	633.0	4.0	123	
10510	633.0	638.0	5.0	261	
10511	638.0	642.0	4.0	898	0.026
10514	705.0	708.0	3.0	241	
10515	708.0	712.0	4.0	714	0.019
10537	750.0	753.8	3.8	255	
10538	759.7	764.0	4.3	974	0.020
10539	764.0	768.3	4.3	337	
10540	789.3	793.0	3.7	311	
10541	793.0	797.7	4.7	1234	0.037
10542	797.7	802.0	4.3	225	
10543	802.0	806.0	4.0	1510	0.050
10544	806.0	810.0	4.0	981	0.031
10545	810.0	814.0	4.0	641	0.018
10546	814.0	818.0	4.0	451	0.015
10547	818.0	822.0	4.0	381	

10548	822.0	827.0	5.0		273	
10549	842.5	844.3	1.8		1287	0.029
10550	844.3	846.3	2.0	VG	2070	0.048
10551	846.3	847.9	1.6		2156	0.067
10552	847.9	852.0	4.1		1785	0.051
10553	912.0	914.9	2.9	VG		0.49
10554	942.0	946.5	4.5		10000	0.30
10555	946.5	950.0	3.5		1921	0.043
10556	950.0	954.0	4.0		1115	0.035
10557	954.0	958.0	4.0		125	
10558	958.0	963.0	5.0		241	
10559	1066.5	1070.0	3.5		287	
10560	1070.0	1074.0	4.0		1014	0.027
10561	1074.0	1078.0	4.0		5575	0.16
10562	1078.0	1082.0	4.0		5960	0.18
10563	1082.0	1086.0	4.0		1403	0.039
10564	1086.0	1088.5	2.5		744	0.017
10565	1118.0	1122.0	4.0		126	
10566	1122.0	1127.0	5.0			
10567	1127.0	1132.0	5.0		265	
10568	1132.0	1137.0	5.0		85	
10569	1137.0	1143.0	6.0		79	
10570	1151.0	1155.0	4.0		1052	0.025

The table below lists the assay results of Hole #BR87-25A:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
10571	136.5	140.0	3.5	97	
10572	140.0	143.0	3.0	53	
10573	143.0	146.0	3.0	540	0.018
10574	146.0	149.0	3.0	10000	0.32
10575	149.0	152.0	3.0	3900	0.11
10576	152.0	156.0	4.0	1002	0.029
10577	361.6	366.0	4.7	338	
10578	425.3	429.0	3.7	301	
10579	429.0	433.0	4.0	127	
10580	433.0	436.0	3.0	101	
10581	436.0	442.0	6.0	763	0.029
10582	442.0	447.0	5.0	729	0.028
10583	447.0	452.0	5.0	1267	0.030
10584	452.0	457.0	5.0	2064	0.066
10585	457.0	460.0	3.0	2590	0.081
10586	460.0	463.0	3.0	8050	0.25
10587	463.0	467.0	4.0	1470	0.04
10588	482.5	487.0	4.5	1970	0.055
10589	487.0	492.0	5.0	1966	0.052
10590	492.0	496.0	4.0	2121	0.066
10591	496.0	500.0	4.0	1602	0.081
10592	527.0	531.5	4.5	918	0.025
10593	575.5	580.0	4.5	442	0.017
10594	580.0	584.0	4.0	141	
10595	614.0	619.0	5.0	230	
10596	619.0	624.0	5.0	67	
10597	624.0	629.0	5.0	179	
10598	629.0	634.0	5.0	25	
10599	634.0	639.0	5.0	151	
10600	662.0	666.0	4.0	130	
10601	762.0	767.0	5.0	95	
10602	767.0	770.5	3.5	159	
10603	899.0	903.0	4.0	4538	0.14

The table below lists the assay results of Hole #BR87-26:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
10604	154.0	157.0	3.0	630	0.025
10605	157.0	160.0	3.0	1421	0.042
10606	160.0	162.0	2.0	451	0.010
10607	162.0	165.0	3.0	4657	0.13
10608	165.0	168.5	3.5	4550	0.27
10609	168.5	171.0	2.5	10000	0.64
10610	171.0	174.0	3.0	3485	0.10
10611	174.0	177.5	3.5	800	0.026
10612	247.5	249.5	2.0	2350	0.071
10613	249.5	251.5	2.0	291	
10614	519.5	521.0	1.5	181	
10615	590.0	591.0	1.0 VG		0.22*
10616	599.0	601.5	2.5	831	0.025
10617	601.5	605.0	3.5	1361	0.045
10618	605.0	609.5	4.5	383	
10619	609.5	612.0	2.5	197	
10620	612.0	617.0	5.0	1380	0.040
10621	632.0	635.8	3.8	283	
10622	648.0	652.0	4.0	152	
10623	678.2	681.0	2.8	140	
10624	729.0	731.0	2.0	167	
10625	783.0	787.0	4.0	259	
10626	787.0	792.0	5.0	902	0.025
10627	792.0	797.0	5.0	107	
10628	797.0	802.0	5.0	125	
10629	802.0	807.0	5.0	215	...
10630	807.0	812.0	5.0	1000	0.19
10631	812.0	814.0	2.0 VG		/11' 0.88*
10632	814.0	818.0	4.0	1750	... 0.054
10633	818.0	822.0	4.0	305	
10634	822.0	827.0	5.0	127	
10635	827.0	829.5	2.5 VG		0.045*
10636	998.5	1002.0	3.5	165	

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10637	1002.0	1007.0	5.0	101
10638	1057.5	1060.0	2.5	99
10639	1060.0	1062.5	2.5	78

The table below lists the assay results of Hole #BR87-27:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
10640	52.5	54.0	1.5	1936	0.055
10641	174.5	176.0	1.5	401	0.013
10642	520.0	525.0	5.0	3021	0.097
10643	525.0	530.0	5.0	1955	0.058
10644	530.0	534.0	4.0	1936	0.057
10645	619.5	621.5	2.0	147	
10646	621.5	623.0	1.5	718	0.022
10647	623.0	626.0	3.0	1305	0.041
10648	626.0	629.0	3.0	757	0.025
10649	629.0	632.0	3.0	1239	0.035
10650	632.0	637.0	5.0	1082	0.035
10651	637.0	641.0	4.0	451	0.015
10652	644.5	646.2	1.7	95	
10653	664.3	665.8	1.5	261	
10654	673.0	677.0	4.0	534	0.44
10655	677.0	680.0	3.0	VG 10000	/7' cut 3.64*
10656	704.2	708.2	4.0	2846	0.091
10657	708.2	710.7	2.5	371	
10658	710.7	716.1	5.4	627	0.020
10659	716.1	718.8	2.7	217	
10660	718.8	723.5	4.7	746	... 0.022
10661	723.5	728.0	4.5	10000	0.27
10662	728.0	730.0	2.0	VG 10000	0.25
10663	730.0	735.0	5.0		/19.5 0.54*
10664	735.0	739.0	4.0	2532	0.083
10665	739.0	743.0	4.0	VG	... 0.028*
10666	743.0	747.1	4.1	374	
10667	762.5	767.0	4.5	575	0.016
10668	767.0	771.0	4.0	453	0.014
10669	771.0	774.0	3.0	339	
10670	778.5	782.0	3.5	881	0.027
10671	782.0	787.0	5.0	844	0.024
10672	787.0	792.0	5.0	1430	0.039
10673	792.0	797.0	5.0	1045	0.024

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10674	797.0	801.5	4.5	1061	0.026
10675	847.0	851.0	4.0	171	
10676	869.0	872.0	3.0	73	

The table below lists the assay results of Hole #BR87-28:

# sample	From (ft.)	to (ft.)	footage	Au ppb	Au oz./t
10677	107.8	110.5	2.7	1435	0.036
10678	110.5	113.5	3.0	337	
10679	129.5	132.5	3.0	1672	0.039
10680	132.5	135.5	3.0	257	
10681	135.5	138.5	3.0	25	
10682	138.5	141.0	2.5	123	
10683	174.0	176.0	2.0	625	0.022
10684	176.0	178.0	2.0	1417	0.037
10685	178.0	182.0	4.0	796	0.020
10686	270.0	273.0	3.0	473	0.016
10687	273.0	276.0	3.0	211	
10688	276.0	279.0	3.0	503	0.016
10689	279.0	282.0	3.0	678	0.023
10690	282.0	285.0	3.0	4105	0.11
10691	467.5	470.5	3.0	850	0.025
10724	678.3	682.0	3.7	371	
10725	682.0	686.0	4.0	1405	0.035
10726	686.0	689.0	3.0	7121	0.16
10727	689.0	693.5	4.5	512	0.014
10728	693.5	697.0	3.5	521	0.015
10729	697.0	699.0	2.0	267	
10730	699.0	703.0	4.0	381	
10731	703.0	707.0	4.0	469	0.013
10732	707.0	712.0	5.0	391	
10733	728.7	732.0	3.3	325	
10734	732.0	735.0	3.0	179	
10735	735.0	737.0	2.0	302	
10736	744.0	749.0	5.0	1207	0.017
10737	749.0	754.0	5.0	440	0.013
10738	789.5	790.5	1.0	VG	0.13*
10739	803.0	807.0	4.0	293	
10740	807.0	811.0	4.0	412	0.013
10741	811.0	815.0	4.0	279	
10742	815.0	819.0	4.0	471	0.013

10743	819.0	821.0	2.0	10000	0.266	0.42
10744	821.0	825.0	4.0	10000	/14'	0.34
10745	825.0	830.0	5.0	538		0.017
10746	830.0	833.0	3.0	10000		0.48
10747	833.0	836.5	3.5	169		
10748	867.0	871.0	4.0	10000	0.194	0.42
10749	871.0	875.0	4.0	5400	/15'	0.15
10750	875.0	878.0	3.0	231		
10751	878.0	882.0	4.0	5253		0.16
10752	906.5	909.0	2.5	233	0.13	
10753	909.0	912.0	3.0	5631	/5.5'	0.24
10754	918.0	921.0	3.0	1751		0.054
10755	921.0	925.0	4.0	1461		0.041
10756	936.0	941.0	5.0	1198		0.026
10757	985.0	988.0	3.0	253		
10758	988.0	992.0	4.0	1186		0.034
10759	1088.0	1093.0	5.0	633		0.017

APPENDIX III

LIST OF MAPS



LIST OF MAPS

✓ Drill Plan
Scale 1:5000

✓ Section 600m.E
Scale 1:1200

✓ Section 675m.E
Scale 1:1200

✓ Section 750m.E
Scale 1:1200

✓ Section 825m.E
Scale 1:1200

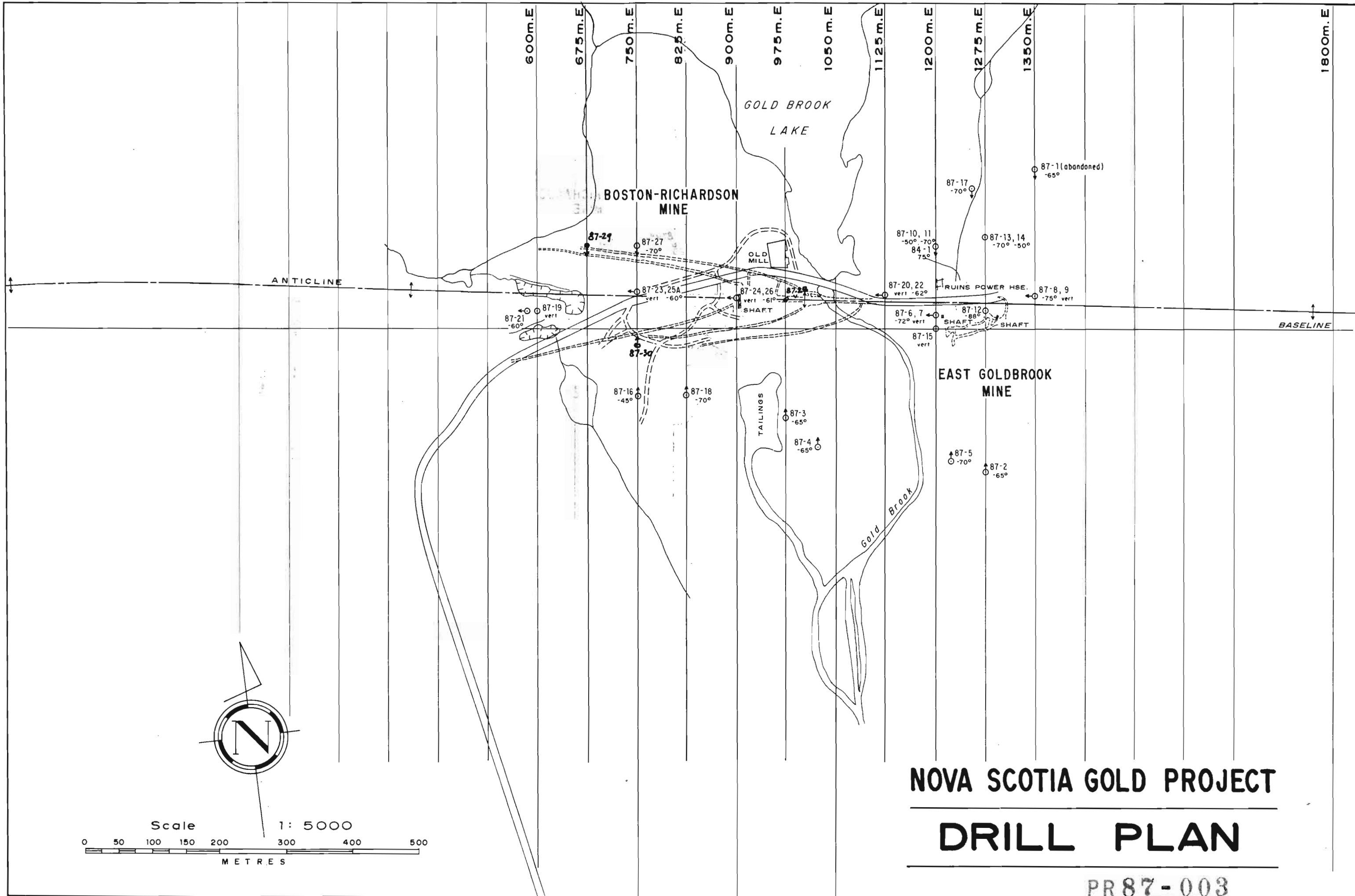
✓ Section 900m.E
Scale 1:1200

✓ Section 975m.E
Scale 1:1200

✓ Longitudinal Section - Looking North
Scale 1:1200

NY





NOVA SCOTIA GOLD PROJECT

DRILL PLAN

PR87-003

SOUTH

NORTH

78

Proposed Hole

BR-19

Proposed Hole

-65°

-75°

B-R BELT
MINED OUT

NEW BELT

Sub L.

0.22
11'

0.23
20'

3rd BELT

0.11
4'

1st L.

-500'L.
(152m.)

700'
650' (198.2m) 700' (213m.)

-1000'L.
(304m.)

PR 87-003

Trace Of

BOSTON-RICHARDSON BELT

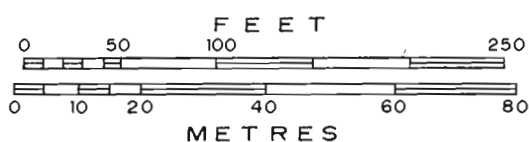
& Location Of

NEW BELT

Sect. 600m.E

NOTE: values expressed as oz / t (Au) over length (ft)

Scale 1:1200



SOUTH

NORTH

B.L.

Proposed Hole

Proposed Hole

-65°

-70°

B-R BELT
mined out

NEW BELT

Sub L.

1st L.

2nd L.

-500'L.
(152m.)

700'
(213m.)

700'
(213m.)

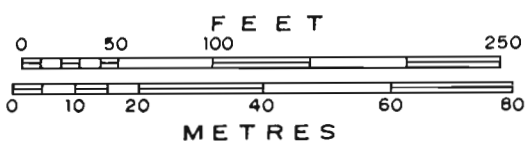
-1000'L.
(304m.)

PR 87-003

Trace Of
BOSTON-RICHARDSON BELT
& Location Of
NEW BELT

Sect. 675m.E

Scale 1:1200



SOUTH

NORTH

BR-16

0' -45°

32-30

BR-23

vert.

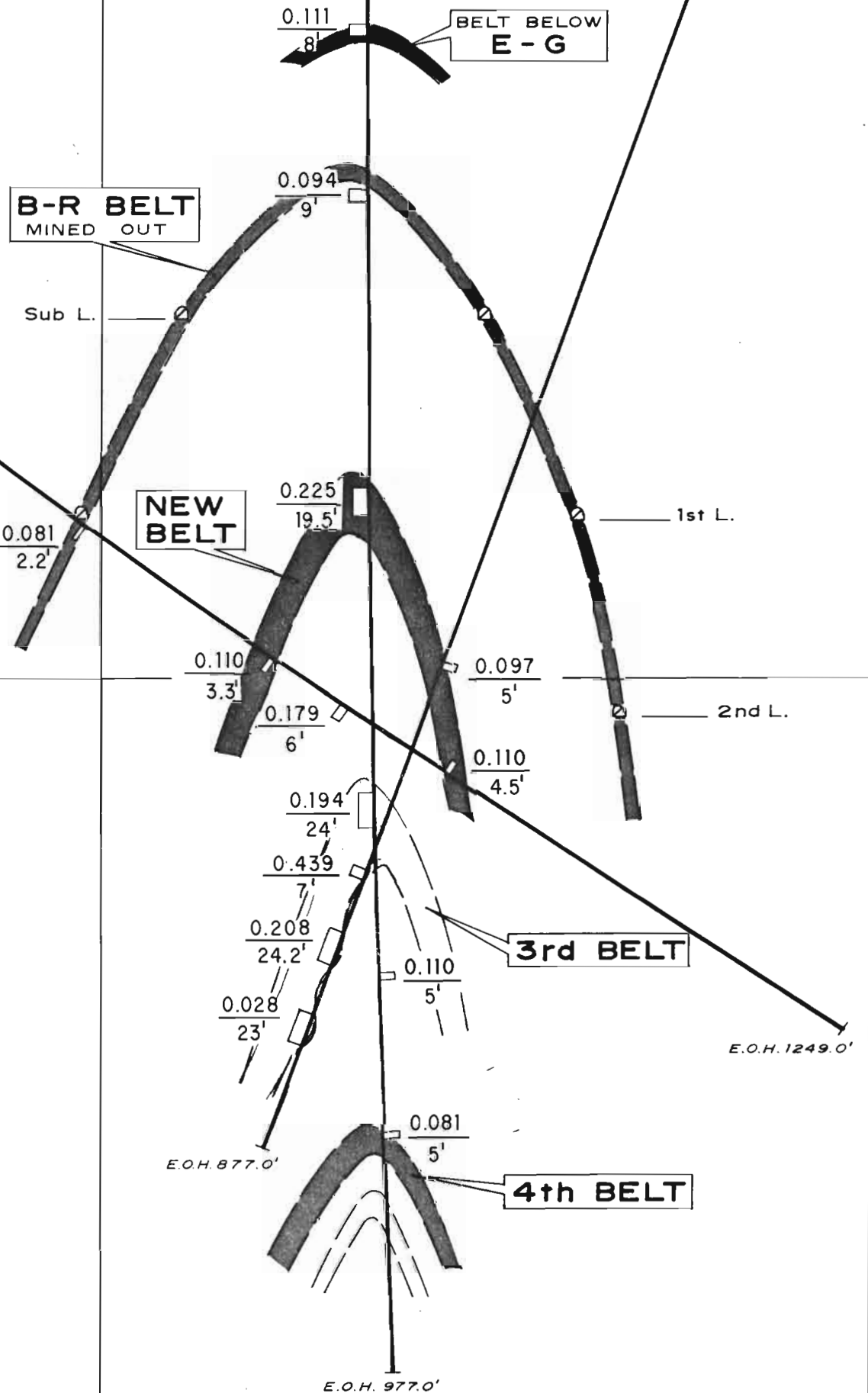
BR-27

-70°

B.L.

-500'L.
(152m.)

-1000'L.
(304m.)



PR 87-003

Trace Of

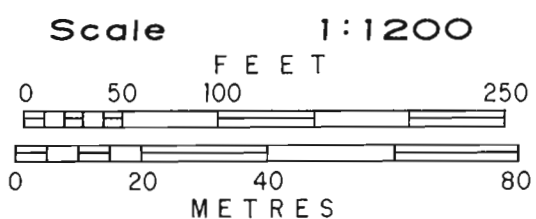
BOSTON-RICHARDSON BELT

& Location Of

NEW BELTS

Sect. 750m.E

NOTE: Assay values expressed as oz/t (Au) over length (ft.)



SOUTH

NORTH

.7B

BR 87-18
Dip - 70°
(825m. E-100m. S)
2707'E-328'S

Proposed Hole

Proposed Hole

- 70°

- 75°

B-R BELT
MINED OUT

1st L.

2nd L.

NEW BELT

3rd BELT

-500'L.
(152m.)

-1000'L.
(304m.)

0.136

8'

0.041

13'

0.370

- 1.5'

900'
(274m)

1100'
(335m.)

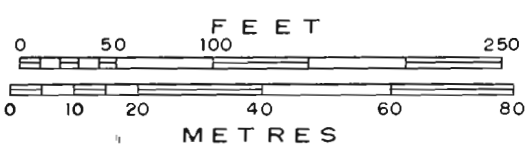
E.O.H. 153.0'

PR 87-003

Trace Of
BOSTON-RICHARDSON BELT
& Location Of
NEW BELT

Sect. 825m.E

Scale 1:1200



SOUTH

NORTH

Proposed Hole

BR87-24

Proposed Hole

-75°

-90°

-85°

BELT BELOW EAST GOLDBROOK ?

0.52
1'

V.G.

0.11
3' B-R BELT

1st L.

-500'L.
(152m.)

2nd L.

0.16
6'

NEW BELT

3rd L.

3RD BELT

0.49
2.9'

4TH BELT ?

0.19
8'

1000'
(304m.)

-1000'L.
(304m.)

5TH BELT ?

0.13
12'

1100'
(335m.)

1200'
(365.8m.)

PR87-003

Trace Of

BOSTON-RICHARDSON BELT

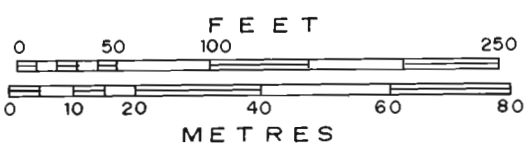
& Location Of

NEW BELT

Sect. 900m.E

NOTE: values expressed as oz / t (Au) over length (ft)

Scale 1:1200



SOUTH

NORTH

BR - 03

BL

Proposed Hole

0

-500'L.
(152m.)

2nd L.

3rd L.

INCLINE

B-R BELT

NEW BELT

3rd BELT

-1000'L.
(304m.)

1200' (365m.) 1386' (422m)

Trace Of

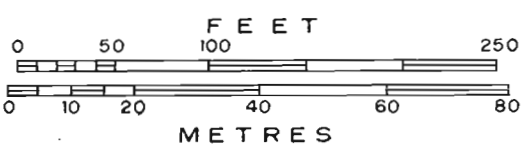
BOSTON-RICHARDSON BELT

& Location Of

NEW BELT

Sect. 975m.E

Scale 1:1200



PR87-003

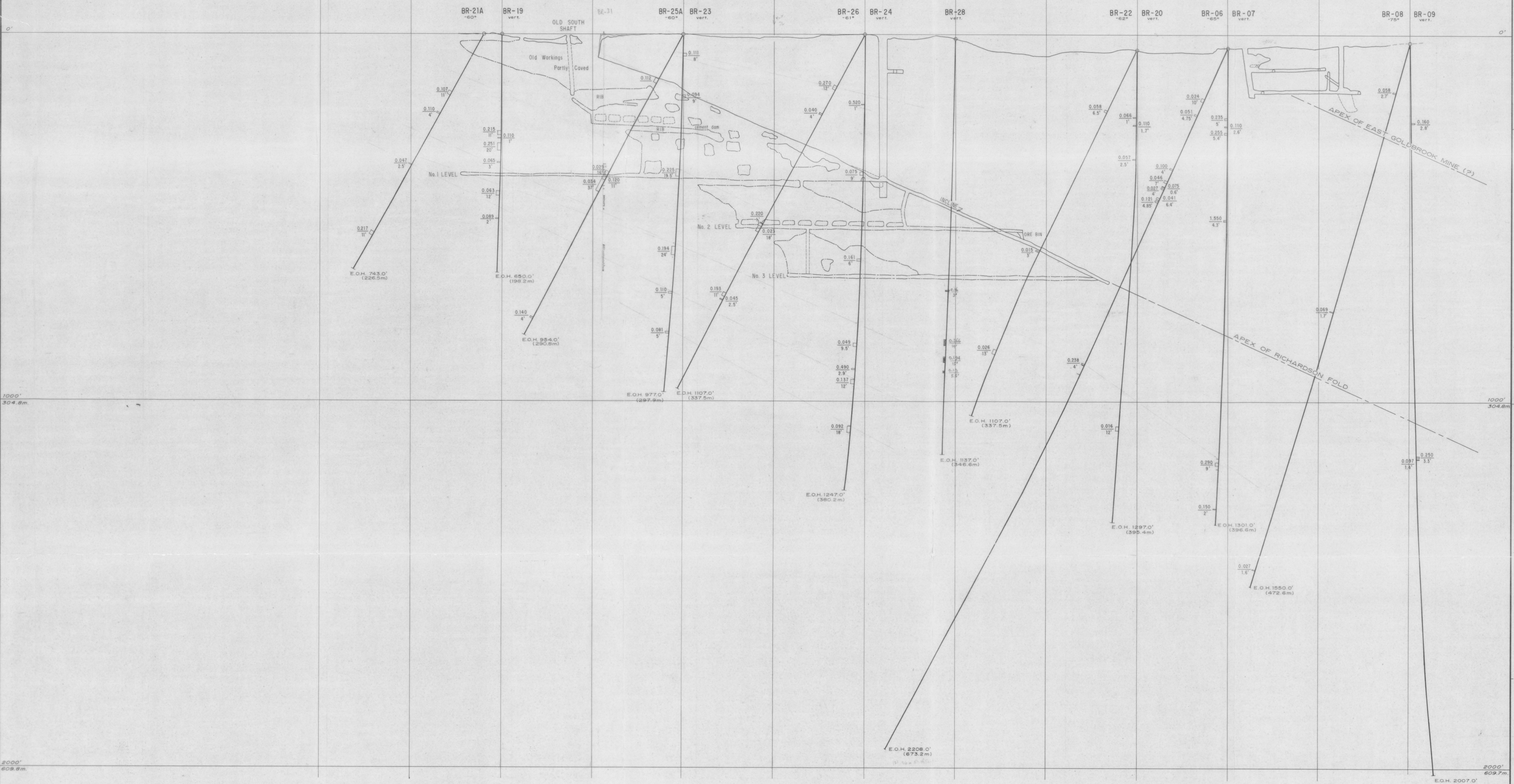
WEST

EAST

450 m.E
525 m.E
600 m.E
675 m.E
750 m.E
825 m.E
900 m.E
975 m.E
1050 m.E
1125 m.E
1200 m.E
1275 m.E
1350 m.E

BOSTON-RICHARDSON MINE

EAST GOLDBROOK MINE



1000'
304.8m

1000'
304.8m

2000'
609.6m

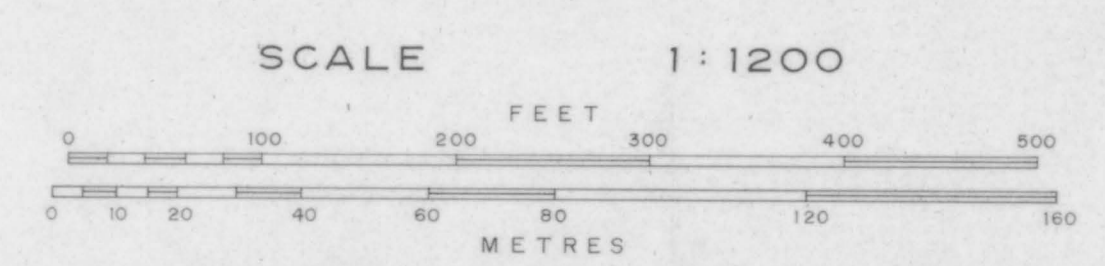
2000'
609.6m

E.O.H. 2007.0'
(611.9m)

LOCATION OF
NEW BELT AND 3RD BELT
BELOW
BOSTON-RICHARDSON MINE

LONGITUDINAL SECTION

LOOKING NORTH



NOTE: Plane of section is at 50m. north of baseline O.